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A PARAMETRIC STUDY OF PLANFORM AND
AEROELASTIC EFFECTS ON AERODYNAMIC CENTER,
 α - AND q - STABILITY DERIVATIVES

APPENDIX A

A COMPUTER PROGRAM FOR CALCULATING
 α - AND q - STABILITY DERIVATIVES AND INDUCED
DRAG FOR THIN ELASTIC AEROPLANES AT
SUBSONIC AND SUPERSONIC SPEEDS

by

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1. INTRODUCTION

The computer program used to determine the rigid and elastic stability derivatives presented in the summary report (Ref. 1) is listed in this appendix along with instructions for its use, sample input data and answers. This program represents the airplane at subsonic and supersonic speeds as (a) thin surface(s) (without dihedral) composed of discrete panels of constant pressure according to the method of Woodward (Ref. 2) for the aerodynamic effects and slender beam(s) for the structural effects.

Given a set of input data, the computer program calculates an aerodynamic influence coefficient matrix [A] and a structural influence coefficient matrix [C] by the methods specified above. In a different option [C] can be read in from tape.

The stability derivatives determined by this program and the equations used in their calculation are given in Table 1. From the table it can be seen that for rigid stability derivatives (as well as ΔC_p) [A] is needed, whereas for elastic stability derivatives both [A] and [C] are required.

The program is compatible with the geometry requirements and definitions of reference 3, using assumptions defined in the Appendix to this report.

Using the method of Reference 4 the program is also capable of computing C_{D_i}/C_L^2 for rigid and elastic wings.

Stability Derivatives for a Rigid Airplane

<u>Derivatives</u>	<u>Formulas</u>	<u>Dimension</u>
$C_{L\alpha}$	$\frac{1}{S} \{1\}^T [A] \{1\}$	radian ⁻¹
C_{Lq}	$-\frac{2}{S\bar{c}} \{1\}^T [A] \{x_i\}$	radian ⁻¹
$C_{m\alpha}$	$\frac{1}{S\bar{c}} \{x_i\}^T [A] \{1\}$	radian ⁻¹
C_{mq}	$-\frac{2}{S\bar{c}^2} \{x_i\}^T [A] \{x_i\}$	radian ⁻¹

Stability Derivatives for an Equivalent Elastic Airplane

	<u>Derivatives</u>	<u>Formulas</u>	<u>Dimension</u>
Zero mass (constant load factor)	$C_{L\alpha_E}$	$\frac{1}{S} \{1\}^T [B][A] \{1\}$	radian ⁻¹
	C_{Lq_E}	$-\frac{2}{S\bar{c}} \{1\}^T [B][A] \{x_i\}$	radian ⁻¹
	$C_{m\alpha_E}$	$\frac{1}{S\bar{c}} \{x_i\}^T [B][A] \{1\}$	radian ⁻¹
	C_{mq_E}	$-\frac{2}{S\bar{c}^2} \{x_i\}^T [B][A] \{x_i\}$	radian ⁻¹

Table 1 Longitudinal Stability Derivatives for Rigid and Elastic Airplanes

Stability Derivatives for an Equivalent Elastic Airplane (continued)

	<u>Derivatives</u>	<u>Formulas</u>	<u>Dimension</u>
Inertial (varying load factor)	C_{Lq_1}	$\frac{2}{S\bar{c}} \{1\}^T [B][A][C] \{m_i\} U_1^2$	non-dim.
	C_{mq_1}	$\frac{2}{S\bar{c}^2} \{x_i\}^T [B][A][C] \{m_i\} U_1^2$	non-dim.
	$C_{L\ddot{\theta}_1}$	$\frac{1}{S} \{1\}^T [B][A][C] \{m_i x_i\}$	sec ²
	$C_{m\ddot{\theta}_1}$	$\frac{1}{S\bar{c}} \{x_i\}^T [B][A][C] \{m_i x_i\}$	sec ²
	$C_{L\dot{w}_1}$	$-\frac{1}{S} \{1\}^T [B][A][C] \{m_i\}$	sec ² ft ⁻¹
	$C_{m\dot{w}_1}$	$-\frac{1}{S\bar{c}} \{x_i\}^T [B][A][C] \{m_i\}$	sec ² ft ⁻¹
	$\frac{\partial C_L}{\partial n}$	$-g C_{L\dot{w}_1}$	non-dim.
	$\frac{\partial C_m}{\partial n}$	$-g C_{m\dot{w}_1}$	non-dim.
	$C_{L\alpha_E}$	$(1 - \frac{\partial C_L}{\partial n} \frac{1}{C_{L_{trim}}})^{-1} C_{L\alpha_E}$	radian ⁻¹
	$C_{m\alpha_E}$	$C_{m\alpha_E} + \frac{\partial C_m}{\partial n} (\frac{C_{L\alpha_E}}{C_{L_{trim}} - \frac{\partial C_L}{\partial n}})$	radian ⁻¹

Note: $[B] = [[1] \quad -\bar{q}_1 [A][C]]^{-1}$

Table 1 Longitudinal Stability Derivatives for Rigid and Elastic Airplanes (Concluded)

2. TABLE OF SYMBOLS

The units used for the physical quantities defined in this paper are given both in the International System of Units (SI) and the U.S. Customary Units.

<u>Symbols</u>	<u>Input Data</u> <u>Description</u>	<u>Dimension</u>
ALT	Altitude	Feet (m.)
ALTNUM	Number of altitude runs to be made	
AM	Mach Number	
AMASS (I)	Mass of panel "I"	slugs (Kgm)
[C]	Structural influence coefficient matrix	rad/lb. (rad/N.)
c_{ij}	Structural influence coefficient, angle of attack induced on panel i due to a unit load on panel j	rad/lb (rad/N)
CLDES	Desired lift coefficient	
CPCWL	Constant percent chord-wise lines	
CPSWL	Constant percent stream-wise lines	
CREF	Reference Chord	Feet (m.)
CSHT	Structural root chord of the horizontal tail	Feet (m.)
CSMW	Structural root chord of the main wing	Feet (m.)
EI (I)	EI value of the Ith elastic axis segment	lb - inch ² (N-m ²) or lb - ft ²
GJ (I)	GJ value of the Ith elastic axis segment	lb - inch ² or lb - ft ² (N-m ²)
IASIGN (K)	The Kth element of the array IASIGN and the number of an elastic axis end-point to which the Kth panel is attached	
KONTL	= 1 for fuselage geometry data = 2 for wing geometry data = 3 for horizontal tail geometry data = 4 for canard geometry data	

<u>Symbols</u>	<u>Description</u>	<u>Dimension</u>
LPNL (1)	Number of panels on front fuselage	
LPNL (2)	Number of panels on rear fuselage	
LPNL (3)	Numbers of panels on main wing	
LPNL (4)	Number of panels on horizontal tail	
M	Maximum number of elastic axis end-points	
MOVTEL	= 0, Non-movable tail = 1, Movable tail	
N	Total number of panels or, total number of unit loading points	
NI	Attachment point of horizontal tail elastic axis to rear fuselage elastic axis, point number	
NC	Number of sections of the aerodynamic surface	
NCNTL	See Sec. 4 for complete description	
NCNTL	= 0 if geometry data are input according to the present program = 1 if geometry data are prepared according to Ref. 1	
NCNTL	= 1 for front fuselage data = 2 for rear fuselage data = 3 for main wing data = 4 for horizontal tail data	
NCP1	Number of CPCWL on fuselage	
NCP2	Number of CPCWL on wing	
NCP3	Number of CPCWL on horizontal tail	
NCP4	Number of CPCWL on canard	
NCPSWL	Number of constant percent stream-wise lines	
NEA	Number of elastic axis end-points	

<u>Symbols</u>	<u>Description</u>	<u>Dimension</u>
NEI GJ	= 0 if EI and GJ values are in lb-inch ² = 1 if EI and GJ values are in lb-ft ²	
RHO	Air density	Slugs/ft ³ (Kg/m ³)
SOS	Speed of sound	ft/sec. (m/sec)
SREF	Reference area	ft ² (m ²)
TITLE	Any title for computer run	
W	Total weight of the airplane	lb. (N.)
WDTHHT	One-half the width of the fuselage at the horizontal tail	Feet (m)
WDTHMW	One-half the width of the fuselage at the main wing	Feet (m)
XCG (I)	x-coordinate of the loading point "I"	Feet (m)
XEA (I)	x-coordinate of the elastic axis end-point "I"	Feet (m)
XREF	Attachment point of the main wing elastic axis to the fuselage elastic axis, x-coordinate	Feet (m)
XXL (1)	x-coordinate of the L.E. of inboard chord	Feet (m)
XXL (2)	x-coordinate of L.E. of outboard chord	Feet (m)
XXT (1)	x-coordinate of T.E. of inboard chord	Feet (m)
XXT (2)	x-coordinate of T.E. of outboard chord	Feet (m)
YCG (I)	y-coordinate of the loading point "I"	Feet (m)
YEA (I)	y-coordinate of the elastic axis end-point "I"	Feet (m)
YL (1)	y-coordinate of inboard chord	Feet (m)
YL (2)	y-coordinate of outboard chord	Feet (m)
Z	Z-coordinate of the section under consideration	Feet (m)

Output Data

<u>Symbols</u>	<u>Description</u>	<u>Dimension</u>
[A]	Aerodynamic influence coefficient matrix	$\text{ft}^2 \text{rad}^{-1} (\text{m}^2 \text{rad}^{-1})$
a_{ij}	Aerodynamic influence coefficient, load on panel i resulting from a unit angle of attack on panel j	$\text{ft}^2 \text{rad}^{-1} (\text{m}^2 \text{rad}^{-1})$
ALTITUDE	Altitude	Feet (m)
AREA	Area of a panel	$(\text{Feet})^2 (\text{m}^2)$
CD	Total induced drag coefficient	
CDI	Sectional induced drag coefficient (C_{di})	
CL	Total lift coefficient	
CLALPA	$C_{L\alpha_E}$, Variation of lift coefficient with angle of attack for the elastic case with zero mass	per rad.
CLALPE	$C_{L\alpha_E}$, Variation of lift coefficient with angle of attack for the elastic case including mass effect	per rad.
CLALPR	$C_{L\alpha}$, Airplane lift curve slope	per rad.
CLI	Sectional lift coefficient (C_l)	
CLQ	C_{Lq} , Variation of lift coefficient with pitch rate	per rad.
CLQEBR	C_{Lq_E} , Variation of lift coefficient with pitch rate for the elastic case with zero mass	per rad.
CLQI	C_{Lq_I} , Inertially induced variation of lift coefficient with pitch rate	
CLTDDI	$C_{L\ddot{\theta}_I}$, Inertially induced variation of lift coefficient with pitch angular acceleration	sec.^2
CLTRIM	$C_{L_{Trim}}$	

<u>Symbols</u>	<u>Description</u>	<u>Dimension</u>
CLWDI	$C_{L\dot{w}_I}$, Inertially induced variation of lift coefficient with rate of downward velocity perturbation	sec. ² per ft. (sec ² /m)
CMALPA	$C_{m\alpha_E}$, Variation of pitching moment coefficient with angle of attack for the elastic case with zero mass	per rad.
CMALPE	$C_{m\alpha_E}$, Variation of pitching moment coefficient with angle of attack for the elastic case including mass effect	per rad.
CMALPR	$C_{m\alpha}$, Variation of pitching moment coefficient with angle of attack (i.e., static longitudinal stability)	per rad.
CMQ	C_{mq} , Variation of pitching moment coefficient with pitch rate	per rad.
CMQEBR	C_{mq_E} , Variation of pitching moment coefficient with pitch rate for the elastic case with zero mass	per rad.
CMQI	C_{mq_I} , Inertially induced variation of pitching moment coefficient with pitch rate	
CMTDDI	$C_{m\ddot{\theta}_I}$, Inertially induced variation of pitching moment coefficient with pitch angular acceleration	sec. ²
CMWDI	$C_{m\dot{w}_I}$, Inertially induced variation of pitching moment coefficient with rate of downward velocity perturbation	sec. ² per ft (sec. ² /m)
CP	ΔC_p , Change in pressure coefficient between upper and lower surfaces	
CT	Sectional leading edge thrust coefficient	
DCLDN	$\partial C_L / \partial n$, Variation of lift coefficient with load factor	

<u>Symbols</u>	<u>Description</u>	<u>Dimension</u>
DCMDN	$\partial C_m / \partial n$, Variation of pitching moment coefficient with load factor	
DYNAMIC PRESSURE	Dynamic pressure	lb per ft ² (N/m ²)
EI (I)	EI Value for the Ith elastic axis segment	lb-ft ² (N-m ²)
GAMMA	Non-dimensional local circulation ($C_{i_c}/2b$)	
GJ (I)	GJ value for the Ith elastic axis segment	lb-ft ² (N-m ²)
IASIGN (I)	Number of elastic axis end-point to which panel "I" is attached	
MASS (I)	Mass of Ith panel	Slugs (Kg)
REF. AREA	Reference area	(Feet) ² (m ²)
REF. CHORD	Reference chord	Feet (m)
RHO	Air density	Slugs/ft ³ (Kg/m ³)
SOS	Speed of sound	ft. per. sec. (m/sec)
VELOCITY	= (Mach Number) x (speed of sound)	ft. per. sec. (m/sec)
WEIGHT	Weight of the airplane	lb. (N)
XCG (I)	x-coordinate of the centroid of Ith panel or the Ith unit loading point	Feet (m)
XCP (I)	x-coordinate of the control point of Ith panel	Feet (m)
YEA (I)	x-coordinate of the Ith elastic axis end-point	Feet (m)
Y	Non-dimensional spanwise location	
YCG (I)	y-coordinate of the centroid of Ith panel or the Ith unit loading point	Feet (m)
YCP (I)	y-coordinate of the control point of Ith panel	Feet (m)
YEA (I)	y-coordinate of the Ith elastic axis end-point	Feet (m)
ZCP (I)	z-coordinate of the control point of Ith panel	Feet (m)

3. PREPARATION OF INPUT DATA

The preparation of input data for this computer program is done in three steps:

- Step 1 Preparation of planform geometry data (Sec. 3.1)
- Step 2 Preparation of mass distribution data (Sec. 3.2)
- Step 3 Preparation of structural data (Sec. 3.3)

3.1 Preparation of Planform Geometry Data

The ground rules for defining the planform geometry and for dividing a planform into aerodynamic panels are described below.

A general planform is taken as an example. Its projections in the x-y plane and the x-z plane are given in Figure 1.

The following paneling definitions should be observed.

1 Break Lines

A break line on a planform is a stream line which connects the leading and trailing edges and occurs when either the leading - or trailing - edge has a slope discontinuity. Root and tip chords are also considered as break lines. A break line on one lifting surface creates a break line on the others. (See Figure 1.)

Referring to the x-y plane view of the planform, there are 14 break lines. Table 2 defines these break lines precisely.

TABLE 2

<u>Break Line</u>	<u>Explanation</u>
1-1'	Root chord of fuselage
2-2'	Tip chord of fuselage
3-3'	Root chord of wing
4-4'	Due to fuselage-wing overlapping
5-5'	Due to break line 12-12' on horizontal tail
6-6'	Due to slope discontinuity at 6'
7-7'	Due to break line 14-14' on horizontal tail
8-8'	Due to slope discontinuity at 8
9-9'	Tip chord of wing
10-10'	Root chord of horizontal tail
11-11'	Due to horizontal tail-fuselage overlapping
12-12'	Due to slope discontinuity at 12
13-13'	Due to break line 6-6'
14-14'	Tip chord of horizontal tail

2 Sections

A section is a region on the configuration between two consecutive break lines. For the example planform of Figure 1 there are seen to be 11 sections.

The variable NC on input card 4 sets the number of sections.

3 Constant Percent Chordwise Lines (CPCWL)

These are the lines which divide the sections in the chordwise direction. In general there could be any number of CPCWL's in a section. In the current program it is limited to 35. These can be different on different aerodynamic surfaces. The 0% and 100% lines are the leading and trailing edges of the section. For accurate values of C_{D_i} / C_L^2 , these lines are selected by using the scheme given in Ref. 3.

4 Constant Percent Streamwise Lines (CPSWL)

These are the lines which divide the section in the streamwise direction. In general

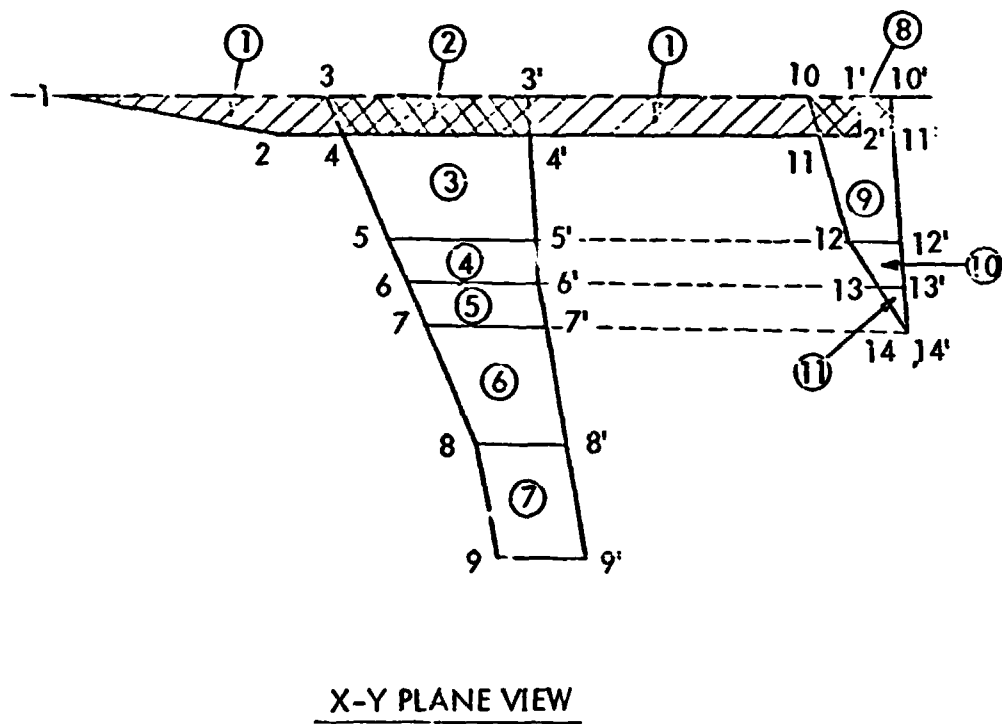
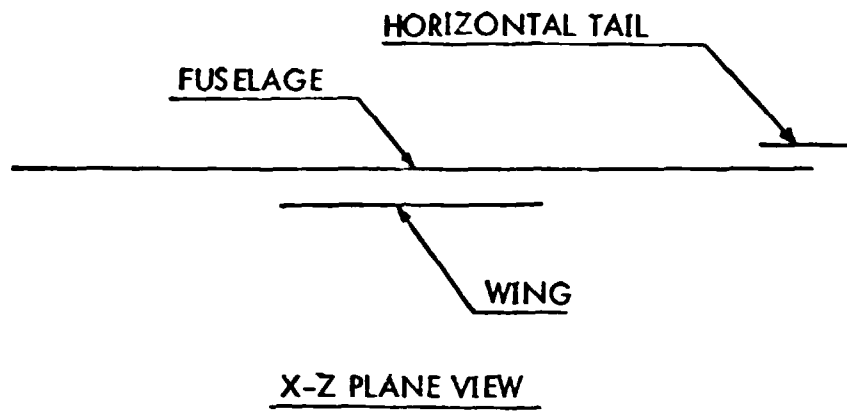


Figure 1. Example Platform

there could be any number of CPSWL's in a section. In the current program it is limited to 35. However, in case one section is behind another section in the streamwise direction, or one section is directly above another section, it is desirable to use the same CPSWL's. The 0% and 100% lines are the inboard and outboard chords of the section.

5 Panel Numbers

Panels are numbered in the increasing order of section numbers, from inboard to outboard of the section and from the leading edge to the trailing edge.

6 Total Number of Panels (N)

The present computer program is limited to 300 panels.

7 Control Point of a Panel

In all cases the downwash control point is located at 0.95 of the local chord which passes through the centroid of the panel.

3.2 Preparation of Mass Distribution Data

In the wing-body-tail program there are three different types of mass distributions to be considered: wing mass, body mass and tail mass. A procedure for determining these masses cannot be given such that all types of airplanes are covered by it. For the family of parametric wings studied herein, a detailed procedure for the calculation of mass distribution is included in Appendix D of the Summary Report (Ref. 5). It is possible to develop such procedures for tails and fuselages of parametric families of airplanes.

The user of this complete WBH program has the following options:

- a) read in a complete mass matrix from an external source.
- b) use the procedure developed for the parametric family of wings in Ref. 1 to find the wing part of the mass matrix. Read in the other mass contributions from an external source.
- c) neglect the effect of mass and mass distribution.

Whether or not option c) is realistic depends on the type of airplane under study. In Ref. 1 it was shown that in many instances the effect of mass is negligible. For transport type (low load-factor type) airplanes this is definitely not so.

3.3 Preparation of Structural Data

Given an EI distribution for fuselage and EI and GJ distribution for wing and horizontal tail, the method given in Appendix E of the Summary Report (Ref. 6) is used to determine all the input data for structural matrix.

4. INPUT DATA FORMAT

This computer program has five different options, depending upon the value of "NCNTL", which appears on input data card number 1.

NCNTL	Input Cards	Program Computes	Program Outputs
0	All cards except 16	[A], Rigid derivatives, Δ Cp, [C], Elastic derivatives	Rigid derivatives, Δ Cp, Elastic derivatives
1	Cards 0, 1 thru 11	[A], Rigid derivatives, Δ Cp	Rigid derivatives, Δ Cp
2	Cards 0, 1 and 13 thru 20	[C]	[C]
3	Cards 0 thru 12 and 21 and 22	[A], Rigid derivatives, Δ Cp, Elastic derivatives	Rigid derivatives, Δ Cp, Elastic derivatives
4	All cards except 16	[A], Rigid derivatives, Δ Cp, [C], Elastic derivatives	Rigid derivatives, Δ Cp, [C], Elastic derivatives

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
0	(16A5)	TITLE	Any title for computer run
1	(3I3)	N*	Total number of panels or number of unit loading points
		M	Number of elastic axis end points of that elastic axis which has the maximum number of end points.
		NCNTL	= 0 Calculates [A], ΔC_p , [C] and all the derivatives = 1 Calculates [A], ΔC_p and rigid derivatives = 2 Calculates only [C] with printout = 3 Calculates [A], ΔC_p , rigid derivatives then reads [C] from tape and calculates elastic derivatives = 4 Calculates [A], ΔC_p , [C] and all the derivatives. Also prints out [C].
2	(I2)	NCONT	= 0 Input to be prepared according to the present program = 1 Use configuration data cards of Ref. 3 (except card 1). (For assumptions of data reduction see Appendix)
3	(4I2)	NCP1	Number of constant percent chordwise lines on fuselage.
		NCP2	Number of constant percent chordwise lines on wing.
		NCP3	Number of constant percent chordwise lines on horizontal tail.
		NCP4	Number of constant percent chordwise lines on canard.
		If NCONT = 1, skip to card number 7	
4	(I2)	NC	Number of sections of the aerodynamic surfaces.

*'N' must be inputted if NCNTL = 2

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
5	(2I2)	NCPSWL KONTL	Number of constant percent streamwise lines = 1 for fuselage data = 2 for wing data = 3 for horizontal tail data = 4 for canard data
6	(7F10.5)	XXL (1) XXT (1) YL (1) XXL (2) XXT (2) YL (2) Z	Array of points defining x- and y- coordinates of leading and trailing edges of break lines arranged in order from inboard to outboard, and corresponding z- coordinate
7	(8F10.5)	CPCWL (1) CPCWL (2) CPCWL (3) CPCWL (4) CPCWL (5) CPCWL (6) CPCWL (7) CPCWL (8)	An array defining the locations of constant percent chordwise lines. This card is used only the first time the value of KONTL is defined for each aerodynamic surface. There must be NN* numbers; 8 numbers per card. *NN = NCP1, if KONTL = 1, i.e. fuselage = NCP2, if KONTL = 2, i.e. wing = NCP3, if KONTL = 3, i.e. horizontal tail = NCP4, if KONTL = 4, i.e. canard If NCONT = 1, the CPCWL's are inputted for fuselage, wing, horizontal tail and canard respectively.
8	(8F10.5)	If NCONT = 1, skip to card number 10 CPSWL (1)	An array defining the locations of constant percent streamwise lines for a section of the aerodynamic surface. There must be NCPSWL numbers; 8 numbers per card.

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
		CPSWL (2) (3) (4) (5) (6) (7) (8)	
			Cards 5 thru 8 are repeated NC times.
9	(2F10.5)	SREF CCREF	Reference wing area Reference chord
10	(F10.5)	CCREF	Reference chord If SREF = 0 Program takes the true area as reference area. If CCREF = 0 Program takes the inboard chord of the last processed region as reference chord.
11	(2F10.5)	AM	Mach Number

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
12	(8F10.5)	CLDES AMASS (1) AMASS (2) AMASS (3) AMASS (4) AMASS (5) AMASS (6) AMASS (7) AMASS (8)	Desired lift coefficient for ΔC_p values. If CLDES = 0 ΔC_p values are calculated for $\alpha = 1.0$ radian. An array defining masses of panels. There must be "N" numbers, 8 numbers per card.
13	(7I3)	LPNL (1) LPNL (2) LPNL (3) LPNL (4) N1 MOVTEL NEIGJ	Number of panels on front fuselage Number of panels on rear fuselage Number of panels on wing Number of panels on horizontal tail Attachment point of horizontal tail elastic axis to rear fuselage elastic axis, point number on the rear fuselage elastic axis. = 0, Non-movable tail = 1, Movable tail = 0, If wing dimensions are in feet and EI and GJ values are in lb-inch ² . = 1, If wing dimensions and EI and GJ are in consistent units (feet only). In case other units are used card number 19 is to be changed

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
14	(40I2)	IASIGN (1) IASIGN (2) IASIGN (3) IASIGN (4) IASIGN (5) . . . (40)	IASIGN (k) is the kth element of the array IASIGN and is the number of an elastic axis end-point to which the kth panel is attached. There must be "N" numbers; 40 numbers per card.
15	(5F10.5)	CSMW CSHT WDTHMW WDTHHT XREF	Structural root chord of the main wing Structural root chord of the horizontal tail One-half the width of the fuselage at the main wing One-half the width of the fuselage at the horizontal tail Attachment point of main wing elastic axis to fuselage elastic axis, x- coordinate.
16	If NCNTL \neq 2, skip to card number 17. (8F10.5)	XCG (1) YCG (1) (2) (2) (3) (3) (4) (4)	x- and y- coordinates of loading points. There must be "2N" numbers, 8 numbers per card.
17	(2I2)	NCNTL	Control number to represent the part of airplane for which XEA, YEA, EI and GJ values are being inputted in next cards. = 1 Front fuselage = 2 Rear fuselage = 3 Main wing = 4 Horizontal tail

<u>Card Number</u>	<u>Format</u>	<u>Code</u>	<u>Explanation</u>
18	(8F10.5)	NEA XEA (1) YEA (1) (2) (2) (3) (3) (4) (4)	Number of end-points of elastic axis segments of part of airplane under consideration x- and y- coordinates of end-points of elastic axis. There must be "2XNEA" numbers; 8 numbers per card.
19	(4E15.8)	EI (1) GJ (1) EI (2) GJ (2)	EI and GJ values of elastic axis segments for part of airplane under consideration. There must be "2X(NEA - 1)" numbers, 4 numbers per card.
20	Blank card		Indicates that structural data is over
21	(2F10.5)	W ALTNUM	Total weight of aircraft Number of altitude cases to be run.
22	(3F10.5)	RHO SOS ALT	Density (Slugs per ft ³) Speed of sound (ft. per second) Altitude (ft.)
			Card 22 is repeated "ALTNUM" times.

To obtain [C] for complete airplane, cards 17, 18, and 19 must be repeated with "NCONTL" equal to 1, 2, 3 and 4, with corresponding values of NEA, XEA, YEA, EI and GJ.

5. OUTPUT DATA FORMAT

The output data are divided into five sections.

1. Geometry data

The planform geometry data is outputted exactly in the same way as it was inputted. The format is self-explanatory in the output printout. The output variables are:

- a) The number of sections into which the planform is divided.
- b) For each section inboard and outboard chord coordinates are given along with the constant percent chordwise lines and constant percent streamwise lines for that section.
- c) REF. AREA and REF. CHORD represent the reference area and the reference chord respectively.

2. Rigid longitudinal derivatives

Computer Variable	Explanation
CLALPR	$C_{L\alpha}$
CMALPR	$C_{m\alpha}$
CLQ	C_{Lq}
CMQ	C_{mq}

3. Sectional C_{di}/C_L^2 and the total induced drag parameter C_{Di}/C_L^2 for rigid configuration

Computer Variable	Explanation
Y	Non-dimensional spanwise location
CDI	Sectional induced drag coefficient (C_{di})
CLI	Sectional lift coefficient (C_l)
GAMMA	$= C_l C / 2b$ where C = local chord
CT	Sectional leading edge thrust
CDI/CL * * 2	$= C_{di}/C_L^2$
CD/(CL * CL)	$= \frac{\text{Total Induced Drag Coefficient}}{C_L^2}$

4. ΔC_p values for $C_{Ldes.}$ or $\alpha = 1.0$ radians

<u>Computer Variable</u>	<u>Explanation</u>
PANEL NUMBER	Panel number
(XCP, YCP, ZCP)	Control point location
(XCG, YCP = YCG)	Panel centroid location
AREA	Panel area
CP	ΔC_p
MASS	Mass of the panel

5. Panel assignment output

<u>Computer Variable</u>	<u>Explanation</u>
I	Panel number or unit loading point number
(XCG, YCG)	Panel centroid location or unit loading point location
IASIGN	Number of elastic axis end-point to which panel "I" is attached.

6. Elastic axis data

<u>Computer Variable</u>	<u>Explanation</u>
I	Elastic axis end-point number
(XEA, YEA)	Elastic axis end-point location
EI	EI value of the Ith elastic axis segment.
GJ	GJ value of the Ith elastic axis segment.

7. Elastic longitudinal derivatives

<u>Computer Variable</u>	<u>Explanation</u>
WEIGHT	Total weight of the airplane
RHO SOS ALTITUDE	Air density and speed of sound at that altitude
VELOCITY	= (Mach Number X Speed of sound)

DYNAMIC PRESSURE

Dynamic pressure

CLTRIM

$C_{L_{trim}}$

CLALPA

$C_{L_{\alpha_E}}$

CMALPA

C_{m_r}

CLQEBR

$C_{L_{q_E}}$

CMQEBR

$C_{m_{q_E}}$

CLQI

$C_{L_{q_I}}$

CMQI

$C_{m_{q_I}}$

CLWDI

$C_{L_{\dot{w}_I}}$

CMWDI

$C_{m_{\dot{w}_I}}$

CLTDDI

$C_{L_{\ddot{\theta}_I}}$

CMTDDI

$C_{m_{\ddot{\theta}_I}}$

DCLDN

$\partial C_L / \partial n$

DCMDN

$\partial C_m / \partial n$

CLALPE

$C_{L_{\alpha_E}}$

CMALPE

$C_{m_{\alpha_E}}$

8. Cp values for deformed shape

<u>Computer Variables</u>	<u>Explanation</u>
PANEL NUMBER	Panel Number
THETA (E)	θ_E , in rad
CP (E)	ΔC_p

9. Sectional C_{di}/C_L^2 and the total induced drag parameter C_{Di}/C_L^2 for elastic configuration

<u>Computer Variables</u>	<u>Explanation</u>
Y	Non-dimensional spanwise location
CDI	Sectional induced drag coefficient (C_{di})
CLI	Sectional lift coefficient (C_{li})
GAMMA	$= C_{li} C / 2b$
$CDI/C_L^2 * * 2$	$= C_{di}/C_L^2$
$CD/(CL * CL)$	$= \frac{\text{Total Induced Drag Coefficient}}{C_L^2}$

6. TEST CASE 1

This test case deals with Wing 5 of Ref. 1 (see Fig. 2). An input data cards listing is given in Table 3. Output data for this test case are presented in Table 4.

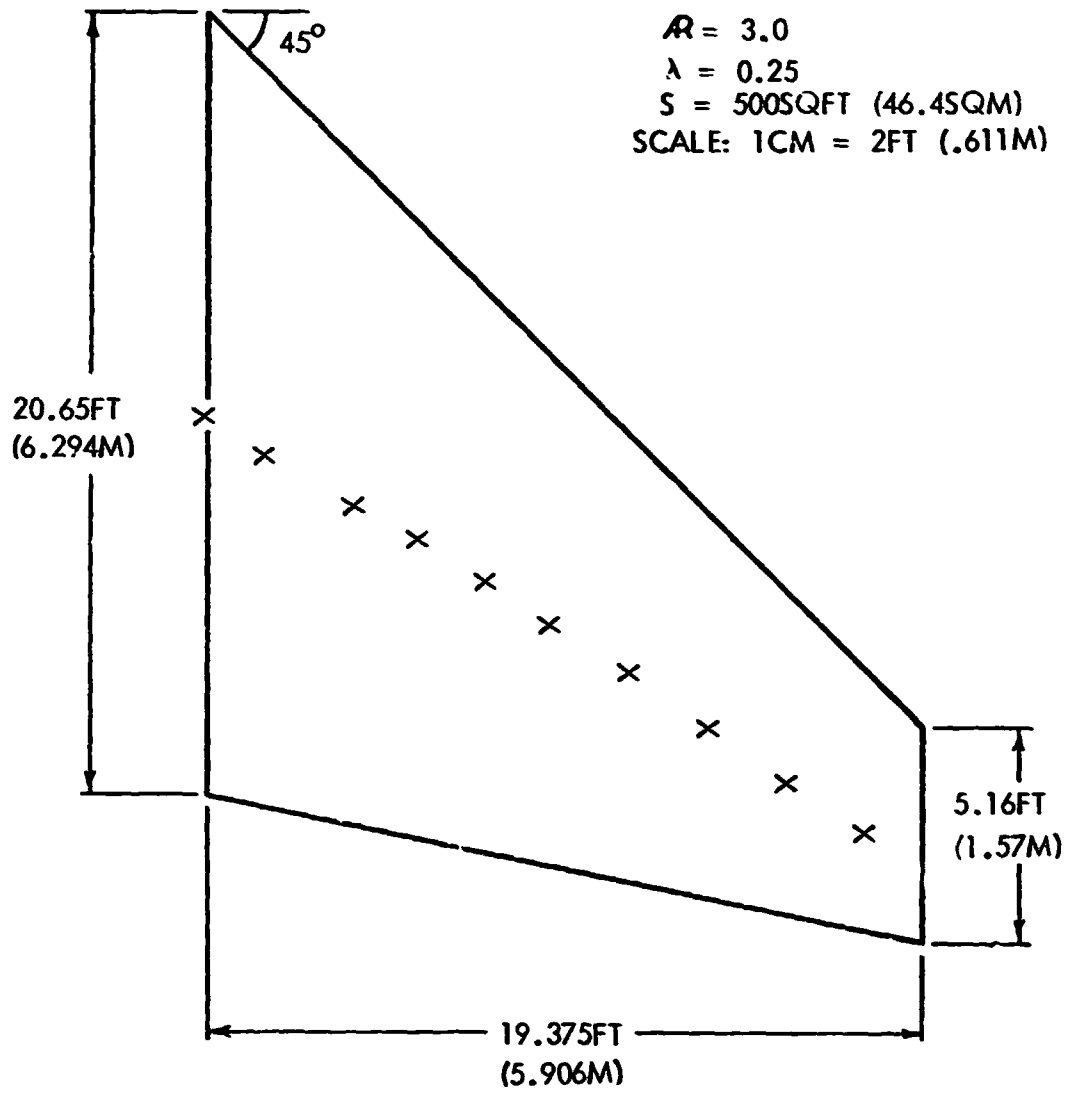


Figure 2. Test Case 1 Platform

Table 3. Listing of Input Data Cards for Test Case 1

Card	TEST CASE 1									
	0	1	2	3	4	5	6	7	8	9
0	0009	01	1102	0.	0.	0.	10.	90.	0.	100.
1				20.65	1.02	10.	90.			
2				19.375	21.	30.				
3				19.375	21.	30.				
4				24.535	33.	40.				
5				19.375	48.	50.				
6				0.	63.	60.				
7				81.						
8				70.						
9										
10										
11				0.	0.	0.	0.	0.	0.	0.
12	0.05274	0.56760	0.74961	9.78339	12.22919	12.22919	12.22919	12.22919	6.55827	2.42984
13	0.05140	0.55315	0.73052	8.87890	11.09857	11.09857	11.09857	11.09857	6.07640	2.39232
14	0.05000	0.53814	0.71070	7.97039	9.96294	9.96294	9.96294	9.96294	5.59139	2.35336
15	0.0481	0.51868	0.68500	7.04972	8.81210	8.81210	8.81210	8.81210	5.09118	2.30285
16	0.04582	0.49310	0.65123	6.11485	7.64351	7.64351	7.64351	7.64351	4.57134	2.23648
17	0.04298	0.46253	0.61085	5.16380	6.45471	6.45471	6.45471	6.45471	4.03316	2.15711
18	0.03962	0.42639	0.56313	4.19757	5.24692	5.24692	5.24692	5.24692	3.47600	2.06332
19	0.03533	0.38025	0.50219	3.20649	4.00808	4.00808	4.00808	4.00808	2.88591	1.94355
20	0.02856	0.30742	0.40601	2.14000	2.67498	2.67498	2.67498	2.67498	2.20343	1.75451
21	0.01296	0.13953	0.18482	0.81376	1.01719	1.01719	1.01719	1.01719	1.19627	1.31873
22	0.00000	0.00000	0.00000							
23	0.00000	0.00000	0.00000							
24	0.02020	0.20303	0.20202	0.30404	0.20202	0.30404	0.40505	0.30404	0.40505	0.50606
25	0.05050	0.70707	0.70808	0.70708	0.80808	0.80909	0.90909	0.90909	0.10101	0.10101
26	0.310									
27	10.6717	0.	11.6527	1.58.	12.8427	3.93	13.8427	5.78		
28	14.9027	7.59	16.0427	9.40	17.3727	11.43	18.7627	13.57		

Table 3 (Continued) Listing of Input Data Cards for Test Case 1

Card	20.1827	15.67	21.5827	17.95	E0109.9	E009
18						
19	1.43	E0101.22	E0101.15		E0109.9	E009
19	7.9	E0096.4	E0095.3		E0094.0	E009
19	3.5	E0092.8	E0092.2		E0091.8	E009
19	1.1	E0099.0	E0084.6		E0083.9	E008
19	1.8	E0081.6	E008			
20						
21	40000.	1.				
22	0.002378	1116.89	0.			

Table 4. Output for Test Case 1

TEST CASE 1

 * GEOMETRY DATA IS DIVIDED IN TO 3 SECTIONS *

DEFINITION OF SECTION 1

```

*****
X-LEADING EDGE      X-TRAILING EDGE      Y-LEADING EDGE      Z
0.000000            20.650000            0.000000            0.000000
19.375000            24.535000            19.375000            0.000000
THERE ARE 9 CONSTANT PERCENT CHORDWISE LINES AT
0.000000            12.000000            21.000000            33.000000            48.000000            63.000000            81.000000            100.000000
THERE ARE 11 CONSTANT PERCENT STREAMWISE LINES AT
0.000000            10.000000            20.000000            30.000000            40.000000            50.000000            60.000000            70.000000            80.000000            90.000000            100.000000
REF. AREA= 0.90073E 03
REF. CHORD= 0.20533E 02
CLALPR = 0.34357E 01
CPALPR = 0.324543E 01
CLG     = 0.49350E 01
CMG     = 0.39753E 01
    
```

SECTIONAL CD/CL/CL2 FOR WIND

CD	CL1	GAMMA	CT	CD/CL/CL2
0.04935	2.23450	0.65032	0.00000	0.021471
0.14930	2.73837	0.64793	0.00000	0.21190
0.24923	2.97042	0.64391	0.00000	0.25164
0.34915	3.22645	0.63853	0.00000	0.27333
0.44906	3.51039	0.62828	0.00000	0.29739
0.54894	3.82793	0.59996	0.00000	0.32478
0.64879	4.18995	0.57308	0.00000	0.35435
0.74857	4.59807	0.53721	0.00000	0.38953
0.84828	4.90074	0.47491	0.00000	0.41917
0.94782	4.40561	0.33927	0.00000	0.37323

TOTAL LEADING EDGE THRUST COEFFICIENT= 0.
 TOTAL INDUCED DRAG COEFFICIENT= 0.34357E 01
 CD/CL/CL2= 0.25136E 00

MACH NUMBER = 1.50

CP VALUES ARE FOR ALPHA 1.00000 RADIAN

PANEL NUMBER	XC	YCP	ZCP	XCG	AREA	CP	MASS
1	1.14394	0.95617	0.	1.05718	0.39279	0.73427E 01	0.0527400
2	3.23226	0.95617	0.	2.25072	4.22926	0.297761E 01	0.5674000
3	5.34255	0.95617	0.	4.23728	3.40379	0.25439E 01	0.7446100
4	7.39709	0.95617	0.	6.32537	4.62125	0.24591E 01	9.7933900
5	10.35209	0.95617	0.	9.00926	5.76332	0.24225E 01	12.2221200
6	13.33993	0.95617	0.	11.99225	5.77632	0.24225E 01	12.2221200
7	16.98490	0.95617	0.	15.27377	6.93158	0.23959E 01	6.5582700
8	20.55291	0.95617	0.	18.95200	7.31667	0.23686E 01	2.4298400
9	3.7229	2.8250	0.	2.98612	0.36218	0.79479E 01	0.0511000
10	4.99242	2.8250	0.	4.09437	3.99473	0.34973E 01	0.5531500
11	6.56324	2.8250	0.	5.91428	3.19568	0.29500E 01	0.7306200
12	8.3332	2.8250	0.	7.84370	4.2691	0.2581E 01	8.4709
13	11.55203	2.8250	0.	10.31225	5.3614	0.25255E 01	11.098700
14	14.30754	2.8250	0.	13.06987	5.72614	0.24645E 01	11.098700
15	17.58397	2.8250	0.	16.09554	6.39137	0.24350E 01	6.0764000
16	21.25391	2.8250	0.	19.48766	6.74644	0.24152E 01	2.3923200
17	4.79153	4.82894	0.	4.91447	0.31157	0.79279E 01	0.0500000
18	6.75149	4.82894	0.	5.92183	3.59210	0.47256E 01	0.5311400
19	8.2737	4.82894	0.	7.59910	2.95558	0.34374E 01	0.7102000
20	10.25541	4.82894	0.	9.36159	3.9077	0.2795E 01	2.9705000
21	12.7814	4.82894	0.	11.62456	4.8596	0.2520E 01	9.962400
22	15.2926	4.82894	0.	14.14697	4.87496	0.25749E 01	9.942400
23	18.27717	4.82894	0.	16.91722	5.85115	0.25099E 01	5.5913000
24	21.45376	4.82894	0.	20.0232	6.17422	0.2463E 01	2.3814000
25	6.31252	6.76493	0.	6.84256	0.36095	0.79999E 01	0.0441900
26	8.51715	6.76493	0.	7.75706	3.2667	0.54445E 01	0.5144000
27	9.34994	6.76493	0.	9.27970	2.5547	0.39764E 01	0.6150000
28	11.70311	6.76493	0.	10.89007	3.54063	0.32779E 01	7.042200
29	13.36350	6.76493	0.	12.93769	4.42578	0.27051E 01	8.412100
30	16.25274	6.76493	0.	15.22493	4.42578	0.27291E 01	8.4612000
31	19.37337	6.76493	0.	17.73980	5.31094	0.2523E 01	5.0211800
32	21.96166	6.76493	0.	20.55890	5.60599	0.2524E 01	2.3021500
33	8.93316	8.70347	0.	8.77031	0.27034	0.80007E 01	0.0498200
34	10.26358	8.70347	0.	9.59195	2.91014	0.6169E 01	0.4931000
35	11.51401	8.70347	0.	10.96008	2.38334	0.4524E 01	0.651200
36	13.3776	8.70347	0.	12.39788	3.1048	0.35669E 01	8.1144000
37	15.17394	8.70347	0.	14.24659	3.16560	0.3164E 01	7.547100
38	17.22505	8.70347	0.	16.30070	3.97560	0.27154E 01	7.6435100
39	19.5628	8.70347	0.	18.56033	4.71073	0.2706E 01	4.5713000
40	22.25449	8.70347	0.	21.09364	5.03577	0.2524E 01	2.2348000
41	10.75334	10.63563	0.	10.69758	0.29773	0.8000E 01	0.0498000
42	12.2454	10.63563	0.	11.42640	2.5061	0.6704E 01	0.4425300
43	13.5164	10.63563	0.	12.6198	2.1526	0.5212E 01	0.6178500
44	15.37126	10.63563	0.	15.91532	2.92034	0.4101E 01	5.134000
45	18.37504	10.63563	0.	17.3771	3.5343	0.3497E 01	6.4567100
46	18.19713	10.63563	0.	17.3771	3.5343	0.3497E 01	6.4567100
47	20.36537	10.63563	0.	19.3816	4.2651	0.2759E 01	4.0351000
48	22.5672	10.63563	0.	21.6285	4.46534	0.2789E 01	2.1571100

49	13.57283	0.	0.	0.20918	0.40098	0.454300
50	13.57011	0.	0.	2.58108	0.51915	0.543360
51	14.74350	0.	0.	1.84515	0.57295	0.583380
52	16.30454	0.	0.	2.46020	0.46595	4.175700
53	17.32990	0.	0.	3.07525	0.38545	5.289200
54	19.18988	0.	0.	3.07525	0.34435	5.2469200
55	21.25103	0.	0.	3.69030	0.31638	3.4740000
56	23.29281	0.	0.	3.69030	0.23725	2.0433200
57	14.50356	0.	0.	0.17851	0.60000	0.0353300
58	15.53741	0.	0.	1.72155	0.75011	0.3802500
59	16.38429	0.	0.	1.97504	0.65725	0.5021900
60	17.43726	0.	0.	2.10004	0.55699	3.2064900
61	18.78189	0.	0.	2.62507	0.43715	4.0088000
62	20.14307	0.	0.	2.62507	0.38613	4.0088000
63	21.75533	0.	0.	3.15008	0.34607	2.8850100
64	23.42218	0.	0.	3.15008	0.31870	1.2415500
65	19.52519	0.	0.	0.62789	0.59000	0.0254800
66	17.22533	0.	0.	1.52202	0.73333	0.3074200
67	17.97668	0.	0.	1.30494	0.72613	0.4000100
68	18.88954	0.	0.	1.73991	0.62359	2.1000000
69	19.53391	0.	0.	2.17489	0.58664	2.6740800
70	21.11344	0.	0.	2.17489	0.43578	2.4716500
71	22.43102	0.	0.	2.50987	0.37043	2.7544300
72	23.37420	0.	0.	2.75486	0.28593	1.7545100
73	18.82134	0.	0.	0.31728	0.80000	0.0129500
74	19.36411	0.	0.	1.26249	0.79800	0.1395300
75	19.36411	0.	0.	1.03483	0.76370	0.1844200
76	20.29780	0.	0.	1.37977	0.70474	0.8137600
77	21.18408	0.	0.	1.72471	0.54812	1.0171900
78	22.07931	0.	0.	1.72471	0.35490	1.0171900
79	23.14453	0.	0.	2.06966	0.19902	1.1562700
80	24.22560	0.	0.	2.18464	0.12185	1.3167300

FIRST PANEL NUMBER ON MAIN WING = 1
 LAST PANEL NUMBER ON MAIN WING = 80
 X-COORDINATE OF FIXED POINT = 0.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR.

COORDINATES OF JOINT -LOADING POINTS AND LOADING POINT ASSIGNMENTS

I	XCG	YCG	LOADING
1	1.05758	0.35517	2
2	2.25072	0.35517	2
3	4.23728	0.35517	2
4	6.32527	0.35517	2
5	9.00982	0.35517	2
6	11.99245	0.35517	2
7	15.27377	0.35517	3
8	18.95240	0.35517	3
9	2.08612	2.39260	2
10	4.08137	2.39260	2
11	5.91828	2.39260	2
12	7.84370	2.39260	2
13	10.31925	2.39260	3
14	13.06937	2.39260	3
15	16.09554	2.39260	4
16	19.48796	2.39260	4
17	4.91447	4.32334	2
18	5.92183	4.32334	2
19	7.35910	4.32334	3
20	9.36199	4.32334	3
21	11.62854	4.32334	4
22	14.14497	4.32334	4
23	16.91722	4.32334	5
24	20.23227	4.32334	5
25	6.44256	6.76493	3
26	7.75706	6.76493	4
27	9.27670	6.76493	4
28	10.98007	6.76493	4
29	12.93769	6.76493	5
30	15.22393	6.76493	5
31	17.73890	6.76493	6
32	20.55890	6.76493	7
33	8.77031	8.70347	5
34	9.15919	8.70347	5
35	10.96000	8.70347	5
36	12.39788	8.70347	5
37	14.24658	8.70347	6
38	16.50070	8.70347	6
39	18.95602	8.70347	7
40	21.09364	8.70347	7
41	10.69758	10.53563	6
42	11.42640	10.53563	6
43	12.63998	10.53563	6
44	13.91532	10.53563	6
45	15.55516	10.53563	7
46	17.37721	10.53563	7
47	19.386146	10.53563	8
48	21.42845	10.53563	8
49	12.62416	12.37311	7
50	13.26020	12.37311	7
51	14.31918	12.37311	7
52	15.43222	12.37311	7
53	16.66528	12.37311	8
54	18.45333	12.37311	8
55	20.20240	12.37311	8
56	22.16347	12.37311	9

57	14.94974	14.30356	8
58	15.09302	14.50356	8
59	15.99728	14.50356	8
60	16.94731	14.50356	8
61	18.17359	14.50356	9
62	19.52868	14.50356	9
63	21.02290	14.50356	9
64	22.69801	14.50356	10
65	14.47163	16.43333	9
66	15.92475	16.43333	9
67	17.47452	16.43333	9
68	19.16309	16.43333	9
69	19.47897	16.43333	10
70	20.60350	16.43333	10
71	21.84269	16.43333	10
72	23.23208	16.43333	10
73	18.39424	18.36411	10
74	19.75264	18.36411	10
75	19.34886	18.36411	10
76	19.97552	18.36411	10
77	20.78122	18.36411	10
78	21.67645	18.36411	10
79	22.66123	18.36411	10
80	23.78552	18.36411	10

NUMBER OF ELASTIC AXIS POINTS ON MAIN WING *10

COORDINATES OF ELASTIC AXIS SEGMENTS

I	XEA	YEA
1	19.167170	0.
2	11.65270	1.58000
3	12.84270	3.93000
4	13.84270	5.78000
5	14.90270	7.59000
6	16.04270	9.40000
7	17.37270	11.43000
8	18.76270	13.57000
9	20.18270	15.57000
10	21.58270	17.95000

ELASTIC AXIS TORSIONA. AND BENDING STIFFNESS

I	EI	KGJ
1	0.9931E 03	0.9472E 09
2	0.7986E 03	0.6375E 09
3	0.5496E 03	0.4444E 09
4	0.3681E 03	0.2778E 09
5	0.2431E 03	0.1844E 09
6	0.1522E 03	0.1250E 09
7	0.7432E 07	0.6250E 07
8	0.3171E 07	0.2709E 07
9	0.1350E 07	0.1111E 07

ELASTIC DERIVATIVES FOR MACH NUMBER 1.50.

WEIGHTS 43000.
 SMO 0.00237903
 VELCC17A 3.16753E 04 S.O.S. 1116.890 ALTITUDE 0.
 DYNAMIC PRESSURE 0.33372E 04
 PLTBN 3.2339.

CLALP# 0.20432E 01
 CHALP# 0.12973E 01
 CLCE# 0.19200E 01
 CMCE# 0.16587E 01
 CLCI 0.10921E 02
 CMCI 0.25712E 02
 CLDI 0.11335E 03
 CMDI 0.17458E 04
 CLTDI 0.22955E 02
 CMTDI 0.19225E 02
 DCLDN 0.15650E 02
 DCUDN 0.10457E 02
 CLALP# 0.17735E 01
 CHALP# 0.10719E 01

PANEL NUMBER	PHENATE	CP(F)
1	-0.52732E-01	0.69744E 01
2	-0.52732E-01	0.29210E 01
3	-0.52732E-01	0.24118E 01
4	-0.52732E-01	0.23761E 01
5	-0.52732E-01	0.21922E 01
6	-0.52732E-01	0.19056E 01
7	-0.17414E 00	0.13588E 01
8	-0.17414E 00	0.11277E 01
9	-0.52732E-01	0.74537E 01
10	-0.52732E-01	0.36917E 01
11	-0.52732E-01	0.27945E 01
12	-0.52732E-01	0.24049E 01
13	-0.17414E 00	0.19991E 01
14	-0.17414E 00	0.18610E 01
15	-0.25442E 00	0.13504E 01
16	-0.25442E 00	0.12266E 01
17	-0.52732E-01	0.75763E 01
18	-0.52732E-01	0.44717E 01
19	-0.17414E 00	0.27786E 01
20	-0.17414E 00	0.24402E 01
21	-0.25442E 00	0.18957E 01
22	-0.25442E 00	0.18366E 01
23	-0.33737E 00	0.13103E 01
24	-0.33737E 00	0.11152E 01
25	-0.17414E 00	0.66374E 01
26	-0.25442E 00	0.45950E 01
27	-0.25442E 00	0.32207E 01
28	-0.25442E 00	0.25964E 01
29	-0.33737E 00	0.18943E 01
30	-0.33737E 00	0.17008E 01
31	-0.45040E 00	0.12311E 01
32	-0.59953E 00	0.77673E 00
33	-0.33737E 00	0.51622E 01
34	-0.33737E 00	0.47008E 01
35	-0.33737E 00	0.35353E 01

36	-0.35757E 00	0.27226E 01
37	-0.43949E 00	0.14877E 01
38	-0.45949E 00	0.16944E 01
39	-0.33903E 00	0.10802E 01
40	-0.53975E 00	0.93197E 00
41	-0.45949E 00	0.43261E 01
42	-0.43949E 00	0.45880E 01
43	-0.45949E 00	0.37463E 01
44	-0.45949E 00	0.28760E 01
45	-0.33903E 00	0.18039E 01
46	-0.35903E 00	0.15930E 01
47	-0.72758E 00	0.96465E 00
48	-0.72758E 00	0.26467E 00
49	-0.59975E 00	0.32974E 01
50	-0.53903E 00	0.41404E 01
51	-0.59975E 00	0.38231E 01
52	-0.59975E 00	0.28130E 01
53	-0.72758E 00	0.17258E 01
54	-0.72758E 00	0.15426E 01
55	-0.72758E 00	0.12422E 01
56	-0.83371E 00	0.78759E 00
57	-0.72748E 00	0.21794E 01
58	-0.72758E 00	0.33421E 01
59	-0.72758E 00	0.36500E 01
60	-0.72758E 00	0.30629E 01
61	-0.83371E 00	0.18105E 01
62	-0.83371E 00	0.15469E 01
63	-0.83371E 00	0.13894E 01
64	-0.83371E 00	0.9943E 00
65	-0.83371E 00	0.83303E 01
66	-0.83371E 00	0.2453E 01
67	-0.83371E 00	0.33596E 01
68	-0.83371E 00	0.34461E 01
69	-0.83371E 00	0.25990E 01
70	-0.83371E 00	0.17063E 01
71	-0.87113E 00	0.14772E 01
72	-0.87113E 00	0.11382E 01
73	-0.87113E 00	0.10310E 01
74	-0.87113E 00	0.17008E 01
75	-0.87113E 00	0.23751E 01
76	-0.87113E 00	0.29215E 01
77	-0.87113E 00	0.26461E 01
78	-0.87113E 00	0.18784E 01
79	-0.87113E 00	0.98268E 00
80	-0.87113E 00	0.51049E 00

SECTIONAL COEFFICIENT FOR WING

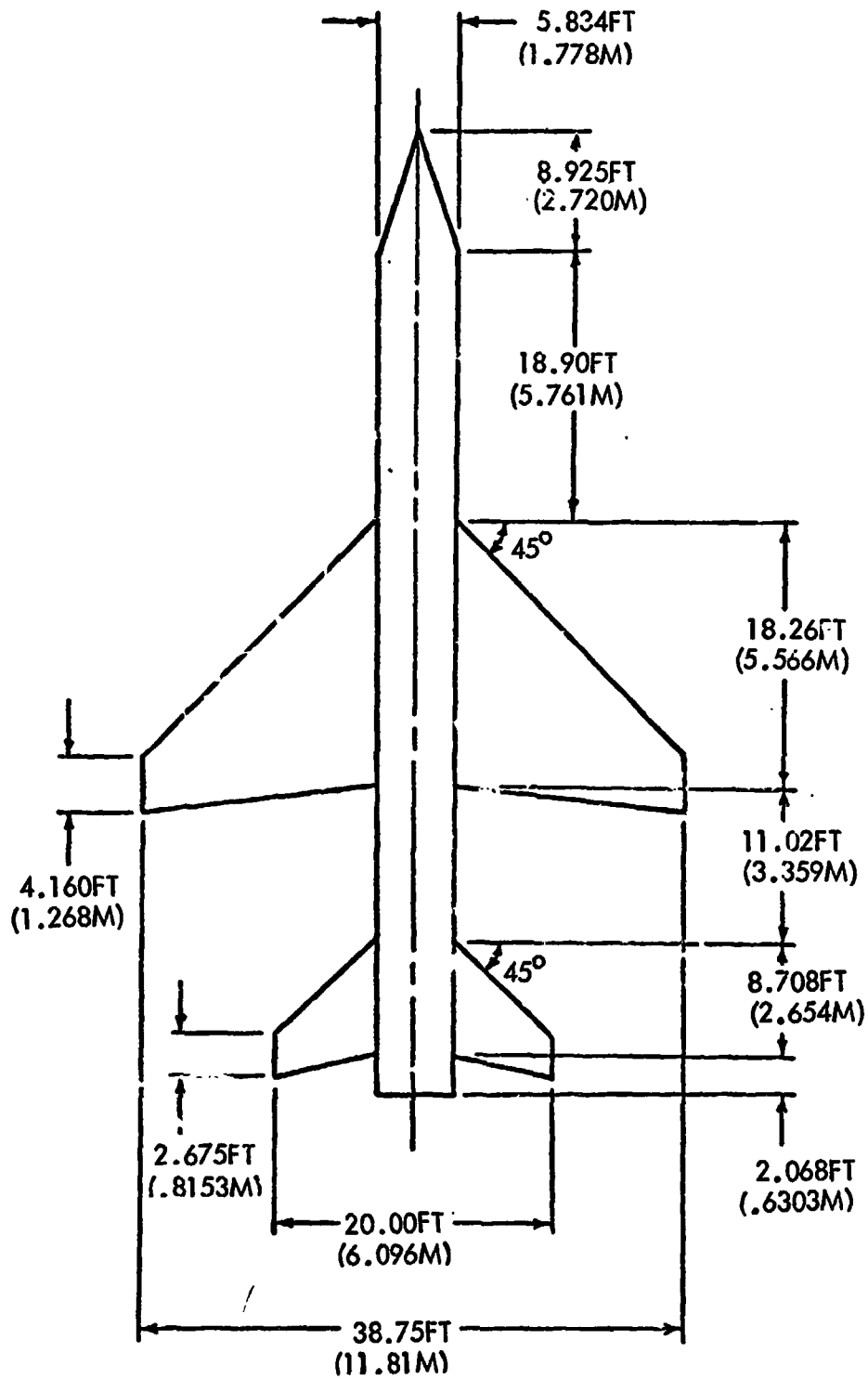
0.04935	1.81491	GLI	0.50760	CT	0.457638
0.14930	1.75593	1.97826	0.48835	0.	0.56728
0.24923	1.63792	2.06393	0.45835	0.	0.53532
0.34915	1.40372	2.11576	0.41177	0.	0.44627
0.44906	1.21892	2.09374	0.37354	0.	0.38751
0.54894	0.95574	2.11400	0.32687	0.	0.30703
0.64878	0.70391	2.08552	0.27927	0.	0.22375
0.74857	0.45114	2.04177	0.23678	0.	0.14152
0.84828	0.20274	2.02664	0.19449	0.	0.09356
0.94782	0.20453	2.01111	0.13172	0.	0.07008
		1.71044			

TOTAL LEADING EDGE THRUST COEFFICIENT= 0.
TOTAL INDUSED. DRAG COEFFICIENT= 0.12549E 01
CP/(CL*CL)= 0.37896F 00

THIS CASE IS COMPLETE

7. TEST CASE 2

This test case deals with a complete elastic wing, body and horizontal tail configuration. Figure 3 defines the overall geometry for this case. Figure 4 defines the elastic axis location. Input data cards are listed in Table 5. Output data listing for this case is given in Table 6.



SCALE: 1CM = 5FT

Figure 3. Test Case 2 Platform.

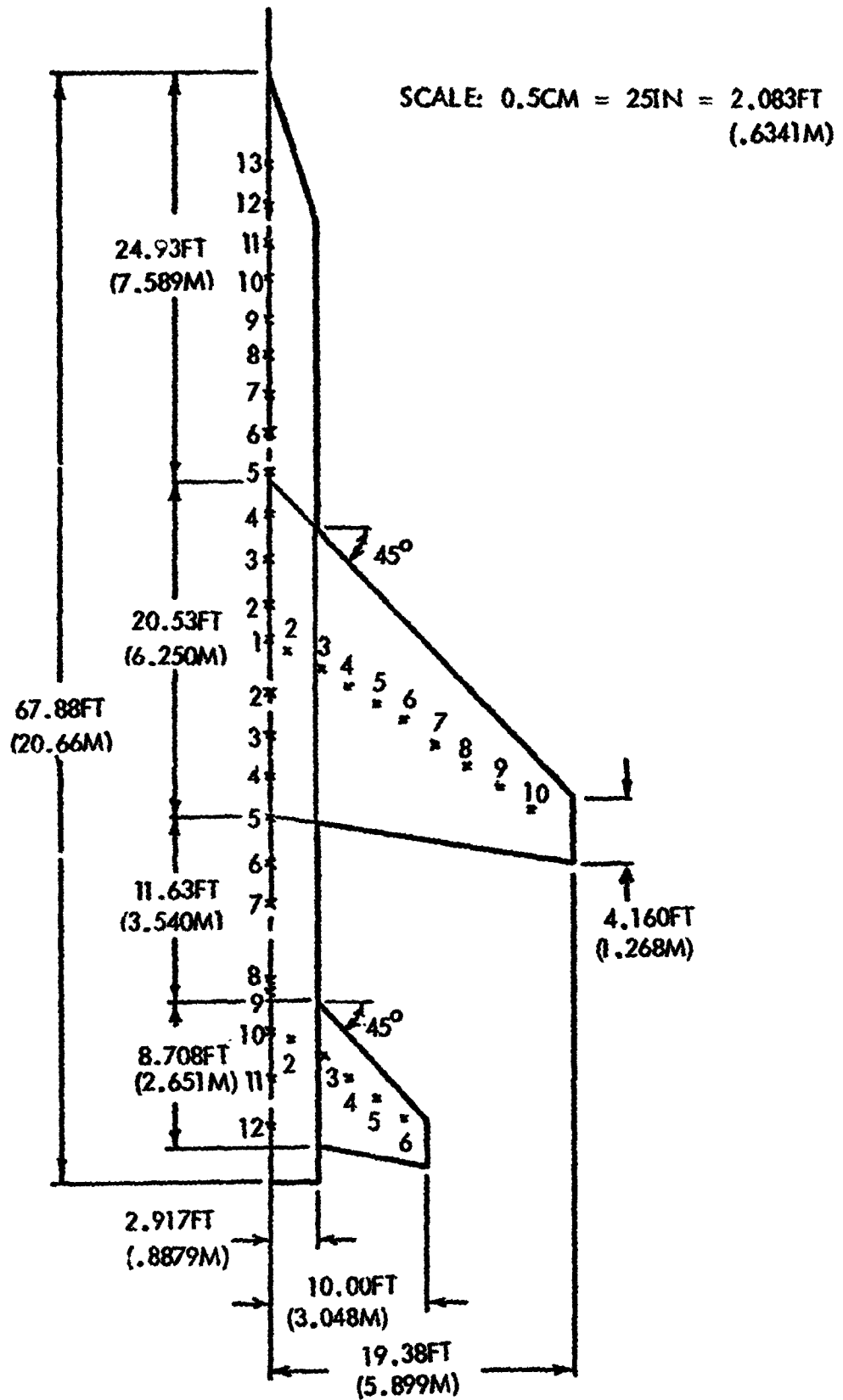


Figure 4. Elastic Axis End Points for Test Case 2.

Table 5. Listing of Input Data Cards for Test Case 2

Card	TEST CASE -2
0	
1	128013000
2	00
3	100907
4	03
5	0201
6	0.
7	0.
7	44.444444
7	88.888889
8	0.
5	1102
6	27.825
7	0.
7	100.
8	0.
8	77.7211
5	0603
6	57.10417
7	0.
8	0.
9	500.11719
11	1.5
12	2.5
12	127.05
12	24.8
12	5.67917
12	5.33442
12	4.99498
12	4.62752
	67.87917
	5.555556
	50.
	94.444444
	100.
	46.08333
	1.0203
	8.8607
	88.8603
	65.8125
	5.613
	20.
	14.455
	10.79
	104.94
	10.89
	2.09387
	2.06369
	2.03753
	2.00333
	0.
	11.11111
	55.55556
	61.11111
	66.66667
	8.925
	10.66667
	22.22222
	27.77778
	72.22222
	67.87917
	2.91667
	2.91667
	19.375
	48.
	44.3035
	55.4427
	66.5819
	44.47917
	33.
	48.63917
	19.375
	48.
	44.3035
	55.4427
	66.5819
	64.34583
	30.
	60.
	67.02083
	50.
	80.
	20.522
	39.27
	0.48989
	0.44807
	0.43858
	0.42626
	0.41102
	18.954
	45.045
	0.04547
	0.04439
	0.04345
	0.04223
	0.04072
	22.05
	40.96
	0.64702
	0.63166
	0.61836
	0.60095
	0.57945
	33.415
	38.75
	8.48499
	7.84316
	7.20557
	6.52464
	6.60738
	62.484
	37.785
	10.60619
	9.80390
	9.00692
	8.1577
	7.27224
	94.720
	34.3
	10.60619
	9.80390
	9.00692
	8.1577
	7.27224

Table 5 (Continued) Listing of Input Data Cards for Test Case 2

12	4.24075	1.96107	0.05094	0.51418	0.72492	6.62124	8.27650	8.27650
12	4.86817	2.24699	0.04704	0.47481	0.66937	5.36289	6.74866	6.74866
12	4.17083	2.1378	0.04209	0.42485	0.59891	4.14585	5.18227	5.18227
12	3.43494	1.99931	0.03447	0.34793	0.49051	2.81425	3.51777	3.51777
12	2.60095	1.78626	0.01866	0.18335	0.26558	1.17233	1.46540	1.46540
12	1.43098	1.34418	0.19152	0.32024	1.16015	1.70609	2.04489	2.11749
12	0.17771	0.29715	1.07648	1.58306	1.90709	2.02521	0.16058	0.26866
12	0.97330	1.43131	1.73713	1.91140	0.13581	0.22709	0.82270	1.20965
12	1.48909	1.74530	0.07811	0.120610	0.47317	0.69583	0.91339	1.35979
13	0.09093	0.03000	0.1000					
14	1.31200	0.90706	0.40302	0.20202	0.20202	0.30402	0.20202	0.20202
14	0.50303	0.40506	0.60404	0.50606	0.70708	0.80606	0.70708	0.80606
14	0.91008	0.80909	1.01010	1.00202	0.30303	0.30303	0.40404	0.40404
14	0.50505	0.50506						
15	8.33333	4.16667	2.91667	2.91667	35.609			
17	0.113							
18	35.609	0.	33.3333	0.	30.4167	0.	27.6042	0.
18	25.	0.	22.5	0.	20.	0.	17.5	0.
18	15.4167	0.	12.7083	0.	10.4167	0.	8.125	0.
18	5.4167	0.						
19	2.8512	E011	E	2.4192	E011	E		
19	2.00	E011	E	1.656	E011	E		
19	1.3824	E011	E	1.0732	E011	E		
19	8.928	E010	E	7.2	E010	E		
19	5.348	E010	E	3.744	E010	E		
19	2.88	E010	E	1.728	E010	E		
17	0.212							
18	35.609	0.	38.95	0.	41.75	0.	44.375	0.
18	47.0833	0.	49.7916	0.	52.5	0.	57.2917	0.
18	57.7083	0.	60.625	0.	63.5417	0.	66.4553	0.

Table 5 (Continued) Listing of Input Data Cards for Test Case 2

19	3.168	E011	E	3.168	E011	E		
19	3.1392	E011	E	2.9952	E011	E		
19	2.2752	E011	E	1.6416	E011	E		
19	1.152	E011	E	8.064	E010	E		
19	5.472	E010	E	2.304	E010	E		
19	2.8	E009	E					
17	0310							
18	35.609	0.		36.59	37.78	3.93	38.78	5.78
18	39.84	7.59		40.98	42.31	11.43	43.70	13.67
18	45.12	15.67		46.52				
19	1.43	E0101.22		17.95	E0109.9	E009		
19	7.9	E0096.4		E0101.15	E0094.0	E009		
19	3.5	E0092.8		E0095.3	E0091.8	E003		
19	1.1	E0099.0		E0092.2	E0083.9	E008		
19	1.8	E0081.6		E0084.6				
17	0406			E008				
18	60.625	0.		61.25	62.57	3.72	63.63	5.51
18	64.84	7.29		65.89				
19	4.5	E0093.9		9.07	E0092.7	E009		
19	2.0	E0091.4		E0093.4	E0097.5	E008		
19	5.0	E0083.5		E0091.0				
20				E008				
21	76000.	1.						
22	0.002378	1116.89	0.					

Table 6. Output for Test Case 2
TEST CASE 2

```

.....
6 350 ERY DATA IS DIVIDED IN TO 3 TESTIONS .
.....

DEFINITION OF SECTION 1
.....
X-LEADING EDGE      V-TRAILING EDGE      V-LEADING EDGE      Z
8.92500             47.87917             0.00000             0.00000
THERE ARE 19 CONSTANT PERCENT STRENGTH LINES AT 2.91667
THERE ARE 9 CONSTANT PERCENT STRENGTH LINES AT 22.222
THERE ARE 2 CONSTANT PERCENT STRENGTH LINES AT 24.444
THERE ARE 2 CONSTANT PERCENT STRENGTH LINES AT 100.000
66.667             77.778             38.689             50.000
THERE ARE 44.444             55.556             61.111

DEFINITION OF SECTION 2
.....
X-LEADING EDGE      V-TRAILING EDGE      V-LEADING EDGE      Z
27.22200           46.08333             2.91667             0.00000
THERE ARE 9 CONSTANT PERCENT STRENGTH LINES AT 19.37500
THERE ARE 11 CONSTANT PERCENT STRENGTH LINES AT 46.000
THERE ARE 11 CONSTANT PERCENT STRENGTH LINES AT 55.443
THERE ARE 17.722             25.542             44.304             55.443
THERE ARE 77.721             89.960             100.000

DEFINITION OF SECTION 3
.....
X-LEADING EDGE      V-TRAILING EDGE      V-LEADING EDGE      Z
57.10437           45.01247             2.91667             0.00000
THERE ARE 7 CONSTANT PERCENT STRENGTH LINES AT 12.70000
THERE ARE 4 CONSTANT PERCENT STRENGTH LINES AT 50.000
THERE ARE 4 CONSTANT PERCENT STRENGTH LINES AT 100.000
REF. AREA = 0.50000
REF. CHORD = 0.14456
CALPR = 0.58346
CALPR = 0.11000
CL3 = 0.22300
CL3 = 0.17000

```

SECTIONAL C_D/C_{DREF} FOR WING

y	C_D/C_{DREF}	C_T	C_{DREF}	C_T	C_D/C_{DREF}
0.13773	2.5674	0.17614	2.5332	0.31722	0.17209
0.25294	2.17519	0.21721	2.49319	0.51013	0.18024
0.31129	3.13375	2.21721	3.13375	0.50523	0.24464
0.41141	3.17672	2.32720	3.13472	0.53626	0.21029
0.48053	3.37510	2.42547	3.17437	0.53613	0.21708
0.57909	3.97713	2.47947	3.97713	0.55623	0.21750
0.60753	4.37716	2.22558	4.37716	0.51759	0.23398
0.75191	4.70622	2.42547	4.70622	0.50073	0.31554
0.95319	5.27708	2.22558	5.27708	0.44656	0.34857
0.99319	5.07923	2.22558	5.12923	0.32356	0.33162

SECTIONAL C_D/C_{DREF} FOR HORIZONTAL TAIL

y	C_D/C_{DREF}	C_T	C_{DREF}	C_T	C_D/C_{DREF}
0.36074	2.17614	0.17614	2.17614	0.44182	0.14349
0.52211	2.21721	0.21721	2.21721	0.32691	0.14754
0.44333	2.32720	0.23270	2.32720	0.33230	0.15343
0.78432	2.42547	0.24257	2.42547	0.27396	0.14012
0.92482	2.22558	0.22258	2.22558	0.13447	0.14674

TOTAL LEADING EDGE TRUST COEFFICIENTS C_L
 TOTAL INDUCED DRAG COEFFICIENTS C_{Di}
 C_D/C_{DREF} 0.25677E 01

YAC4 NUMBERS 1.50

CP VALUES ARE FOR ALPHA 1.303000 RADIAN

PAVEL NUMBER	YCP	YPO	ZCP	YCT	AREA	CP	WARS
1	7.71334	1.42413	0.	6.12231	13.27585	0.20071= 71	2.5000000
2	11.23731	1.42413	0.	9.656127	13.27585	0.31042= 71	10.7200000
3	14.76927	1.42413	0.	13.18074	13.27585	0.57315= 70	19.0340000
4	19.29223	1.42413	0.	16.70927	13.27585	0.25210= 70	27.5220000
5	21.82421	1.42413	0.	20.23816	13.27585	0.11004= 70	22.0300000
6	25.35516	1.42413	0.	23.76713	13.27585	0.11114= 70	37.4150000
7	29.88612	1.42413	0.	27.29609	13.27585	0.32670= 70	52.4340000
8	32.41317	1.42413	0.	30.82505	13.27585	0.12516= 71	54.7200000
9	35.94203	1.42413	0.	34.35402	13.27585	0.18722= 71	27.0370000
10	39.47079	1.42413	0.	37.88298	13.27585	0.22374= 71	34.9300000
11	43.00000	1.42413	0.	41.41194	13.27585	0.23012= 71	39.2700000
12	46.52874	1.42413	0.	44.94091	13.27585	0.17116= 71	40.9500000
13	50.05791	1.42413	0.	48.46987	13.27585	0.47018= 70	38.7200000
14	53.58647	1.42413	0.	51.99883	13.27585	0.78512= 71	37.7300000
15	57.11443	1.42413	0.	55.52780	13.27585	0.64567= 70	34.1700000
16	60.64240	1.42413	0.	59.05676	13.27585	0.12537= 71	24.8000000
17	64.17037	1.42413	0.	62.58572	13.27585	0.11335= 71	18.4200000
18	67.69834	1.42413	0.	66.11469	13.27585	0.17424= 70	0.0450000
19	71.22631	1.42413	0.	69.64365	13.27585	0.46433= 71	0.4800000
20	74.75428	1.42413	0.	73.17262	13.27585	0.25311= 71	0.6470000
21	78.28225	1.42413	0.	76.70159	13.27585	0.20925= 71	8.4300000
22	81.81022	1.42413	0.	80.23056	13.27585	0.21132= 71	10.6030000
23	85.33819	1.42413	0.	83.75953	13.27585	0.22024= 71	10.6030000
24	88.86616	1.42413	0.	87.28850	13.27585	0.22735= 71	5.6720000
25	92.39413	1.42413	0.	90.81747	13.27585	0.23335= 71	2.0340000
26	95.92210	1.42413	0.	94.34644	13.27585	0.12714= 72	0.0440000
27	99.45007	1.42413	0.	97.87541	13.27585	0.53670= 71	0.4130000
28	102.97804	1.42413	0.	101.40438	13.27585	0.32118= 71	7.8310000
29	106.50601	1.42413	0.	104.93335	13.27585	0.23212= 71	0.8130000
30	110.03398	1.42413	0.	108.46232	13.27585	0.27362= 71	5.1340000
31	113.56195	1.42413	0.	111.99129	13.27585	0.23872= 71	2.0530000
32	117.08992	1.42413	0.	115.52026	13.27585	0.17572= 72	0.2830000
33	120.61789	1.42413	0.	119.04923	13.27585	0.50613= 71	0.4380000
34	124.14586	1.42413	0.	122.57820	13.27585	0.37733= 71	0.6160000
35	127.67383	1.42413	0.	126.10717	13.27585	0.20860= 71	7.2250000
36	131.20180	1.42413	0.	129.63614	13.27585	0.25270= 71	9.0490000
37	134.72977	1.42413	0.	133.16511	13.27585	0.24614= 71	9.0340000
38	138.25774	1.42413	0.	136.69408	13.27585	0.24624= 71	4.9340000
39	141.78571	1.42413	0.	140.22305	13.27585	0.24412= 71	2.3350000
40	145.31368	1.42413	0.	143.75202	13.27585	0.96670= 71	0.0420000
41	148.84165	1.42413	0.	147.28099	13.27585	0.64531= 71	0.4260000
42	152.36962	1.42413	0.	150.80996	13.27585	0.43971= 71	0.6300000
43	155.89759	1.42413	0.	154.33893	13.27585	0.32613= 71	0.6300000
44	159.42556	1.42413	0.	157.86790	13.27585	0.27623= 71	8.1550000
45	162.95353	1.42413	0.	161.39687	13.27585	0.26334= 71	8.1550000
46	166.48150	1.42413	0.	164.92584	13.27585		
47	170.00947	1.42413	0.	168.45481	13.27585		
48	173.53744	1.42413	0.	171.98378	13.27585		

49	44.11207	8.71237	0.	42.30333	1.64507	0.25512	71	4.6273260
50	46.74223	8.70287	0.	45.35419	1.64754	0.25049	71	2.0333600
51	33.75757	9.44711	0.	34.51701	2.18303	0.62777	71	0.3137200
52	35.21153	9.44711	0.	35.27674	2.02341	0.66659	71	0.4110000
53	37.35251	9.44711	0.	36.54017	1.75359	0.42538	71	0.5724500
54	39.55177	9.44711	0.	37.84312	2.71144	0.37045	71	6.6272300
55	42.42127	9.44711	0.	39.47449	2.76430	0.35045	71	7.2722400
56	45.32525	9.44711	0.	41.47247	2.74430	0.27930	71	7.2722400
57	48.30177	9.44711	0.	43.57945	3.51714	0.26743	71	4.2847600
58	45.28141	0.44711	0.	45.99308	3.50145	0.24002	71	1.9510700
59	36.21034	11.11358	0.	35.16669	2.21001	0.90174	71	0.6506400
60	37.59735	11.11358	0.	36.84142	2.25904	0.75212	71	0.5148000
61	39.42123	11.11358	0.	37.94401	1.75244	0.54546	71	0.7249200
62	37.75232	11.11358	0.	39.14557	2.46294	0.41749	71	6.6212400
63	41.42275	11.11358	0.	40.64370	3.06743	0.33042	71	0.2745000
64	43.10254	11.11358	0.	42.35056	3.08743	0.29042	71	0.2745000
65	45.11445	11.11358	0.	44.20599	3.70491	0.28412	71	4.3581700
66	47.24743	11.11358	0.	46.20604	3.71074	0.27171	71	2.2460000
67	39.75175	12.01332	0.	39.01132	2.16063	0.80672	71	0.4170000
68	39.76317	12.01332	0.	39.59180	1.24382	0.80872	71	0.4248000
69	37.44276	12.01332	0.	39.25740	1.39334	0.64302	71	0.4533700
70	41.73652	12.01332	0.	40.27328	2.12444	0.48224	71	5.8520000
71	42.23374	12.01332	0.	41.48030	2.55556	0.38512	71	6.7484500
72	43.26544	12.01332	0.	43.32218	2.58555	0.33512	71	6.7106600
73	45.11293	12.01332	0.	44.92904	3.18667	0.31702	71	4.1708300
74	47.94521	12.01332	0.	46.71945	3.16171	0.27202	71	2.1578000
75	39.62228	14.74193	0.	39.45219	2.13124	0.87614	71	0.6420000
76	42.74227	14.74193	0.	40.33229	1.62720	0.83422	71	0.2405000
77	41.47311	14.74193	0.	41.14962	1.33421	0.73322	71	0.3901000
78	42.43734	14.74193	0.	42.00134	1.77894	0.57412	71	4.1185800
79	43.44194	14.74193	0.	43.02640	2.22162	0.44522	71	5.3227000
80	44.56167	14.74193	0.	44.31114	2.22167	0.30472	71	5.1872000
81	45.80352	14.74193	0.	45.85155	2.46443	0.33612	71	3.4345000
82	47.34574	14.74193	0.	47.31220	2.11667	0.33022	71	3.2903000
83	41.72253	14.74193	0.	41.67251	1.12103	0.84572	71	0.6344700
84	42.46264	14.74193	0.	42.31515	1.31158	0.85112	71	0.3975000
85	43.74224	16.09311	0.	42.71941	1.37507	0.80622	71	0.4251000
86	43.74143	16.09311	0.	43.42698	1.43145	0.53322	71	2.8142500
87	44.25271	16.09311	0.	44.31076	1.73182	0.53112	71	3.5177700
88	45.31177	16.09311	0.	45.27215	1.79182	0.44712	71	3.3177700
89	46.71344	16.09311	0.	46.37315	2.15019	0.30472	71	2.6315500
90	48.14417	16.09311	0.	47.51140	2.26264	0.27952	71	1.7362500
91	43.35062	18.41227	0.	43.52750	1.19221	0.86412	71	0.6106500
92	44.27354	18.41227	0.	43.92711	1.29549	0.85952	71	6.1393500
93	44.27225	18.41227	0.	44.32529	1.91503	0.84322	71	6.2545000
94	45.11312	18.41227	0.	44.84800	1.70809	0.76472	71	1.1723300
95	45.25974	18.41227	0.	45.22121	1.16000	0.61272	71	1.1554000
96	45.60573	18.41227	0.	45.27314	1.36000	0.44402	71	1.4554000
97	47.45623	18.41227	0.	47.07297	1.53200	0.24402	71	1.4308000
98	43.44001	18.41227	0.	48.01553	1.72267	0.12742	71	1.3441000
99	59.74433	3.61743	0.	58.31825	1.64443	0.62252	71	0.1315200
100	59.39123	3.61743	0.	59.61725	1.07782	0.43652	71	0.4202500
101	67.14544	3.61743	0.	59.63746	1.07231	0.23312	71	1.1571500
102	61.78217	3.61743	0.	62.29641	2.29641	0.14832	71	1.2340000
103	61.79024	3.61743	0.	62.86335	2.87032	0.12302	71	2.0446000
104	65.92384	3.61743	0.	64.91534	2.37052	0.11842	71	2.1174000
105	59.62434	5.02102	0.	59.44965	0.77459	0.77459	71	0.2771000
106	67.26244	5.02102	0.	59.94615	1.91234	0.47012	71	0.2371500
107	61.27844	5.02102	0.	60.81144	1.46589	0.26224	71	1.3744000
108	62.44435	5.02102	0.	62.02192	1.95493	0.11312	71	1.5330600

109	64.35035	5.02102	0.	43.57801	2.44314	0.124327	11	1.9370900
110	65.04598	5.02102	0.	65.30699	2.44314	0.113762	11	2.7252100
111	61.03403	6.43331	0.	60.84375	3.45252	0.648342	11	1.5564000
112	61.92258	6.43331	0.	61.24122	3.74089	0.505367	11	1.5584400
113	62.37144	6.43331	0.	61.98883	1.20749	0.706498	11	0.9743000
114	63.45377	6.43331	0.	62.97441	1.41244	0.122792	11	1.4513100
115	64.21274	6.43331	0.	64.27103	2.11580	0.146702	11	1.3321300
116	65.14394	6.43331	0.	65.69027	2.01580	0.114122	11	1.9114400
117	62.36144	7.84324	0.	62.26749	3.35564	0.415302	11	0.1368100
118	62.76649	7.84324	0.	62.50589	3.59543	0.521351	11	0.2277300
119	63.46264	7.84324	0.	63.15007	3.35104	0.359422	11	0.8227000
120	64.35177	7.84324	0.	63.94148	1.27073	0.223772	11	1.2387500
121	65.46551	7.84324	0.	64.94589	1.58844	0.157352	11	1.4370600
122	64.59351	7.84324	0.	66.08891	1.58844	0.121142	11	1.7483100
123	63.25402	9.24821	0.	63.67028	3.21683	0.311172	11	0.0231100
124	64.25094	9.24821	0.	63.91894	3.43595	0.418732	11	0.1361000
125	64.34591	9.24821	0.	64.32316	3.59565	0.402242	11	0.4731700
126	63.20174	9.24821	0.	64.90338	3.29885	0.287382	11	0.6251300
127	66.02231	9.24821	0.	65.64833	1.16108	0.142162	11	0.9132000
128	66.35114	9.24821	0.	66.47817	1.16109	0.549322	11	1.3397900

FIRST PANEL NUMBER ON FRONT FUSELAGE = 1
 LAST PANEL NUMBER ON FRONT FUSELAGE = 9
 FIRST PANEL NUMBER ON REAR FUSELAGE = 10
 LAST PANEL NUMBER ON REAR FUSELAGE = 19
 FIRST PANEL NUMBER ON MAIN WING = 12
 LAST PANEL NUMBER ON MAIN WING = 93
 FIRST PANEL NUMBER ON HORIZONTAL TAIL = 99
 LAST PANEL NUMBER ON HORIZONTAL TAIL = 129
 STRUCTURAL CHORD FOR MAIN WING = 6.33333
 STRUCTURAL CHORD FOR HORIZONTAL TAIL = 4.15667
 HALF THE WIDTH OF FUSELAGE AT ROOT CHORD OF THE MAINWING = 3.91667
 HALF THE WIDTH OF FUSELAGE AT ROOT CHORD OF THE HORIZONTAL TAIL = 3.91667
 X-COORDINATE OF FIXED POINTS = 35.50900

COORDINATES OF MILITARY LOADING POINTS AND LOADING POINT ASSIGNMENTS

I	YCG	YCG	IASIGN
1	5.12331	1.42413	13
2	9.65127	1.42413	12
3	13.1824	1.42413	10
4	16.7022	1.42413	9
5	20.2316	1.42413	7
6	23.7613	1.42413	6
7	27.2909	1.42413	4
8	30.8205	1.42413	3
9	34.3502	1.42413	2
10	37.8798	1.42413	2
11	41.4094	1.42413	3
12	44.9391	1.42413	5
13	48.4687	1.42413	5
14	51.9983	1.42413	7
15	55.5279	1.42413	7
16	59.0575	1.42413	8
17	62.5872	1.42413	10
18	66.1168	1.42413	11
19	69.6464	1.42413	12
20	73.1760	3.53722	2
21	76.7056	3.53722	2
22	80.2352	3.53722	2
23	83.7648	3.53722	2
24	87.2944	3.53722	2
25	90.8240	3.53722	3
26	94.3536	3.53722	4
27	97.8832	5.0469	2
28	101.4128	5.0469	2
29	104.9424	5.0469	2
30	108.4720	5.0469	2
31	112.0016	5.0469	3
32	115.5312	5.0469	3
33	119.0608	5.0469	4
34	122.5904	5.0469	4
35	126.1200	6.52245	2
36	129.6496	6.52245	2
37	133.1792	6.52245	3
38	136.7088	6.52245	3
39	140.2384	6.52245	4
40	143.7680	6.52245	4
41	147.2976	6.52245	5
42	150.8272	6.52245	5
43	154.3568	8.00767	3
44	157.8864	8.00767	3
45	161.4160	8.00767	3
46	164.9456	8.00767	4
47	168.4752	8.00767	4
48	172.0048	8.00767	5
49	175.5344	8.00767	5
50	179.0640	8.00767	5
51	182.5936	9.46711	4
52	186.1232	9.46711	4
53	189.6528	9.46711	5
54	193.1824	9.46711	5
55	196.7120	9.46711	6
56	200.2416	9.46711	6

57	43.55335	9.46711	7
58	45.99708	9.46711	7
59	35.12459	11.1359	5
60	36.54142	11.1359	5
61	37.96981	11.1359	6
62	39.14557	11.1359	6
63	40.2817	11.10359	7
64	42.3515	11.10359	7
65	44.26399	11.1359	8
66	44.28139	11.1359	8
67	39.0132	12.93343	6
68	39.5910	12.93343	6
69	39.5578	12.93343	7
70	40.57199	12.93343	7
71	41.9845	12.93343	8
72	43.33218	12.93343	8
73	44.9204	12.93343	8
74	46.7145	12.93343	9
75	39.63259	14.76193	7
76	41.14352	14.76193	7
77	42.00134	14.76193	8
78	43.5914	14.76193	8
79	43.5914	14.76193	9
80	44.31114	14.76193	9
81	45.55155	14.76193	9
82	47.1522	14.76193	10
83	41.62251	15.26911	8
84	42.09335	15.26911	8
85	42.73141	16.58911	9
86	43.42159	16.58911	9
87	44.31176	16.58911	10
88	45.29295	16.58911	10
89	46.37115	16.58911	10
90	47.5814	16.58911	10
91	43.52177	18.40977	9
92	43.82211	18.40977	9
93	44.32529	18.40977	10
94	44.8417	18.40977	10
95	45.52112	18.40977	10
96	46.2714	19.41977	10
97	47.02177	19.41977	10
98	49.01353	19.41977	10
99	54.03325	3.61743	2
100	59.64325	3.61743	2
101	58.63336	3.61743	2
102	61.05335	3.61743	2
103	62.99335	3.61743	3
104	64.91334	3.61743	3
105	57.40355	5.2412	3
106	59.96375	5.2412	3
107	61.81154	5.0412	3
108	62.02322	5.0412	3
109	61.57301	5.1212	3
110	65.30499	5.0412	4
111	67.95979	6.43331	4
112	61.28422	6.13331	4
113	61.98683	6.43331	4
114	62.99461	6.43331	4
115	64.27333	6.43331	4
116	65.59327	6.43331	5

117	62.26743	7.84324	4
119	62.50583	7.84324	4
119	63.15537	7.84324	5
120	63.94559	7.84324	5
121	64.9659	7.84324	5
122	65.09311	7.84324	5
123	63.67129	9.24821	5
124	63.91994	9.24821	5
125	64.32319	9.24821	5
126	64.90339	9.24821	6
127	65.64933	9.24821	6
128	66.47917	9.24821	6

NUMBER OF ELASTIC AXIS POINTS ON FRONT FUSE-LAGE #13

COORDINATES OF ELASTIC AXIS SEGMENTS

I	XEA	YEA
1	35.60921	0.
2	33.3333	0.
3	30.4157	0.
4	27.6042	0.
5	25.0000	0.
6	22.5000	0.
7	20.0000	0.
8	17.5000	0.
9	15.4157	0.
10	12.7093	0.
11	10.4157	0.
12	8.1253	0.
13	5.4157	0.

ELASTIC AXIS TORSIONAL AND BENDING STIFFNESS

I	EI	KGJ
1	1.199E+10	0.
2	0.159E+10	0.
3	0.139E+10	0.
4	0.115E+10	0.
5	0.950E+9	0.
6	0.793E+9	0.
7	0.520E+9	0.
8	0.500E+9	0.
9	0.371E+9	0.
10	0.260E+9	0.
11	0.200E+9	0.
12	0.120E+9	0.

NUMBER OF ELASTIC AXIS POINTS ON REAR FJSE-A3B #12

COORDINATES OF ELASTIC AXIS SEGMENTS

I	XEA	YEA
1	35.6099	0.
2	38.9503	0.
3	41.7500	0.
4	44.3750	0.
5	47.0933	0.
6	49.7916	0.
7	52.5000	0.
8	57.2917	0.
9	57.7083	0.
10	60.6250	0.
11	63.5417	0.
12	66.4583	0.

ELASTIC AXIS TORSIONAL AND BENDING STIFFNESS

I	ET	KGJ
1	2.220E 10	0.
2	2.220E 10	0.
3	9.219E 10	0.
4	9.219E 10	0.
5	2.158E 10	0.
6	2.114E 10	0.
7	0.800E 10	0.
8	0.560E 9	0.
9	0.380E 9	0.
10	0.160E 9	0.
11	0.194E 8	0.

NUMBER OF ELASTIC AXIS POINTS ON MAIN JING #10

COORDINATES OF ELASTIC AXIS SEGMENTS

I	XEA	YEA
1	35.6090	0.5000
2	36.5900	1.5000
3	37.7800	3.9000
4	39.7800	5.7000
5	41.6000	7.5000
6	43.0000	9.4000
7	45.0000	11.4000
8	47.7000	13.6000
9	49.1200	15.6000
10	50.5200	17.9000

EL0 AXIS TORSIONAL AND BENDING STIFFNESS KGJ

1	0.9931E 8	1.8472E 08
2	0.7985E 8	1.6175E 08
3	0.5485E 8	0.8444E 08
4	0.3681E 8	0.2779E 08
5	0.2431E 8	0.1944E 08
6	0.1529E 8	0.1250E 08
7	0.7639E 7	0.6250E 07
8	3.3194E 7	0.2779E 07
9	3.1250E 7	0.1111E 07

NUMBER OF ELASTIC AXIS POINTS ON HORIZONTAL. TABLE 6

COORDINATES OF ELASTIC AXIS SEGMENTS

I	XEA	YEA
1	60.6250	0.
2	61.2500	1.4300
3	62.5700	3.7200
4	63.9300	5.5100
5	64.8400	7.2900
6	65.9900	9.0700

ELASTIC AXIS TORSIONAL AND BENDING STIFFNESS

I	EI	KQJ
1	3.3125E 8	0.2706E 08
2	0.2361E 8	5.1875E 08
3	0.1389E 8	1.9728E 07
4	0.8845E 7	0.2206E 07
5	0.3872E 7	0.2451E 07

ELASTIC DERIVATIVES FOR EACH NUMBER= 1.50

WEIGHT= 740.0 S.O.S.# 1115.990 ALTITUDE= 0.
 VELOCITY= 0.1975 U
 DYNAMIC PRESSURE= 0.13372E 04

CLYD1= 0.04534
 CLAPAS= 0.2501E 01
 CLAPAS= 0.2501E 01
 CLCEN= 0.1637E 03
 CLCEN= 0.1637E 03
 CLC1 = 0.5101E 02
 CLC1 = 0.1977E 01
 CLW1 = 0.15217E-03
 CLW1 = 0.5021E-01
 CLYD1= 0.7501E-02
 CLYD1= 0.24201E-01
 CLC1N = 0.51227E-02
 CLC1N = 0.16372E-01
 CLAP1 = 0.23304E 01
 CLAP1 = 0.53372E 04

PANEL (METRIC) (SIF)

NUMBER			
1	0.5272E-01	0.22114E 01	0.22114E 01
2	0.5443E-01	0.11512E 01	0.11512E 01
3	0.50054E-01	0.58595E 00	0.58595E 00
4	0.44223E-01	0.24020E 00	0.24020E 00
5	0.33777E-01	0.50713E-01	0.50713E-01
6	0.27747E-01	0.77277E-01	0.77277E-01
7	0.15375E-01	0.28047E 00	0.28047E 00
8	0.18043E-01	0.11815E 01	0.11815E 01
9	0.45078E-02	0.17357E 01	0.17357E 01
10	-0.13735E-01	0.19497E 01	0.19497E 01
11	-0.15713E-01	0.17113E 01	0.17113E 01
12	-0.15771E-01	0.14114E 01	0.14114E 01
13	-0.21718E-01	0.9795E 00	0.9795E 00
14	-0.21745E-01	0.20321E 00	0.20321E 00
15	-0.2462E-01	-0.12754E 00	-0.12754E 00
16	-0.24875E-01	0.57504E-01	0.57504E-01
17	-0.24875E-01	0.57504E-01	0.57504E-01
18	-0.50175E-01	0.74821E 00	0.74821E 00
19	-0.50175E-01	0.17474E 02	0.17474E 02
20	-0.54909E-01	0.45795E 01	0.45795E 01
21	-0.54909E-01	0.24471E 01	0.24471E 01
22	-0.57315E-01	0.19562E 01	0.19562E 01
23	-0.65012E-01	0.19495E 01	0.19495E 01
24	-0.73274E-01	0.19044E 01	0.19044E 01
25	-0.15449E 00	0.15161E 01	0.15161E 01
26	-0.36152E 00	0.13112E 01	0.13112E 01
27	-0.54935E-01	0.12337E 02	0.12337E 02
28	-0.57749E-01	0.22197E 01	0.22197E 01
29	-0.59154E-01	0.30195E 01	0.30195E 01
30	-0.60466E-01	0.22922E 01	0.22922E 01
31	-0.18574E 00	0.17297E 01	0.17297E 01
32	-0.19254E 00	0.17574E 01	0.17574E 01
33	-0.29017E 00	0.14195E 01	0.14195E 01
34	-0.27579E 00	0.13472E 01	0.13472E 01
35	-0.61377E-01	0.10770E 02	0.10770E 02
36	-0.61341E-01	0.57453E 01	0.57453E 01

37	-0.191145	00	0.32191	01
38	-0.191145	00	0.24352	01
39	-0.257248	00	0.199145	01
40	-0.555258	00	0.17221	01
41	-0.111757	00	0.11194	01
42	-0.352748	00	0.12672	01
43	-0.111757	00	0.52659	01
44	-0.191145	00	0.59559	01
45	-0.206666	00	0.34451	01
46	-0.166152	00	0.23333	01
47	-0.166152	00	0.16594	01
48	-0.196135	00	0.19703	01
49	-0.49332	00	0.11297	01
50	-0.49332	00	0.11614	01
51	-0.286365	00	0.59459	01
52	-0.286365	00	0.22123	01
53	-0.166152	00	0.55713	01
54	-0.196135	00	0.29752	01
55	-0.47332	00	0.17083	01
56	-0.49332	00	0.15454	01
57	-0.61215	00	0.10437	01
58	-0.61215	00	0.17542	01
59	-0.166152	00	0.51114	01
60	-0.166152	00	0.54275	01
61	-0.20332	00	0.39533	01
62	-0.49332	00	0.27772	01
63	-0.41215	00	0.15772	01
64	-0.41215	00	0.18420	01
65	-0.74521	00	0.21659	00
66	-0.74521	00	0.10153	01
67	-0.49332	00	0.47120	01
68	-0.49332	00	0.55100	01
69	-0.61215	00	0.40744	01
70	-0.61215	00	0.59161	01
71	-0.74521	00	0.15117	01
72	-0.74521	00	0.14151	01
73	-0.74521	00	0.11523	01
74	-0.83262	00	0.55244	00
75	-0.61215	00	0.35152	01
76	-0.61215	00	0.29184	01
77	-0.74521	00	0.47234	01
78	-0.74521	00	0.32167	01
79	-0.83262	00	0.18481	01
80	-0.83262	00	0.13770	01
81	-0.83262	00	0.14502	01
82	-0.81332	00	0.11094	01
83	-0.74521	00	0.24352	01
84	-0.74521	00	0.37507	01
85	-0.61215	00	0.39444	01
86	-0.83262	00	0.24122	01
87	-0.81332	00	0.26506	01
88	-0.81332	00	0.18174	01
89	-0.81332	00	0.13493	01
90	-0.61312	00	0.12474	01
91	-0.83262	00	0.16434	01
92	-0.83262	00	0.21194	01
93	-0.61312	00	0.34731	01
94	-0.61312	00	0.17495	01
95	-0.61312	00	0.33144	01
96	-0.83312	00	0.23644	01

07	-0.8132E-00	0.1179E-01							
08	-0.8132E-00	0.4491E-00							
09	-0.4165E-01	0.5293E-01							
100	-0.4212E-01	0.2149E-01							
101	-0.4251E-01	0.1237E-01							
102	-0.4304E-01	0.6412E-01							
103	-0.6982E-01	0.7293E-00							
104	-0.7155E-01	0.8041E-00							
105	-0.5272E-01	0.3059E-01							
106	-0.5272E-01	0.2924E-01							
107	-0.5272E-01	0.1674E-01							
108	-0.5272E-01	0.1179E-01							
109	-0.5272E-01	0.4391E-00							
110	-0.5574E-01	0.2420E-01							
111	-0.5574E-01	0.5314E-01							
112	-0.5574E-01	0.3740E-01							
113	-0.6587E-01	0.2232E-01							
114	-0.6387E-01	0.1622E-01							
115	-0.6587E-01	0.1276E-01							
116	-0.6587E-01	0.1149E-01							
117	-0.6587E-01	0.2984E-01							
118	-0.6587E-01	0.4913E-01							
119	-0.6587E-01	0.3150E-01							
120	-0.6587E-01	0.2153E-01							
121	-0.6259E-01	0.1794E-01							
122	-0.6959E-01	0.1342E-01							
123	-0.5059E-01	0.5989E-01							
124	-0.6959E-01	0.3177E-01							
125	-0.6959E-01	0.4642E-01							
126	-0.6959E-01	0.3124E-01							
127	-0.6959E-01	0.1471E-01							
128	-0.6959E-01	0.3341E-00							

SECTIONAL - 20/CL002 139 2110									
V									
0.19773	1.2242	2.2389	0.50645	0.	0.24509				
0.24274	1.2438	2.2494	0.28330	0.	0.18418				
0.23819	1.5302	2.5936	0.43418	0.	0.14927				
0.41341	1.5302	2.5936	0.41156	0.	0.10625				
0.48653	1.3203	2.2327	0.35213	0.	0.08457				
0.57376	1.0547	2.2271	0.32243	0.	0.07455				
0.65733	0.5107	2.2612	0.27576	0.					
0.74131	0.5729	2.2833	0.23922	0.					
0.95416	0.4509	2.3043	0.20196	0.					
0.95018	0.4403	2.2004	0.14159	0.					

SECTIONAL CD/CL002 FOR HORIZONTAL TAIL						
V	CDI	SLI	DAVIA	GT	CD/CL002	
0.36074	1.20603	1.27064	0.25794	0.	0.22201	
0.20210	1.52072	1.51159	0.25140	0.	0.26155	
0.89333	1.77221	1.76703	0.27456	0.	0.32810	
0.24432	2.22915	2.46797	0.27639	0.	0.42327	
0.92432	2.37831	2.76795	0.22842	0.	0.47466	

TOTAL LEADING EDGE TRICOUNT COEFFICIENTS 0.
 TOTAL TRICOUNT DRAG COEFFICIENTS 0.38991E 01
 CD/CL002 0.34963E 00

THIS CASE IS COMPLETE

8. TEST CASE 3

In this test case the geometry data of one of the examples given in Ref. 3 is used. This geometry data is reduced by the program to calculated rigid stability derivatives and ΔC_p values. Figure 5 gives the actual geometrical description and geometry assumed by the program. Input data cards are listed in Table 7 and output data are listed in Table 8.

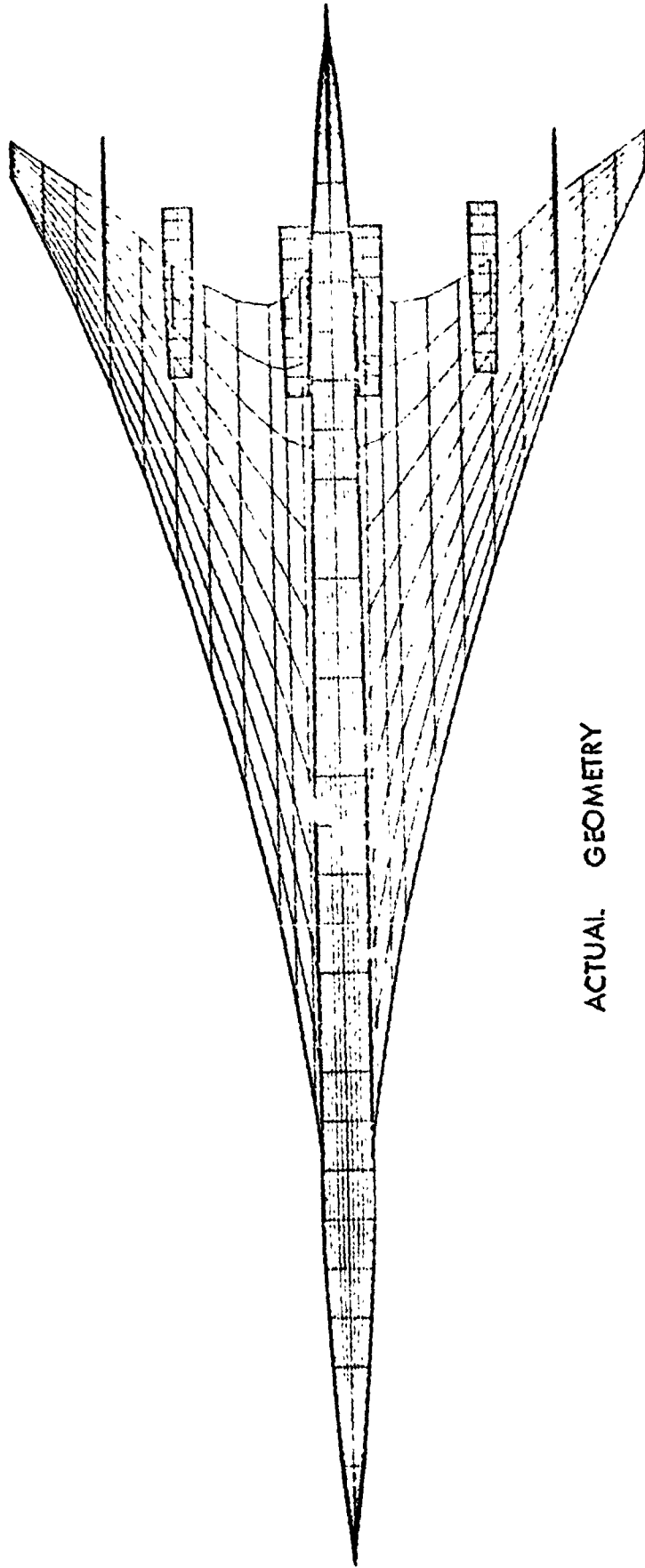
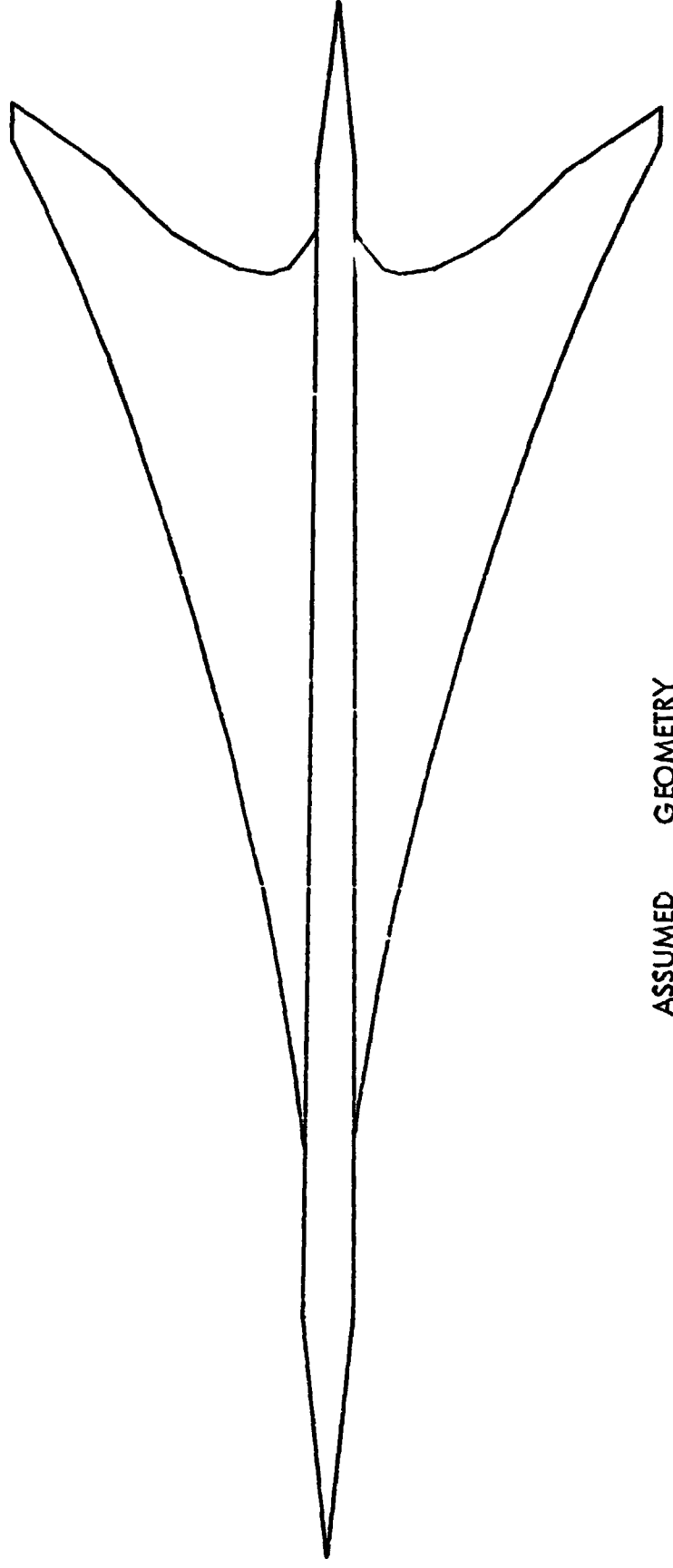


Figure 5. Actual and Assumed Planform Geometry for Test Case 3.



ASSUMED GEOMETRY

Figure 5 (Continued) Actual and Assumed Planform Geometry for Test Case 3

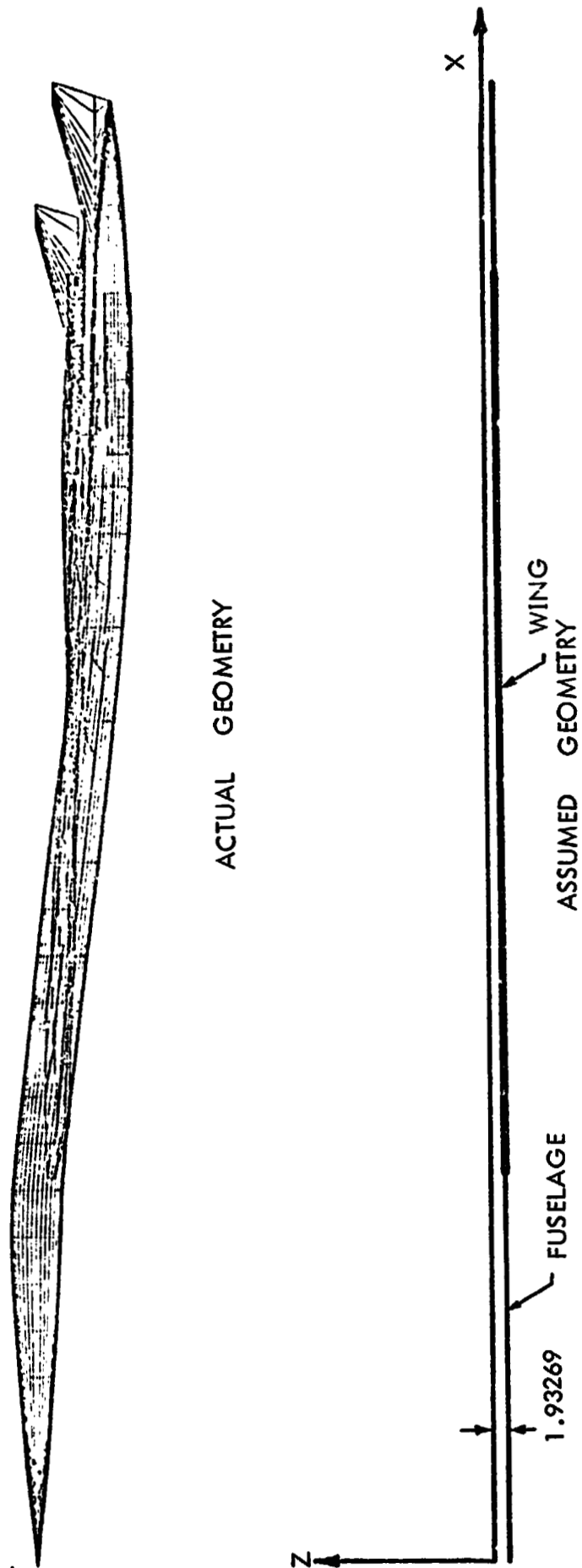


Figure 5 (Continued) Actual and Assumed Planform Geometry for Test Case 3

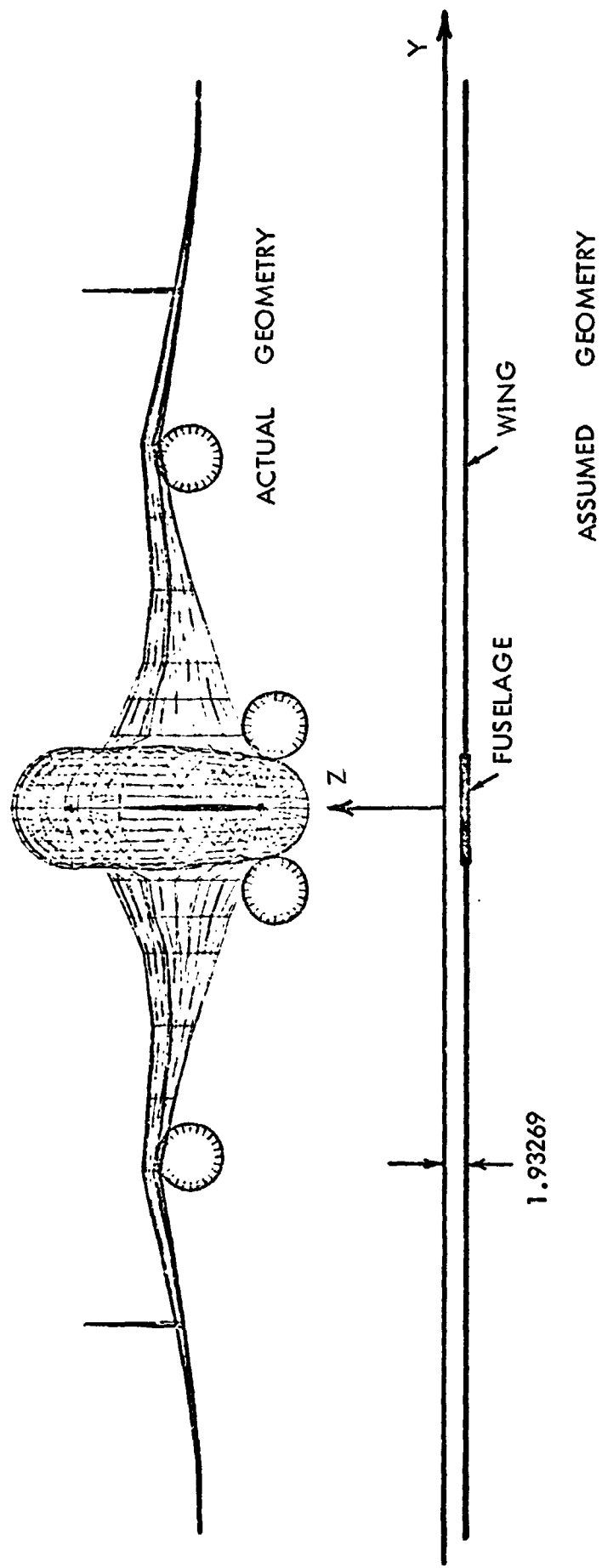


Figure 5 (Continued) Actual and Assumed Platform Geometry for Test Case 2

Table 7 (Continued) Listing of Input Data Cards for Test Case 3

2	0.	.0225	.1085	.16	.249	.258	.3135	.304	.278	.238	TZORD 8
2	.185	.1235	.0568								TZORD 8
2	0.	.02	.1055	.158	.248	.2858	.305	.311	.308	.2995	TZORD 9
2	.2845	.2635	.2385								TZORD 9
2	0.	.0085	.049	.0695	.1175	.144	.155	.158	.1595	.1585	TZORD 10
2	.1545	.148	.1398								TZORD 10
2	0.	-.003	-0.014	-.023	-.043	-.061	-.077	-.09	-.1005	-.11	TZORD 11
2	-.1155	-.119	-.1224								TZORD 11
2	0.	-.0025	-.01	-.017	-.0325	-.047	-.062	-.075	-.088	-.1	TZORD 12
2	-.1115	-.122	-.1324								TZORD 12
2	0.	.304	.491	.803	1.069	1.28	1.43	1.518	1.55	1.451	WAFORD 1
2	1.162	.678	0.	.71	.962	1.156	1.296	1.373	1.396	1.294	WAFORD 1
2	0.	.265	.423								WAFORD 2
2	1.028	.593	0.	.635	.889	1.079	1.204	1.272	1.263	1.136	WAFORD 2
2	0.	.226	.338								WAFORD 3
2	.885	.506	0.	.596	.87	1.074	1.2	1.25	1.234	1.083	WAFORD 3
2	0.	.204	.274								WAFORD 4
2	.832	.472	0.	.559	.886	1.111	1.246	1.294	1.242	1.087	WAFORD 4
2	0.	.144	.175								WAFORD 5
2	.828	.466	0.	.522	.886	1.145	1.289	1.341	1.285	1.125	WAFORD 5
2	0.	.066	.09								WAFORD 6
2	.852	.48	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 6
2	0.	.006	.033								WAFORD 7
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 7
2	0.	.006	.033								WAFORD 8
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 8
2	0.	.005	.033								WAFORD 9
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 9
2	0.	.006	.033								WAFORD 10
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 10
2	0.	.006	.033								WAFORD 11
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 11
2	0.	.006	.033								WAFORD 12
2	.88	.495	0.	.495	.88	1.155	1.32	1.375	1.32	1.155	WAFORD 12

Table 8. Output for Test Case 3

SST CONFIGURATION WITH CAMBERED CIRCULAR BODY (NASA-TMX-2074) AT MACH 2.6

.....
 GEOMETRY DATA IS DIVIDED IN 12 SECTIONS

DEFINITION OF SECTION 1

X-LEADING EDGE	X-TRAILING EDGE	Y-LEADING EDGE	Z
0.	312.0000	0.	-1.93259
44.73134	255.54817	5.05000	-1.93269
THERE ARE 13 CONSTANT PERCENT STREAMWISE LINES AT			
0.	4.147	12.500	23.833
			29.167
			37.500
			45.833
			54.167
			62.500
			70.833
			79.167
			87.500
100.000			
THERE ARE 2 CONSTANT PERCENT STREAMWISE LINES AT			
0.	100.000		

DEFINITION OF SECTION 2

X-LEADING EDGE	X-TRAILING EDGE	Y-LEADING EDGE	Z
82.50000	12.40000	5.05000	-1.93269
93.90000	260.00000	5.50000	-1.93269
THERE ARE 9 CONSTANT PERCENT STREAMWISE LINES AT			
0.	3.429	12.000	21.000
			33.000
			45.000
			57.000
			69.000
			81.000
			93.000
			100.000
100.000			
THERE ARE 2 CONSTANT PERCENT STREAMWISE LINES AT			
0.	100.000		

DEFINITION OF SECTION 3

X-LEADING EDGE	X-TRAILING EDGE	Y-LEADING EDGE	Z
93.80000	250.00000	5.50000	-1.93269
114.19900	256.50000	9.90000	-1.93269
THERE ARE 9 CONSTANT PERCENT STREAMWISE LINES AT			
0.	3.429	12.000	21.000
			33.000
			45.000
			57.000
			69.000
			81.000
			93.000
			100.000
100.000			
THERE ARE 2 CONSTANT PERCENT STREAMWISE LINES AT			
0.	100.000		

DEFINITION OF SECTION 4

X-LEADING EDGE	X-TRAILING EDGE	Y-LEADING EDGE	Z
114.19900	256.50000	9.90000	-1.93269
130.42900	255.49900	13.20000	-1.93269
THERE ARE 9 CONSTANT PERCENT STREAMWISE LINES AT			
0.	3.429	12.000	21.000
			33.000
			45.000
			57.000
			69.000
			81.000
			93.000
			100.000
100.000			
THERE ARE 2 CONSTANT PERCENT STREAMWISE LINES AT			
0.	100.000		

DEFINITION OF SECTION 5

X-LEADING EDGE	X-TRAILING EDGE	Y-LEADING EDGE	Z
130.42900	255.49900	13.20000	-1.93269
157.98000	256.50000	17.50000	-1.93269
THERE ARE 9 CONSTANT PERCENT STREAMWISE LINES AT			
0.	3.429	12.000	21.000
			33.000
			45.000
			57.000
			69.000
			81.000
			93.000
			100.000
100.000			
THERE ARE 9 CONSTANT PERCENT STREAMWISE LINES AT			
0.	100.000		

0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 6

X-LEADING EDGE X-TRAILING EDGE V-LEADING EDGE Z
 157,9000 256,5500 19,5000 -1,93269
 161,2900J 259,6000 24,0000 -1,93269
 THERE ARE 7 CONSTANT PERCENT STRAIGHT LINES AT
 0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 7

X-LEADING EDGE X-TRAILING EDGE V-LEADING EDGE Z
 181,29000 219,6000 26,0000 -1,93269
 202,41000 263,65100 33,00000 -1,93269
 THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
 0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 8

X-LEADING EDGE X-TRAILING EDGE V-LEADING EDGE Z
 202,41000 263,65100 33,00000 -1,93269
 221,63000 249,44900 39,50000 -1,93269
 THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
 0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 9

X-LEADING EDGE X-TRAILING EDGE V-LEADING EDGE Z
 221,6300J 259,44900 39,50000 -1,93269
 239,16000 275,69900 46,20000 -1,93269
 THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
 0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 10

X-LEADING EDGE X-TRAILING EDGE V-LEADING EDGE Z
 239,16000 275,69900 46,20000 -1,93269
 255,00000 250,35000 52,50000 -1,93269
 THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
 0, J.429 12,000 21,000 31,000 46,000 63,000 81,000 100,000
 THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
 0, 100,000

DEFINITION OF SECTION 11

```

*****
X-LEADING EDGE      X-TRAILING EDGE      VALLEADING EDGE      Z
250.00000          280.35000          22.50000              -1.93269
259.25000          284.90000          29.40000              -1.93269
THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
3.429              12.000              21.000              30.000              40.000              50.000              60.000              70.000              80.000              90.000              100.000
THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
0.
100.000

```

```

DEFINITION OF SECTION12
*****
X-LEADING EDGE      X-TRAILING EDGE      VALLEADING EDGE      Z
250.23000          284.90000          29.40000              -1.93269
292.00000          299.40000          36.00000              -1.93269
THERE ARE 9 CONSTANT PERCENT STRAIGHT LINES AT
3.429              12.000              21.000              30.000              40.000              50.000              60.000              70.000              80.000              90.000              100.000
THERE ARE 2 CONSTANT PERCENT STRAIGHT LINES AT
0.
100.000
REF. AREA= 0.94940E 04
REF. CHORD= 0.18010E 03

```

```

CLALPR = 0.19707E 01
CYALPR = 0.23124E 01
CXB = 0.20422E 01
CXB = 0.02997E 01

```

SECTIONAL COEFFICIENTS FOR WING

Y	C _D	C _L	C _M	CT	CD/CL ²
0.09510	0.74648	0.73334	0.21576	-0.20188	0.14974
0.12436	0.89140	1.35347	0.42622	-0.18407	0.21704
0.17495	0.99437	1.23155	0.42550	-0.126398	0.24154
0.24904	1.03942	1.43539	0.41056	-0.37596	0.24732
0.34911	1.16875	1.74234	0.29674	-0.57369	0.31696
0.47724	1.24205	2.12112	0.25028	-0.86407	0.34695
0.54779	1.30510	2.33739	0.23302	-1.26188	0.34409
0.64751	1.34315	3.13314	0.20533	-1.79480	0.34432
0.74689	1.32789	3.99773	0.16216	-2.56008	0.34012
0.84697	1.02877	5.23334	0.10000	-4.102757	0.27820
0.94403	-0.44797	6.54133	0.11172	-7.133990	-0.13494

```

TOTAL LEADING EDGE THRUST COEFFICIENT=0.52438 00
TOTAL INDUCED DRAG COEFFICIENTS 0.13973 31
CD/CL2= 0.29710E 00

```


YACJ NUMBER: 1.50
.....

30 VALUES ARE FOR ALPHA: 1.000000 RADIAN
.....

PAVEL NUMBER	YCP	YCB	ZCP	YCS	AREA	CP
1	31.7911	2.38096	0.19329	26.69419	59.79482	0.191822 00
2	51.9911	2.38096	0.19329	43.58726	112.11350	0.46672E 00
3	76.0132	2.38096	0.19329	55.92468	112.11350	0.21329E 00
4	98.4297	2.38096	0.19329	98.3212	112.11350	0.27512E 00
5	120.8474	2.38096	0.19329	110.74556	112.11350	0.18224E 00
6	143.2642	2.38096	0.19329	133.17658	112.11350	0.75232E 00
7	165.6827	2.38096	0.19329	135.59441	112.11350	0.93295E 00
8	188.1013	2.38096	0.19329	178.0195	112.11350	0.9882E 00
9	210.5211	2.38096	0.19329	200.4927	112.11350	0.9979E 00
10	232.9456	2.38096	0.19329	222.82671	112.11350	0.66972E 00
11	255.3694	2.38096	0.19329	245.2414	112.11350	0.1864E 00
12	277.7940	2.38096	0.19329	273.2573	16.11701	0.29712E 00
13	93.4349	5.81453	0.19329	90.93375	4.70297	0.19902E 01
14	108.0989	5.81453	0.19329	131.3796	23.70347	0.94124E 00
15	127.5441	5.81453	0.19329	116.5825	24.15443	0.7750E 00
16	148.1094	5.81453	0.19329	134.7441	32.70399	0.45017E 00
17	169.8062	5.81453	0.19329	158.13648	40.25749	0.99342E 00
18	195.9174	5.81453	0.19329	194.1320	47.5099	0.10216E 01
19	225.7110	5.81453	0.19329	212.7838	47.5099	0.1765E 00
20	259.9774	5.81453	0.19329	244.7812	90.95282	0.71242E 00
21	189.7219	8.20749	0.19329	106.3696	17.49590	0.2310E 01
22	221.5432	8.20749	0.19329	115.6135	45.83440	0.1261E 01
23	135.5035	8.20749	0.19329	159.2394	47.1997	0.1031E 01
24	153.8219	8.20749	0.19329	145.4718	61.79329	0.12294E 01
25	175.7727	8.20749	0.19329	166.4292	75.36562	0.1057E 01
26	199.9048	8.20749	0.19329	189.5011	79.36562	0.10715E 01
27	227.5967	8.20749	0.19329	215.0455	91.3794	0.10350E 01
28	124.3437	11.51402	0.19329	233.6745	98.73105	0.96754E 00
29	256.8514	11.51402	0.19329	124.5842	12.11452	0.8020E 01
30	137.7259	11.51402	0.19329	182.5898	37.79124	0.1464E 01
31	163.7397	11.51402	0.19329	144.31204	57.45232	0.1469E 01
32	185.3847	11.51402	0.19329	158.3116	52.70775	0.12025E 01
33	185.4559	11.51402	0.19329	176.4431	65.13720	0.1159E 01
34	207.5409	11.51402	0.19329	178.4847	67.13720	0.11360E 01
35	229.4024	11.51402	0.19329	218.57165	77.46164	0.1090E 01
36	254.7685	11.51402	0.19329	233.3246	83.77179	0.9451E 00
37	137.4658	16.37052	0.19329	145.6217	23.28107	0.4175E 01
38	159.7524	16.37052	0.19329	152.4633	63.19117	0.22143E 01
39	164.9243	16.37052	0.19329	162.2697	67.16169	0.14071E 01
40	189.1332	16.37052	0.19329	174.0145	81.98224	0.14160E 01
41	199.7942	16.37052	0.19329	199.2350	110.50261	0.1297E 01
42	233.6941	16.37052	0.19329	206.0899	110.50277	0.13347E 01
43	233.6941	16.37052	0.19329	234.3792	142.72374	8.1174E 01
44	254.9364	16.37052	0.19329	245.3147	140.09489	0.1072E 01
45	172.0314	22.97539	0.19329	170.71937	20.03725	0.15320E 01
46	179.4809	22.97539	0.19329	176.05449	50.08442	0.19976E 01
47	187.4370	22.97539	0.19329	183.8649	52.99275	0.2052E 01
48	194.0037	22.97539	0.19329	193.20296	70.12369	0.17405E 01

49	211,2090	22,97539	81,33259	205,20679	87,45461	0,15246E 01
50	224,5469	22,97539	81,33259	218,54470	87,45461	0,14110E 01
51	249,4181	22,97539	81,33259	245,21619	107,19282	0,11122E 01
52	257,2691	22,97539	81,33259	249,64516	111,42717	0,12813E 01
53	193,70771	29,54407	81,33259	192,61911	129,81535	0,22755E 01
54	199,5480	29,54407	81,33259	196,87298	137,22402	0,15287E 01
55	205,5424	29,54407	81,33259	203,00318	141,50405	0,13748E 01
56	214,1491	29,54407	81,33259	213,37747	159,44139	0,21200E 01
57	226,5923	29,54407	81,33259	219,84465	167,17573	0,18124E 01
58	235,1382	29,54407	81,33259	220,32333	181,12722	0,17222E 01
59	247,4719	29,54407	81,33259	224,94147	181,12031	0,15251E 01
60	260,9770	29,54407	81,33259	254,97423	181,12031	0,14463E 01
61	213,4102	36,14462	81,33259	212,54517	141,14155	0,92045E 01
62	217,6824	36,14462	81,33259	215,84559	150,44221	0,13742E 01
63	229,4024	36,14462	81,33259	220,64854	159,74275	0,12226E 01
64	229,5728	36,14462	81,33259	226,42320	173,14171	0,23722E 01
65	235,5437	36,14462	81,33259	235,82511	181,14171	0,21122E 01
66	245,7457	36,14462	81,33259	242,04271	181,14171	0,17423E 01
67	255,5282	36,14462	81,33259	251,04959	181,14171	0,14349E 01
68	265,3142	42,75557	81,33259	261,22457	181,14171	0,14349E 01
69	231,4073	42,75557	81,33259	230,74979	181,14171	0,13442E 02
70	234,2417	42,75557	81,33259	235,30540	181,14171	0,15746E 01
71	237,7974	42,75557	81,33259	237,03541	229,31125	0,47021E 01
72	243,7940	42,75557	81,33259	241,40316	237,13779	0,47021E 01
73	250,1070	42,75557	81,33259	247,23827	33,42705	0,34202E 01
74	251,4860	42,75557	81,33259	250,61505	41,94431	0,27243E 01
75	264,0729	42,75557	81,33259	260,62952	41,94431	0,23875E 01
76	272,1249	49,24852	81,33259	268,40222	50,24355	0,21246E 01
77	247,5227	49,24852	81,33259	247,14597	53,00333	0,19072E 01
78	250,2534	49,24852	81,33259	249,02777	71,24334	0,19275E 02
79	251,1539	49,24852	81,33259	251,74321	17,35599	0,71155E 01
80	256,7740	49,24852	81,33259	255,00007	14,23450	0,51306E 01
81	261,4384	49,24852	81,33259	259,31699	24,27233	0,35972E 01
82	261,1400	49,24852	81,33259	264,02382	31,24115	0,32646E 01
83	271,7469	49,24852	81,33259	269,24178	51,72415	0,23584E 01
84	277,6452	49,24852	81,33259	273,00737	56,46599	0,23907E 01
85	242,2453	55,84042	81,33259	241,91349	59,21725	0,2175E 01
86	265,9787	55,84042	81,33259	263,14693	4,44155	0,2411E 02
87	265,8437	55,84042	3259	265,14693	11,0235	0,1041E 02
88	263,3232	55,84042	3259	267,19382	12,14294	0,57054E 01
89	271,4213	55,84042	3259	270,01507	15,24322	0,32613E 01
90	276,5583	55,84042	3259	273,14957	20,30489	0,4913E 01
91	278,2087	55,84042	81,33259	276,59465	20,30489	0,3111E 01
92	282,2423	55,84042	81,33259	280,44143	22,7125	0,32625E 01
93	275,2433	62,35568	81,33259	275,0528	25,2345	0,23719E 02
94	275,2433	62,35568	81,33259	275,70003	26,2227	0,14413E 02
95	277,3403	62,35568	81,33259	276,83595	6,45174	0,1421E 02
96	280,7494	62,35568	81,33259	278,09990	7,13773	0,7787E 01
97	280,5560	62,35568	81,33259	279,72533	11,4269	0,61415E 01
98	287,3014	62,35568	81,33259	283,52820	11,4269	0,42822E 01
99	284,6035	62,35568	81,33259	283,51300	13,70559	0,33473E 01
300	280,7687	62,35568	81,33259	289,73358	14,10469	0,33258E 01

THIS CASE IS COMPLETE

9. COMPUTER PROGRAM LISTING

The computer program was originally written by members of the Flight Research Laboratory at the University of Kansas for the Honeywell 635 computer system. The version listed in this document is a revised version as optimized by Computer Sciences Corporation of Hampton, Virginia for the CDC 6600 computer at NASA Langley Research Center.

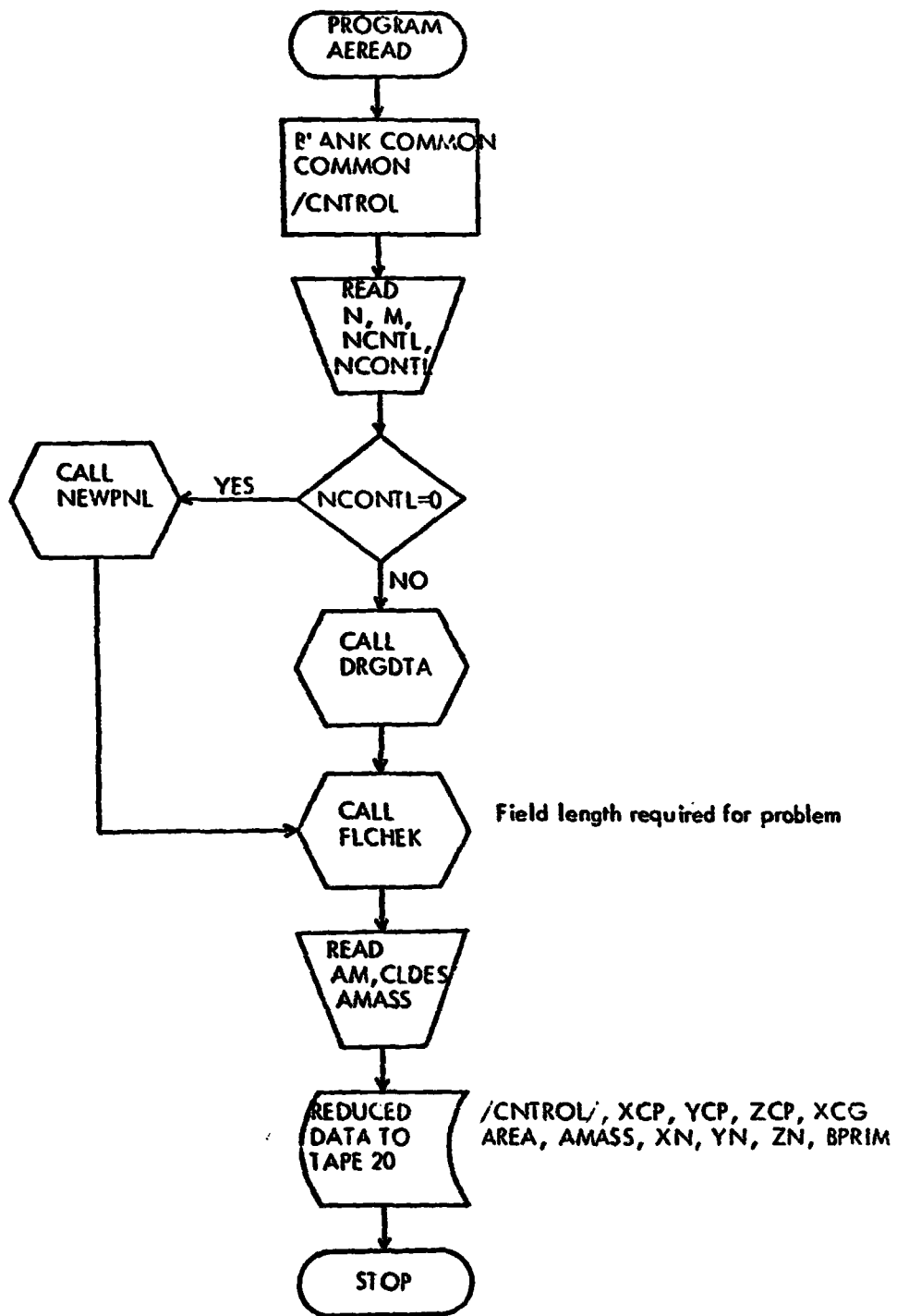


FIGURE 6. FLOW CHART FOR MAIN LINE

FIGURE 6. (continued)

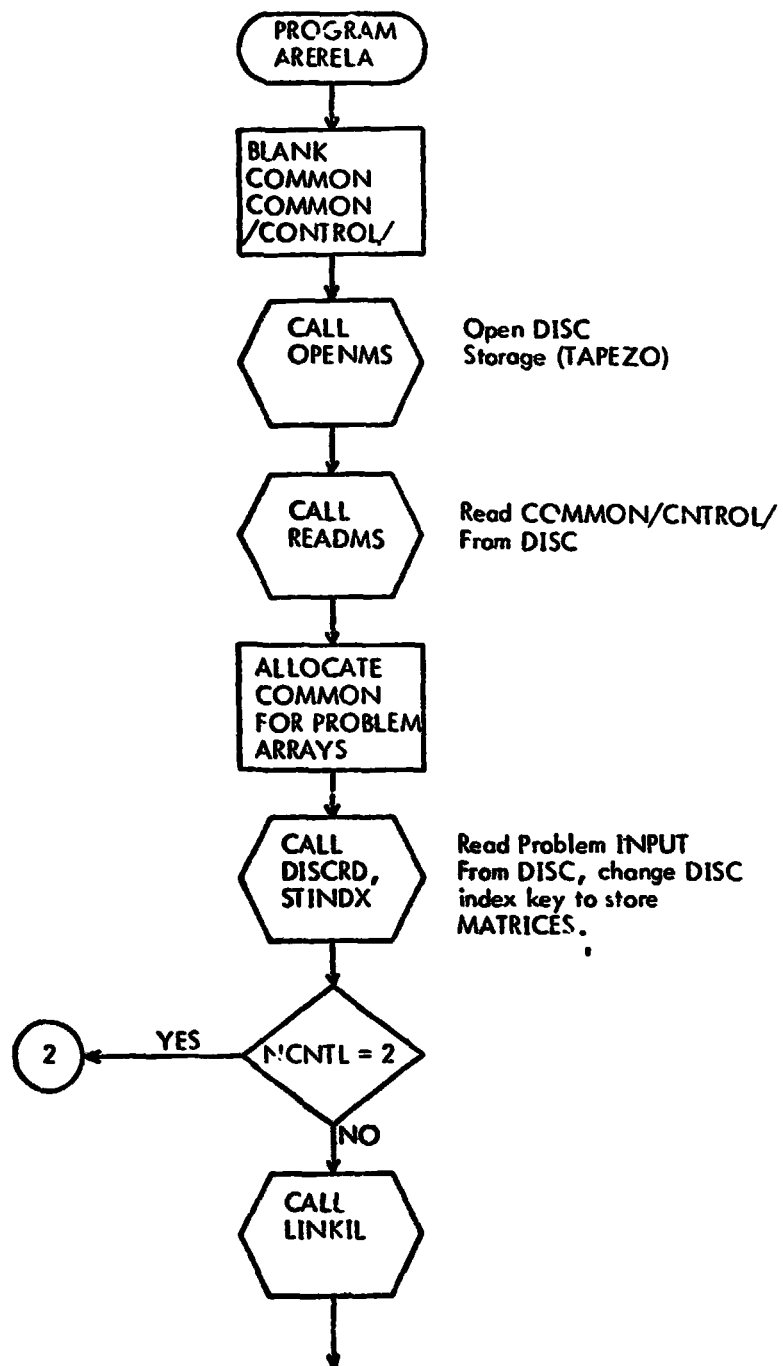


FIGURE 6. (continued)

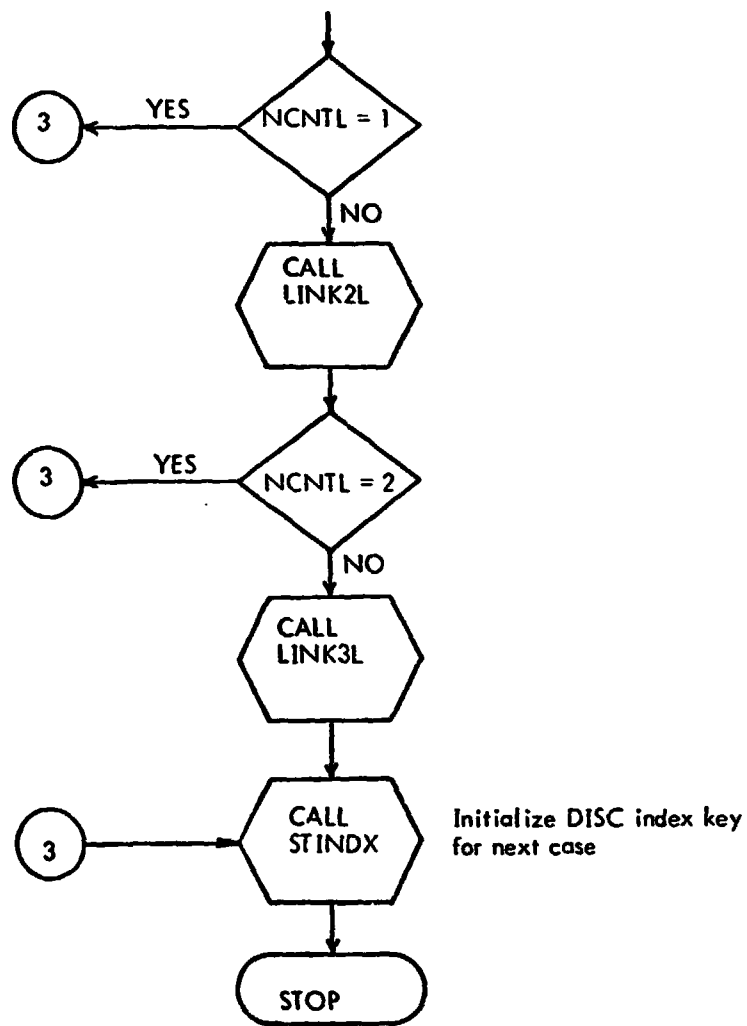


FIGURE 6. (continued)

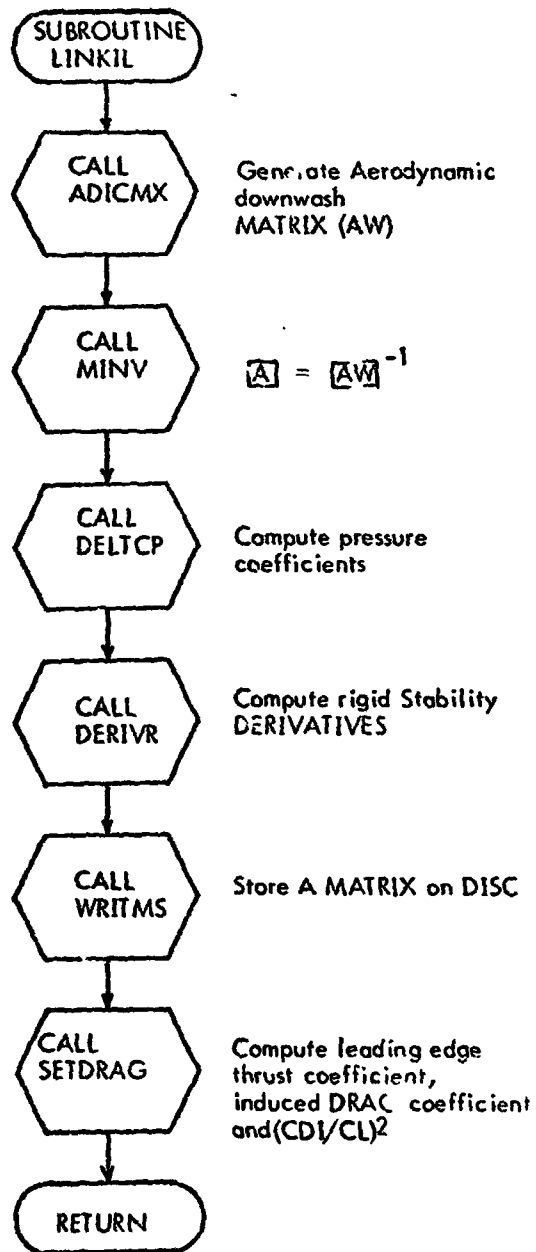


FIGURE 6. (continued)

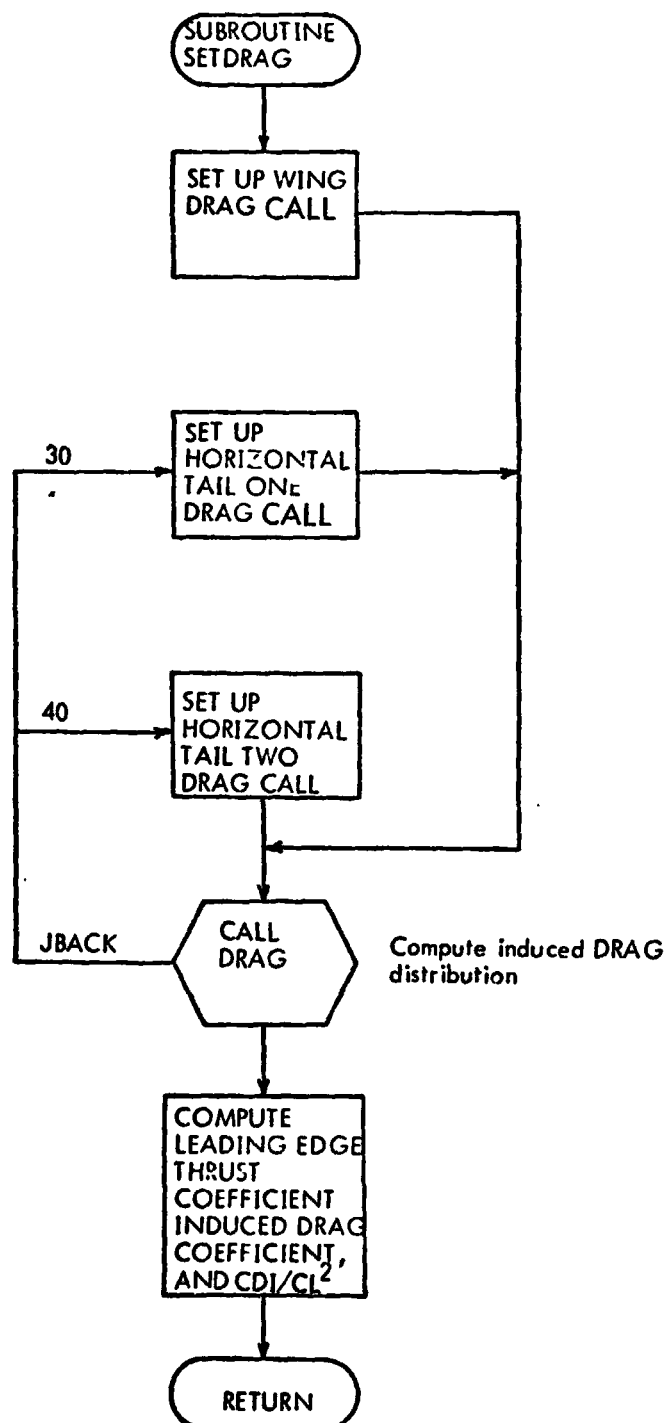
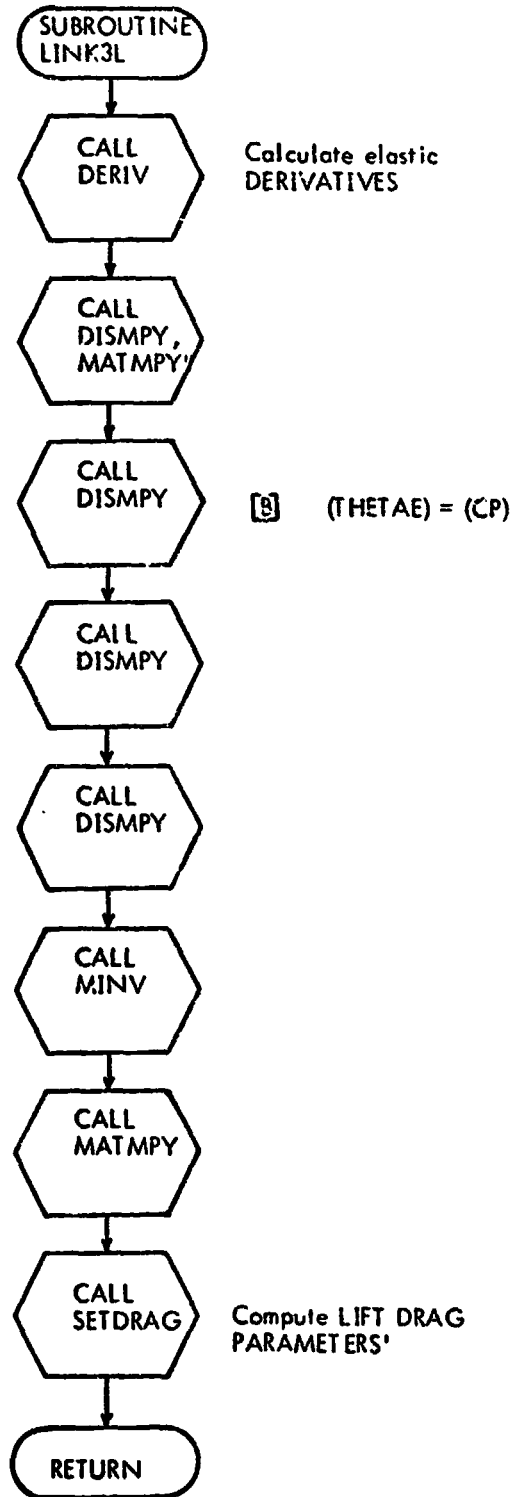


FIGURE 6. (continued)



```

PROGRAM AEREA4(INPUT=201,OUTPUT=201,TAPE5=INPUT,TAPE6=OUTPUT,
1 TAPE20=401)
C.....
C**TWO-STEP PROGRAM FOR CALCULATING ALPHA- AND Q-STABILITY
C DERIVATIVES AND INDUCED DRAG FOR THIN ELASTIC AIRPLANES AT
C SUBSONIC AND SUPERSONIC SPEEDS. MAX PROBLEM SIZE IS 300 PANELS.
C**WRITTEN BY MEMBERS OF FLIGHT RESEARCH LABORATORY, UNIV. OF KANSAS.
C
C JOBSTEP AEREA4 PROCESSES THE INPUT DATA FOR DIVIDING THE
C LIFTING SURFACES INTO AERODYNAMIC PANELS. THE REDUCED DATA
C IS STORED ON A DISC FILE (TAPE20) WHICH IS ACCESSED BY THE
C STABILITY DERIVATIVE COMPUTATION JOBSTEP AEREA4.
C
C**OPTIMIZED BY COMPUTER SCIENCES CORPORATION FOR NASA LANGLEY
C RESEARCH CENTER.
C
C**THE RANDOM-ACCESS DISC I/O CALLS TO OPENMS, READMS, WRITMS,
C WRITIN AND STINDX ARE CDC 6000 DEPENDENT AND MUST BE CHANGED
C FOR USE ON OTHER COMPUTERS.
C MODIFICATIONS BY C.ROLZ AND B.PARKER JUNE 1972.
C LIFTING SURFACES INTO AERODYNAMIC PANELS
C
C IF NCONTL=0 DATA IS INPUTTED ACCORDING TO THE PRESENT
C FORMAT
C IF NCONTL=1 DATA IS INPUTTED ACCORDING TO THE FORMAT
C GIVEN IN NASA-TMX-2074
C.....

```

```

AERE0010
AERE0020
AERE0030
AERE0040
AERE0050
AERE0060
AERE0070
AERE0075
AERE0080
AERE0090
AERE0100
AERE0110
AERE0120
AERE0130
AERE0140
AERE0150
AERE0160
AERE0162
AERE0164
AERE0166
AERE0170
AERE0180
AERE0190
AERE0200
AERE0210
AERE0220
AERE0230
AERE0240
AERE0250
AERE0260

```

```

AERE0270
AERE0280
AERE0290
AERE0300
AERE0310
AERE0320
AERE0330
AERE0340
AERE0350
AERE0360
AERE0370
AERE0380
AERE0390
AERE0400
AERE0410
AERE0420
AERE0430
AERE0440
AERE0450
AERE0460
AERE0470
AERE0480
AERE0490
AERE0500
AERE0510
AERE0520
AERE0530
AERE0540
AERE0550
AERE0560
AERE0570
AERE0580
AERE0590
AERE0600
AERE0610

DIMENSION IND(12)
DIMENSION RANDOM(4,300)
DIMENSION TITLF(16)
COMMON/CONTROL/ LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HT1PNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHTIP,NHT2P,HALFB,ALPHA,HALFB1,HALFB2,NCPSWL,NCFWNG,MAX
C**READ PROGRAM COMMON SET UP FOR 300 PANEL PROBLEM
COMMON XCG(300),XCP(300),YCP(300),ZCP(300),AREA(300),AMASS(300),
1 XN(300,4),YN(300,4),ZN(300,4),RPRIM(300,4)
INTEGER WNGPNL,HT1PNL,HT2PNL
EQUIVALENCE(LPANEL,N,NUM), (NEAMAX,M)
EQUIVALENCE (XCG(1),RANDOM(1,1))
DIMENSION DUM(25)
EQUIVALENCE (LPANEL,DUM(1))
DO 10 I=1,25
10 DUM(I)=0.
MAX=300
C*****
READ (5,4) TITLE
READ (5,5) N,M,NCNTL
READ (5,7) NCONTL
C*****
WRITE (6,6) TITLE
C
C SURROUTINE DRGDTA READS THE GEOMETRY DATA ACCORDING TO THE
C FORMAT GIVEN IN NASA-TMX-2074 AND MAKES AERODYNAMIC PANELS
C CONFORMAL TO THIS PROGRAM
C IF(INCONTL.GT.0)CALL DRGDTA
C
C SURROUTINE NEWPNL USES THE INPUT DATA FORMAT OF THE PRESENT
C PROGRAM FOR FINDING OUT AERODYNAMIC PANELS
C
C IF(INCONTL.EQ.0)CALL NEWPNL
C** FLCHK CHECKS THE FIELD LENGTH REQUIRED FOR AN N PANEL PROBLEM AND

```

```

C STOPS EXECUTION IF THE FIELD LENGTH IS EXCEEDED
CALL FLCKEK(N)
*****
READ (5,8) AM,CLDES
IF (NCNTL.NE.1) READ(5,8)(AMASS(I),I=1,LPANEL)
*****
N4=4*N
C SURROUTINE OPENMS OPENS UP A RANDOM ACCESS FILE FOR DATA STORAGE
C SURROUTINE WRITMS WRITES THE ARRAY ONTO THE RANDOM ACCESS FILE
C
CALL OPENMS(20,IND,12,0)
CALL WRITMS(20,LPANEL,25, 1)
CALL WRITMS(20, XCP(1),N, 2)
CALL WRITMS(20, YCP(1),N, 3)
CALL WRITMS(20, ZCP(1),N, 4)
CALL WRITMS(20, XCG(1),N, 5)
CALL WRITMS(20, ARFA(1),N, 6)
CALL WRITMS(20, AMASS(1),N, 7)
C
C**ARRAYS XN,YN,ZN AND BPRIM ARE STORED WITH ROWS AND COLUMNS
C REVERSED TO FIT DATA STRUCTURE OF JOBSTEP AERELA.
C
DO 20 J=1,300
DO 20 J=1,4 XN(I,J)
CALL WRITMS(20,RANDOM(,1),N4, 8)
DO 21 I=1,200
DO 21 J=1,4 Y(I,J)
CALL WRITMS(20,RANDOM(1,1),N4, 9)
DO 22 I=1,300
DO 22 J=1,4 ZN(I,J)
WRITMS(20,RANDOM(J,I),N4,10)

```

```

AERE0620
AERE0630
AERE0640
AERE0650
AERE0660
AERE0670
AERE0680
AERE0690
AERE0700
AERE0710
AERE0720
AERE0730
AERE0740
AERE0750
AERE0760
AERE0770
AERE0780
AERE0790
AERE0800
AERE0810
AERE0820
AERE0830
AERE0840
AERE0850
AERE0860
AERE0870
AERE0880
AERE0890
AERE0900
AERE0910
AERE0920
AERE0930
AERE0940
AERE0950
AERE0960

```

```
CALL WRITMS(20,RANDOM(I,1),N4,10)
  23 J=1,4
  23 RANDOM(J,1)=FPRIM(I,J)
  CALL WRITMS(20,RANDOM(I,1),N4,11)
  4 FORMAT (16A5)
  5 FORMAT (3I3)
  6 FORMAT (1H1,////,25X,16A5,////)
  7 FORMAT (I2)
  8 FORMAT (8F10.5)
  STOP
  END
```

```
AERE0978
AERE0990
AERE1000
AERE1010
AERE1020
AERE1030
AERE1040
AERE1050
AERE1060
AERE1070
AERE1080
```

```

SURROUTINE FLCHEK(N)
C.....
C**FLCHK DETERMINES PROBLEM FIELD LENGTH REQUIREMENT AND STOPS
C EXECUTION IF FIELD LENGTH IS INSUFFICIENT.
C.....
DIMENSION NFL(1),C(4),L(6)
INTEGER CFL,RFL,FL,O
DATA CFL/10835/,O/32768,4096,512,64/,L(5),L(6)/2*0/
C**CFL IS OBJECT CODE LENGTH. RFL IS FL REQUIRED BY N-PANEL PROBLEM.
C FL IS USER-ASSIGNED FIELD LENGTH.
C
RFL=CFL+28*N+N*N
RFL=MAX0(RFL,19264)
K=LCCF(NFL)
FL=NFL(63-K)
RFL=((RFL-1)/64 + 1)*64
IF(FL.EQ.RFL) RETURN
C
C**CONVERT FIELD LENGTH TO OCTAL
L(1)=RFL/O(1)
DO 10 I=2,4
MFL=MOD(RFL,O(I-1))
L(I)=MFL/O(I)
10 L(I)=MFL/O(I)
900 OFORMAT(1H0,*THE MINIMUM FIELD LENGTH REQUIREMENT FOR THIS PROBLEM
115 *,611,*OCTAL WORDS.*)
WRITE(6,900) L
C
C**STOP JOB IF FIELD LENGTH IS TOO SMALL FOR PROBLEM.
IF(FL.GF.RFL) RETURN
WRITE(6,901)
901 OFORMAT(1H0,*YOUR FIELD LENGTH IS TOO SMALL FOR THIS PROBLEM. EXECUTION
TERMINATED*)
STOP
END

```

```

FLCH010
FLCH020
FLCH030
FLCH040
FLCH050
FLCH060
FLCH070
FLCH080
FLCH090
FLCH0100
FLCH0110
FLCH0120
FLCH0130
FLCH0140
FLCH0150
FLCH0160
FLCH0170
FLCH0180
FLCH0190
FLCH0200
FLCH0210
FLCH0220
FLCH0230
FLCH0240
FLCH0250
FLCH0260
FLCH0270
FLCH0280
FLCH0290
FLCH0300
EXECFLCH0310
FLCH0320
FLCH0330
FLCH0340

```

```

C.....
S:  OUTLINE BREAK(X,Y,Z,N,YY,NN,NNN)
    B*R*E*A*K
C.....
C  SUBROUTINE BREAK GENERATES BREAK LINES ON WING DUE TO
C  HORIZONTAL TAIL AND VICE VERSA
C.....
    DIMENSION X(1),Y(1),Z(1),YY(1)
    NNN=N
    DO 2 I=1,NN
    YY=YY(I)
    DO 1 J=1,N
    IF (Y(J).GE.YYY) GO TO 2
    IF (Y(J).LT.YYY.AND.Y(J+1).GT.YYY) GO TO 3
    GO TO 1
    3 NNN=NNN+1
C
C  SUBROUTINE NEWBRK FINDS OUT THE COORDINATES OF BREAK LINES
    CALL NEWBRK(X(J),X(J+1),Y(J),Y(J+1),Z(J),Z(J+1),YYY,X(NNN),Y(NNN),
    1Z(NNN))
    1 CONTINUE
    2 CONTINUE
    RETURN
    END
C.....
BRAK0010
BRAK0020
BRAK0030
BRAK0040
BRAK0050
BRAK0060
BRAK0070
BRAK0080
BRAK0090
BRAK0100
BRAK0110
BRAK0120
BRAK0130
BRAK0140
BRAK0150
BRAK0160
BRAK0170
BRAK0180
BRAK0190
BRAK0200
BRAK0210
BRAK0220
BRAK0230
BRAK0240

```



```

DRGD0360
DRGD0370
DRGD0380
DRGD0390
DRGD0400
DRGD0410
DRGD0420
DRGD0430
DRGD0440
DRGD0450
DRGD0460
DRGD0470
DRGD0480
DRGD0490
DRGD0500
DRGD0510
DRGD0520
DRGD0530
DRGD0540
DRGD0550
DRGD0560
DRGD0570
DRGD0580
DRGD0590
DRGD0600
DRGD0610
DRGD0620
DRGD0630
DRGD0640
DRGD0650
DRGD0660
DRGD0670
DRGD0680
DRGD0690
DRGD0700

IF (J1.NE.0.AND.J2.EQ.0.AND.J5.EQ.0) NOPTON=4
IF (J1.EQ.0.AND.J2.NE.0.AND.J5.NE.0) GO TO 53
IF (J1.FQ.0.AND.J2.NF.0.AND.J5.FQ.0) GO TO 54
IF (J1.FQ.0.AND.J2.FQ.C.AND.J5.NE.0) GO TO 55
IF (J1.FQ.0.AND.J2.FQ.0.AND.J5.FQ.0) GO TO 56

C      J0 (REFERENCE AREA)
C*****
C      IF (J0.FQ.1) READ (5,58) REFA
C*****
C      J1 (WING DATA)
C*****
C      IF (J1.FQ.0) GO TO 6
C      READ (5,58)(GARR,I=1,NWAFOR)
C      DO 1 I=1,NWAF
C      READ (5,58)X(I),Y(I),Z(I),CHORD;
C      1 CHORD(I)=CHORD(I)+X(I)
C      IF (J1.EQ.(-1)) GO TO 3
C      DO 2 I=1,NWAF
C      2 READ (5,58)(GARR,K=1,NWAFOR)
C      3 DO 4 I=1,NWAF
C      4 READ (5,58)(GARR,K=1,NWAFOR)
C*****
C      ZAVWNG (AVERAGE HFIGHT OF WING)
C      SUM1=0.
C      DO 5 I=1,NWAF
C      5 SUM1=SUM1+Z(I)
C      ZAVWNG=SUM1/(FLOAT(NWAF))
C      NEWAF=NWAF
C*****

```

```

C      J2 (FUSELAGE DATA)
C      J6 (FUSELAGE DATA)
C
      FUSWTH=0.
      6 IF (J2.EQ.0) GO TO 20
C*****
      NFUSXI=1
      DO 8 I=1,NFUS
      NRAD=NRADX(I)
      NFUSXF=NFUSXI+NFORX(I)-1
      READ (5,58)(XFUS(K),K=NFUSXI,NFUSXF)
      IF (J2.EQ.1) GO TO 9
      GO TO 100
      9 DO 10 K=NFUSXI,NFUSXF
      READ (5,58)(DUMMY(L),L=1,NRAD)
C
C      SUBROUTINE MAXVLU FINDS THE VALUE OF THE LARGST ELEMENT
C      OF ARRAY DUMMY
C
      CALL MAXVLU(DUMMY,NRAD,YMAX,KK)
      YFUS(K)=YMAX
      READ (5,58)(DUMMY(L),L=1,NRAD)
      ZFUS(K)=DUMMY(KK)
      10 CONTINUE
      GO TO 8
      100 IF (J6.EQ.0) READ (5,58)(ZFUS(K),K=NFUSXI,NFUSXF)
      READ (5,58)(YFUS(K),K=NFUSXI,NFUSXF)
      DO 7 K=NFUSXI,NFUSF
      7 YFUS(K)=SQRT(YFUS(K)/PAI)
      8 NFUSXI=NFUSXF
C*****
C      ZAVFU (AVERAGE HFIGHT OF FUSELAGE)
C
      SIM2=0.

```

```

DRGD0710
DRGD0720
DRGD0730
DRGD0740
DRGD0750
DRGD0760
DRGD0770
DRGD0780
DRGD0790
DRGD0800
DRGD0810
DRGD0820
DRGD0830
DRGD0840
DRGD0850
DRGD0860
DRGD0870
DRGD0880
DRGD0890
DRGD0900
DRGD0910
DRGD0920
DRGD0930
DRGD0940
DRGD0950
DRGD0960
DRGD0970
DRGD0980
DRGD0990
DRGD1000
DRGD1010
DRGD1020
DRGD1030
DRGD1040
DRGD1050

```

```

DO 12 K=1,NFUSXF
12 SUM2=SUM2+7FUS(K)
ZAVFUS=S(IM2/FL0AT(NFUSXF)
XLF=X(1)
XTF=CHORD(1)
C
C FIND WIDTH OF FUSELAGE
C
C SUBROUTINE WIDTH FINDS OUT THE AVERAGE FUSELAGE WIDTH BETWEEN
C THE GIVEN TWO STATIONS
C
CALL WIDTH(XFUS,YFUS,NFUSXF,XLE,XTE,FUSWTH)
RAD2=FUSWTH/2.
DIFF=ARS(ZAVWNG-ZAVFUS)
IF (DIFF.GT.RAD2) GO TO 13
C
C WING AND FUSELAGE ARE IN THE SAME PLANE
C
ZAVWNG=ZAVFUS
FUSWTH=Y(1)
GO TO 14
C
C CHECK FOR WING INTERSECTION WITH CENTER LINE
C
C
13 NFWAF=NEWAF+1
Y(NFWAF)=0.
X(NFWAF)=X(1)-Y(1)*SIN(SLOPLE(1))/COS(SLOPLE(1))
CHORD(NFWAF)=CHORD(1)-Y(1)*SIN(SLOPLE(1))/COS(SLOPLE(1))
X(1)=X(1)-(Y(1)-FUSWTH)*SIN(SLOPLE(1))/COS(SLOPLE(1))
CHORD(1)=CHORD(1)-(Y(1)-FUSWTH)*SIN(SLOPLE(1))/COS(SLOPLE(1))
Y(1)=FUSWTH
14 CONTINUE
NCOUNT=1
NFUSX]=NFUSXF-1

```

```

DRGD1060
DRGD1070
DRGD1080
DRGD1090
DRGD1100
DRGD1110
DRGD1120
DRGD1130
DRGD1140
DRGD1150
DRGD1160
DRGD1170
DRGD1180
DRGD1190
DRGD1200
DRGD1210
DRGD1220
DRGD1230
DRGD1240
DRGD1250
DRGD1260
DRGD1270
DRGD1280
DRGD1290
DRGD1300
DRGD1310
DRGD1320
DRGD1330
DRGD1340
DRGD1350
DRGD1360
DRGD1370
DRGD1380
DRGD1390
DRGD1400

```

```

C
C
C
FRONT AND REAR FUSELAGE MODIFICATION (STARTS)
AREAR=0.
AREAF=0.
DO 19 I=1,NFUSX1
IF (XFUS(I).LT.XLE) GO TO 15
IF (XFUS(I).GE.XTE) GO TO 16
GO TO 19
15 AREAF=AREAF+(YFUS(I)+YFUS(I+1))*(XFUS(I+1)-XFUS(I))/2.
XF=XFUS(I+1)-XFUS(I)
GO TO 19
16 AREAR=AREAR+(YFUS(I)+YFUS(I+1))*(XFUS(I+1)-XFUS(I))/2.
IF (NCOUNT.EQ.1) GO TO 17
GO TO 19
17 IF (XTE.GT.XFUS(I-1).AND.XTE.LT.XFUS(I)) GO TO 18
XR=XFUS(I)
NCOUNT=2
GO TO 19
18 AREAR=AREAR+(YFUS(I-1)+YFUS(I))*(XFUS(I)-XFUS(I-1))/2.
XR=XFUS(I-1)
NCOUNT=2
19 CONTINUE
A=2.*XF-2.*AREAF/FUSWTH
XFL(2)=XFUS(1)+A
XX=XFUS(NFUSXF)-XR
A=2.*XX-2.*AREAR/FUSWTH
XFT(2)=XFUS(NFUSXF)-A
XFL(1)=XFUS(1)
XFT(1)=XFUS(NFUSXF)
YF(1)=0.
YF(2)=FUSWTH
FRONT AND REAR FUSELAGE MODIFICATION (ENDS)
C
C
C
DRGD1410
DRGD1420
DRGD1430
DRGD1440
DRGD1450
DRGD1460
DRGD1470
DRGD1480
DRGD1490
DRGD1500
DRGD1510
DRGD1520
DRGD1530
DRGD1540
DRGD1550
DRGD1560
DRGD1570
DRGD1580
DRGD1590
DRGD1600
DRGD1610
DRGD1620
DRGD1630
DRGD1640
DRGD1650
DRGD1660
DRGD1670
DRGD1680
DRGD1690
DRGD1700
DRGD1710
DRGD1720
DRGD1730
DRGD1740
DRGD1750

```

```

C          J2 (POD DATA)
C
C          J3 (POD DATA)
C          J4 (FIN DATA)
C          J5 (CANARD DATA)
C
20 IF (J3.FQ.0) GO TO 22
C*****
DO 21 K=1,NP
  READ (5,58)(GARR,I=1,3)
  READ (5,58)(GARR,I=1,NPOLOR)
21 READ (5,58)(GARB,I=1,NPODOR)
C*****
22 IF (J4.FQ.0) GO TO 24
C*****
DO 23 K=1,NF
  READ (5,58)(GARR,I=1,8)
  READ (5,58)(GARR,I=1,NFINOR)
23 READ (5,58)(GARB,I=1,NFINOR)
C*****
24 IF (J5.EQ.0) GO TO 37
C*****
DO 26 K=1,NCAN
  READ (5,58)(XHT(K,I),YHT(K,I),ZHT(K,I),CHRHT(K,I),I=1,2)
  CHRHT(K,1)=CHRHT(K,1)+XHT(K,1)
  CHRHT(K,2)=CHRHT(K,2)+XHT(K,2)
  IF (NCANOR.LT.0) GO TO 25
  READ (5,58)(GARR,I=1,NCANOR)
  READ (5,58)(GARB,I=1,NCANOR)
  GO TO 26
25 NCANOR1=-NCANOR
  READ (5,58)(GARR,I=1,NCANOR1)

```

```

DRGD176J
DRGD177U
DRGD178O
DRGD179O
DRGD180U
DRGD181U
DRGD182U
DRGD183U
DRGD184O
DRGD185U
DRGD186J
DRGD187O
DRGD188U
DRGD189O
DRGD190U
DRGD191U
DRGD192O
DRGD193U
DRGD194U
DRGD195U
DRGD196J
DRGD197U
DRGD198U
DRGD199O
DRGD200U
DRGD201O
DRGD202O
DRGD203O
DRGD204O
DRGD205U
DRGD206O
DRGD207O
DRGD208O
DRGD209U
DRGD210U

```

```

DRGD2110
DRGD2120
DRGD2130
DRGD2140
DRGD2150
DRGD2160
DRGD2170
DRGD2180
DRGD2190
DRGD2200
DRGD2210
DRGD2220
DRGD2230
DRGD2240
DRGD2250
DRGD2260
DRGD2270
DRGD2280
DRGD2290
DRGD2300
DRGD2310
DRGD2320
DRGD2330
DRGD2340
DRGD2350
DRGD2360
DRGD2370
DRGD2380
DRGD2390
DRGD2400
DRGD2410
DRGD2420
DRGD2430
DRGD2440
DRGD2450

READ (5,58)(GARB,I=1,NCAN01)
READ (5,58)(GARB,I=1,NCAN01)
26 CONTINUE
C*****
WIDTH1=0.
WIDTH2=0.
IF (J2.FQ.0) GO TO 27
XLE=XHT(1,1)
XTE=CHR0HT(1,1)
CALL WIDTH(XFUS,YFUS,NFUSXF,XLE,XTE,WDTH1)
IF (NCAN.FQ.1) GO TO 27
XLF=XHT(2,1)
XTE=CHR0HT(2,1)
CALL WIDTH(XFUS,YFUS,NFUSXF,XLE,XTE,WDTH2)
27 CONTINUE
MAA=2
DO 28 I=1,2
XFUS(I)=XHT(1,I)
YFUS(I)=YHT(1,I)
28 ZFUS(I)=CHR0HT(1,I)
ZAVHT(1)=(ZHT(1,1)+ZHT(1,2))/2.
IF (NCAN.FQ.1) GO TO 29
NCONTL=0
IF (XHT(1,2).EQ.XHT(2,1).AND.YHT(1,2).EQ.YHT(2,1).AND.ZHT(1,2).EQ.ZHT(2,1).AND.CHR0HT(1,2).EQ.CHR0HT(2,1)) NCONTL=1
IF (NCONTL.EQ.0) GO TO 30
29 XFUS(1)=XFUS(1)-(XFUS(2)-XFUS(1))*(YFUS(1)-FUSWTH)/(YFUS(2)-YFUS(1))
ZFUS(1)=ZFUS(1)-(ZFUS(2)-ZFUS(1))*(YFUS(1)-FUSWTH)/(YFUS(2)-YFUS(1))
YFUS(1)=FUSWTH
IF (NCAN.FQ.1) GO TO 33
XFUS(3)=XHT(2,2)
YFUS(3)=YHT(2,2)
ZFUS(3)=CHR0HT(2,2)

```

```

ZAVHT(1)=(ZHT(1,1)+ZHT(1,2)+ZHT(2,2))/3.
NCAN=1
MAA=3
GO TO 33
30 DO 31 I=1,2
  XFUS1(I)=XHT(2,I)
  YFUS1(I)=YHT(2,I)
31 ZFUS1(I)=CHRDHT(2,I)
  XFUS1(I)=XFUS1(I)-(XFUS1(I)-XFUS1(1))*(YFUS1(1)-FUSWTH)/(YFUS1(2)-DRGD2540
  YFUS1(I))
  ZFUS1(I)=ZFUS1(I)-(ZFUS1(2)-ZFUS1(1))*(YFUS1(1)-FUSWTH)/(YFUS1(2)-DRGD2560
  YFUS1(1))
  YFUS1(I)=FUSWTH
ZAVHT(2)=(ZHT(2,1)+ZHT(2,2))/2.

C
C SUBROUTINE BREAK FINDS OUT BREAK LINES ON ONE LIFTING
C SURFACE DUE TO THE BREAK LINES ON THE OTHER LIFTING SURFACE
C
C BREAK LINES ON TAIL 1 DUE TO TAIL 2
C
C CALL BREAK(YFUS,YFUS,ZFUS,2,YFUS1,2,NN1)
C
C BREAK LINES ON TAIL 2 DUE TO TAIL 1
C
C CALL BREAK(XFUS1,YFUS1,ZFUS1,2,YFUS,NN1,NN2)
C
C BRFAK LINFs ON WING DUE TO TAIL 1
C
C CALL BREAK(X,Y,CHORD,NEWAF,YFUS,NN1,NEWAF1)
C
C BRFAK LINES ON WING DUE TO TAIL 2
C
C CALL BRFAK(X,Y,CHORD,NEWAF1,YFUS1,NN2,NEWAF2)
C
DRGD2460
DRGD2470
DRGD2480
DRGD2490
DRGD2500
DRGD2510
DRGD2520
DRGD2530
DRGD2540
DRGD2550
DRGD2560
DRGD2570
DRGD258J
DRGD2590
DRGD2600
DRGD2610
DRGD2620
DRGD2630
DRGD2640
DRGD2650
DRGD2660
DRGD2670
DRGD2680
DRGD2690
DRGD2700
DRGD2710
DRGD2720
DRGD2730
DRGD2740
DRGD2750
DRGD276J
DRGD2770
DRGD2780
DRGD2790
DRGD2800

```

```

C          BREAK LINES ON TAIL 1 DUE TO WING          DRGD2810
C          CALL BREAK(XFUS,YFUS,ZFUS,NN1,Y,NEWAF2,NN3) DRGD2820
C          ARFAK LINES ON TAIL 2 DUE TO WING          DRGD2830
C          CALL BREAK(XFUS1,YFUS1,ZFUS1,NN2,Y,NEWAF2,NN4) DRGD2840
C          NN2=NN3                                     DRGD2850
C          NEWAF=NEWAF2                                DRGD2860
C          WDTHT2=WDTH2/2.                             DRGD2870
C          DIFF=ABS(ZAVFUS-ZAVHT(2))                  DRGD2880
C          IF (DIFF.LT.WDTH2) GO TO 32                 DRGD2890
C          NN4=NN4+1                                    DRGD2900
C          YFUS1(NN4)=0.                                DRGD2910
C          XFUS1(NN4)=XFUS1(1)-(XFUS1(2)-XFUS1(1))*YFUS1(1)/(YFUS1(2)-YFUS1(1)) DRGD2920
C          ZFUS1(NN4)=ZFUS1(1)-(ZFUS1(2)-ZFUS1(1))*YFUS1(1)/(YFUS1(2)-YFUS1(1)) DRGD2930
C          NN4=NN4+1                                    DRGD2940
C          YFUS1(NN4)=FUSWTH                            DRGD2950
C          YFUS11=YFUS1(1)-FUSWTH                       DRGD2960
C          XFUS1(NN4)= US1(1)-(XFUS1(2)-XFUS1(1))*YFUS11/(YFUS1(2)-YFUS1(1)) DRGD2970
C          ZFUS1(NN4)=ZFUS1(1)-(ZFUS1(2)-ZFUS1(1))*YFUS11/(YFUS1(2)-YFUS1(1)) DRGD2980
C          NHT2=NN4                                      DRGD2990
C          GO TO 34                                      DRGD3000
C          32 IF (J2.NE.0) ZAVHT(2)=ZAVFUS              DRGD3010
C          GO TO 34                                      DRGD3020
C          33 CONTINUE                                  DRGD3030
C          ARFAK LINES ON WING DUE TO TAIL              DRGD3040
C          CALL BREAK(X,CHORD,NEWAF,YFUS,MAA,NEWAF2)    DRGD3050
C          BREAK LINES ON TAIL DUE TO WING              DRGD3060
C          DRGD3070
C          DRGD3080
C          DRGD3090
C          DRGD3100
C          DRGD3110
C          DRGD3120
C          DRGD3130
C          DRGD3140
C          DRGD3150

```



```

DRGD3160
DRGD3170
DRGD3180
DRGD3190
DRGD3200
DRGD3210
DRGD3220
DRGD3230
DRGD3240
DRGD3250
DRGD3260
DRGD3270
DRGD3280
DRGD3290
DRGD3300
DRGD3310
DRGD3320
DRGD3330
DRGD3340
DRGD3350
DRGD3360
DRGD3370
DRGD3380
DRGD3390
DRGD3400
DRGD3410
DRGD3420
DRGD3430
DRGD3440
DRGD3450
DRGD3460
DRGD3470
DRGD3480
DRGD3490
DRGD3500

CALL BREAK(XFUS,YFUS,ZFUS,MAA,Y,NEWAF2,NN2)
NEWAF=NEWAF2
34 CONTINUE
WDTH1=WDTH1/2.
DIFF=ARS(ZAVFUS-ZAVHT(1))
IF (DIFF.LT.WDTH1) GO TO 35
NN2=NN2+1
YFUS(NN2)=0.
XFUS(NN2)=XFUS(1)-(XFUS(2)-XFUS(1))*YFUS(1)/(YFUS(2)-YFUS(1))
ZFUS(NN2)=ZFUS(1)-(ZFUS(2)-ZFUS(1))*YFUS(1)/(YFUS(2)-YFUS(1))
NN2=NN2+1
YFUS(NN2)=FUSWTH
YFUS11=YFUS(1)-FUSWTH
XFUS(NN2)=XFUS(1)-(XFUS(2)-XFUS(1))*YFUS11/(YFUS(2)-YFUS(1))
ZFUS(NN2)=ZFUS(1)-(ZFUS(2)-ZFUS(1))*YFUS11/(YFUS(2)-YFUS(1))
NHT1= N2
GO TO 36
35 IF (J2.NE.0) ZAVHT(1)=ZAVFUS
36 CONTINUE

C
C SUBROUTINE ORDER ARRANGES ALL THE BREAK LINES IN ORDER
C FROM INBOARD TO OUTBOARD OF WING
C
C COMPARE FOR ALL THE OPTIONS
37 CONTINUE
CALL ORDER(X,Y,CHORD,NEWAF,XWLE,XWTE,YL,IWNG)
IF (NOPTON.EQ.2)OR(NCPTON.EQ.4) GO TO 38
IF (NCAN.NE.0) CALL ORDER(XFUS,YFUS,ZFUS,NN2,XHT1LE,XHT1TE,YHT1,IHDRGD3430
171)
IF (NCAN.EQ.2) CALL ORDER(XFUS1,YFUS1,ZFUS1,NN4,XHT2LE,XHT2TE,YHT2,IHDRGD3450
1,IHT2)
38 CONTINUE
NEWAF=IWNG
NC=NEWAF-1
IF (J2.NF.0) NC=NC+1

```

```

DRGD3510
DRGD3520
DRGD3530
DRGD3540
DRGD3550
DRGD3560
DRGD3570
DRGD3580
DRGD3590
DRGD3600
DRGD3610
DRGD3620
DRGD3630
DRGD.640
DRGD3650
DRGD3660
[ GD3670
DRGD3680
DRGD3690
DRGD3700
DRGD3710
DRGD3720
DRGD3730
DRGD3740
DRGD3750
DRGD3760
DRGD3770
DRGD3780
DRGD3790
LRGD3800
DRGD3810
DRGD3820
DRGD3830
DRGD3840
DRGD3850

IF (IHT1.NE.0) NC=NC+IHT1-1
IF (IHT2.NE.0) NC=NC+IHT2-1
WRITE (6,65) NC
KKK=0
IPANEL=1
C*****
READ (5,59) NCP1,NCP2,NCP3,NCP4
C*****
NPNLF=NCP1
NPNLW=NCP2
NPNLT1=NCP3
NPNT2=NCP4
NWMGP=0
NHT1P=0
NHT2P=0
NPNLF1=NPNLF
NPNLW1=NPNLW
NPNLT1=NPNLT1
NPNL2?=NPNLT2
IF (NOPTON.GT.2) GO TO 39

C
C FUSELAGE ANALYSIS
C
C*****
READ (5,60) (CPCWL(I),I=1,NPNLF1)
C*****
CPSWL(1)=C.
CPSWL(2)=100.

C
C SURROUTINE RITXY~ WRITES THE MODIFIED GEOMETRY DATA
C
C CALL RITXYZ(KKK,XFL,XFT,YF,CPCWL,NPNLF1,CPSWL,2,ZAVFUS)
C
C SURROUTINE PANEL DIVIDES A LIFTING SURFACE INTO AERODYNAMIC
C PANELS

```

```

C          CALL PANFL(XFL,YF,XFT,NPNLF1,2,ZAVFUS)
          IPANEL=LIPANEL+1
C
C          WING ANALYSIS
C
          CRFF=XWTE(1)-XWLE(1)
          39 IST=1
          WNGPNL=IPANEL
          NEWAF1=NEWAF-1
C*****
          READ (5,60) (CPCWL(I),I=1,NPNLW1)
C*****
          HALFR=YL(NEWAF)
          W1=(YL(NWAF)-YL(1))/10.
          IF (ZAVFUS.NF.ZAVWNG) GO TO 42
          40 DO 41 I=1,NEWAF1
C
C          SURROUTINE NEWCOR OUTPUTS THE INBOARD AND OUTBOARD CHORD
          OF LIFTING SURFACE UNDER CONSIDERATION
C
          CALL NEWCOR(XWLE,XWTE,YL,I,XWLE1,XWTE1,YL1)
          INT=(YL(I+1)-YL(I))/W1+0.5
          IF (INT.EQ.0) INT=.
C
C          SUBROUTINE GNCCWL FINDS OUT THE CONSTANT PERCENT STREAMWISE
          LINES (CPSWL) FOR THE LIFTING SURFACE
C
          CALL GNCCWL(INT,CPSWL,1.)
          INT1=INT+1
          CALL RIITXYZ(KKK,XWLE1,XWTE1,YL1,CPCWL,NPNLW1,CPSWL,INT1,ZAVWNG)
          CALL PANEL(XWLE1,YL1,XWTE1,NPNLW1,INT1,ZAVWNG)
          IPANEL=LIPANEL+1
          NWNNGP=NWNNGP+INT1-1
          41 CONTINUE

```

```

DRGD3860
DRGD3870
DRGD3880
DRGD3890
DRGD3900
DRGD3910
DRGD3920
DRGD3930
DRGD3940
DRGD3950
DRGD3960
DRGD3970
DRGD3980
DRGD3990
DRGD4000
DRGD4010
DRGD4020
DRGD4030
DRGD4040
DRGD4050
DRGD4060
DRGD4070
DRGD4080
DRGD4090
DRGD4100
DRGD4110
DRGD4120
DRGD4130
DRGD4140
DRGD4150
DRGD4160
DRGD4170
DRGD4180
DRGD4190
DRGD4200

```

```

          GO TO 43
42 CPSWL(1)=0.
   CPSWL(2)=100.
   CALL NEWCOR(XWLE,XWTF,YL,1,XWLE1,XWTE1,YL1)
   CALL RITXYZ(KK,XWLE1,XWTE1,YL1,CPCWL,NPNLW1,CPSWL,2,ZAVWNG)
   CALL PANEL(XWLE1,YL1,XWTE1,NPNLW1,2,ZAVWNG)
   IPANEL=LIPANEL+1
   IST=2
   NWNGP=1
   GO TO 40
43 CONTINUE
   IF (NOPTCN.EQ.2.OR.NOPTON.EQ.4) GO TO 48
   C
   C
   C      HORIZONTAL TAIL ANALYSIS
   C
   C
   C      IST=1
   C      HALFRI=YHT1(IHT1)
   C      IHT1=IHT1-1
   C      HTIPNL=IPANEL
   C      *****
   C      READ (5,60) (CPCWL(I),I=1,NPNL11)
   C      *****
   C      IF (NOPTON.LE.2.AND.ZAVFUS.NE.ZAVHT(1)) GO TO 51
   C      *****
44 DO 45 I=IST,IHT11
   INT=(YHT1(I+1)-YHT1(I))/WI+0.5
   CALL NEWCOR(XHTILE,XHTITE,YHT1,I,XHLE,XHTE,YHLE)
   IF (INT.EQ.0) INT=1
   INTI=INT+1
   CALL GNCCWL(INT,CPSWL,1.)
   CALL RITXYZ(KK,XHLE,XHTE,YHLE,CPCWL,NPNL11,CPSWL,INTI,ZAVHT(I))
   CALL PANEL(XHLF,YHLE,XHTE,NPNL11,INTI,ZAVHT(1))
   NHTIP=NHTIP+INTI-1
45 IPANEL=LIPANEL+1
   IF (NCAN.NE.2) GO TO 48
   IST=1

```

```

DRGD4210
DRGD4220
DRGD4230
DRGD4240
DRGD4250
DRGD4260
DRGD4270
DRGD4280
DRGD4290
DRGD4300
DRGD4310
DRGD4320
DRGD4330
DRGD4340
DRGD4350
DRGD4360
DRGD4370
DRGD4380
DRGD4390
DRGD4400
DRGD4410
DRGD4420
DRGD4430
DRGD4440
DRGD4450
DRGD4460
DRGD4470
DRGD4480
DRGD4490
DRGD4500
DRGD4510
DRGD4520
DRGD4530
DRGD4540
DRGD4550

```

```

HALFR2=YHT2(IHT2)
HT2PNL=IPANFL
*****
READ (5,60) (CPCWL(I),I=1,NPNL22)
*****
IHT21=IHT2-1
IF (NOPTON.LE.2.AND.ZAVFUS.NE.ZAVHT(2)) GO TO 52
46 DO 47 I=1ST,IHT21
   INT=(YHT2(I+1)-YHT2(I))/W1+0.5
   CALL NEWCOR(XHT2LE,XHT2TE,YHT2,I,XHLE,XHTE,YHLE)
   IF (INT.EQ.0) INT=1
   INT1=INT+1
   CALL GNCCWL(INT,CPSWL,1.)
   CALL RITXYZ(KKK,XHLE,XHTE,YHLE,CPCWL,NPNL22,CPSWL,INT1,ZAVHT(2))
   CALL PANEL(XHLE,YHLE,XHTE,NPNL22,INT1,ZAVHT(2))
   NHT2P=NHT2P+INT1-1
47 IPANFL=LAPANFL+1
48 CONTINUE
   LSTPNL=L PANEL
*****
READ (5,60) CCREFF
*****
IF (CCRFF.NE.0.) CREF=CCRFF
IF (RFFA.NF.0.) GO TO 50
IM=HT1PNL-1
IF (HT1PNL.LE.0) IM=L PANEL
HALFSW=0.
DO 49 I=WNGPNL,IM
49 HALFSW=HALFSW+AREA(I)
RFFA=2.*HALFSW
WRITE (6,66) RFFA,CREF
RETURN
50 HALFSW=RFFA/2.
WRITE (6,66) RFFA,CREF
RETURN

```

```

DRGD4560
DRGD4570
DRGD4580
DRGD4590
DRGD4600
DRGD4610
DRGD4620
DRGD4630
DRGD4640
DRGD4650
DRGD4660
DRGD4670
DRGD4680
DRGD4690
DKGD4700
DRGD4710
DRGD4720
DRGD4730
DRGD4740
DRGD4750
DKGD4760
DKGD4770
DKGD4780
DRGD4790
DRGD4800
DRGD4810
DRGD4820
DRGD4830
DRGD4840
DRGD4850
DRGD4860
DRGD4870
DRGD4880
DRGD4890
DRGD4900

```

```

51 CPSWL(1)=0.
   CPSWL(2)=100.
   CALL NEWCOR(XHT1LE,XHT1TE,YHT1,1,XHLE,XHTE,YHLE)
   CALL RITXYZ(KKK,XHLE,XHTE,YHLE,CPCWL,NPNL11,CPSWL,2,ZAVHT(1))
   CALL PANEL(XHLE,YHLE,XHTE,NPNL11,2,ZAVHT(1))
   IST=2
   NHTIP=1
   GO TO 44
52 CPSWL(1)=0.
   CPSWL(2)=100.
   CALL NEWCOR(XHT2LE,XHT2TE,YHT2,1,XHLE,XHTE,YHLE)
   CALL RITXYZ(KKK,XHLE,XHTE,YHLE,CPCWL,NPNL22,CPSWL,2,ZAVHT(2))
   CALL PANEL(XHLE,YHLE,XHTE,NPNL22,2,ZAVHT(2))
   IST=2
   NHT2P=1
   GO TO 46
53 WRITE (6,61)
   RETURN
54 WRITE (6,62)
   RETURN
55 WRITE (6,63)
   RETURN
56 WRITE (6,64)
   RETURN
57 FORMAT (24I3)
58 FORMAT (10F7.3)
59 FORMAT (4I2)
60 FORMAT (8F10.5)
61 FORMAT (90HTHIS TEST CASE HAS FUSELAGE AND HORIZONTAL TAIL. CHANGED
   1 HORIZONTAL TAIL DATA TO WING DATA. )
62 FORMAT (89HTHIS TEST CASE HAS ONLY FUSELAGE WHICH DOES NOT MAKE AN
   1Y SFNSF. FIRST DATA CARD IS WRONG. )
63 FORMAT (82HTHIS TEST CASE HAS ONLY HORIZONTAL TAIL. CHANGE HORIZON
   1TAL TAIL DATA TO WING DATA. )
64 FORMAT (79HTHIS TEST CASE DOES NOT HAVE ANY AERODYNAMIC SURFACE. FDRGD525U
DRGD4910
DRGD4920
DRGD4930
DRGD4940
DRGD4950
DRGD4960
DRGD4970
DRGD4980
DRGD4990
DRGD5000
DRGD5010
DRGD5020
DRGD5030
DRGD5040
DRGD5050
DRGD5060
DRGD5070
DRGD5080
DRGD5090
DRGD5100
DRGD5110
DRGD5120
DRGD5130
DRGD5140
DRGD5150
DRGD5160
DRGD5170
DRGD5180
DRGD5190
DRGD5200
DRGD5210
DRGD5220
DRGD5230
DRGD5240
DRGD5250

```

```

11RST DATA CARD IS WRNG.      )
65 FORMAT (1H1,/,11X,45H*****DRGD5260
1*,/,11X,32H* GEOMETRY DATA IS DIVIDED IN TO,12,11H SECTIONS *,/,11DRGD5270
2X,45H*****DRGD5280
66 FORMAT (10X,10HREF. AREA=,E12.5,/,10X,11HREF. CHORD=,E12.5)
END
DRGD5290
DRGD5300
DRGD5310

```

```

GNCCU010
GNCCU020
GNCCU030
GNCCU040
GNCCU050
GNCCU060
GNCCU070
GNCCU080
GNCCU090
GNCCU100
GNCCU110
GNCCU120
GNCCU130
GNCCU140
GNCCU150

SUBROUTINE GNCCWL(NPWL,CPCWL,A)
  GN*N*C*C*W*L
  .....
  SURROUTINE GNCCWL FINDS OUT THE CONSTANT PERCENT STREAMWISE
  LINES FOR THE LIFTING SURFACE
  .....
  DIMENSION CPCWL(1)
  CPCWL=100./FLOAT(NPWL)
  CPCWL(1)=0.
  CPCWL(2)=CPCWL/A
  CPCWL(NPWL+1)=100.
  DO 1 I=3,NPWL
    1 CPCWL(I)=CPCWL(I-1)+CPCWL
  RETURN
  END

```



```

C.....SURROUTINE MAXVLU(Y,N,YMAX,KK)
C.....M*A*X*V*L*U
C.....
C.....SURROUTINE MAXVLU FINDS THE VALUE OF THE LARGEST ELEMENT OF
C.....ARRAY Y
C.....
C.....DIMENSION Y(1)
C.....I=1
C.....NN=N+1
C.....1 IF (Y(I)).GT.Y(I+1)) GO TO 2
C.....I=I+1
C.....IF (I.EQ.NN) GO TO 2
C.....GO TO 1
C.....2 YMAX=Y(I)
C.....KK=I
C.....RETURN
C.....END
MAXV0010
MAXV0020
MAXV0030
MAXV0040
MAXV0050
MAXV0060
MAXV0070
MAXV0080
MAXV0090
MAXV0100
MAXV0110
MAXV0120
MAXV0130
MAXV0140
MAXV0150
MAXV0160
MAXV0170

```

```

C
C.....
C.....
C.....
C.....
      SUBROUTINE NEWARK(X1,X2,Y1,Y2,C1,C2,YY,XNEW,YNEW,CNEW)
          N*E*W**R**K
C.....
C.....
C.....
      SUBROUTINE NEWARK FINDS OUT THE COORDINATES OF BREAK LINES
C.....
      YY1=(YY-Y1)/(Y2-Y1)
      X21=X2-X1
      XNEW=X1+X21*YY1
      C21=C2-C1
      CNEW=C1+C21*YY1
      YNEW=YY
      P=TURN
      END
      NBRK0010
      NBRK0020
      NBRK0030
      NBRK0040
      NBRK0050
      NBRK0060
      NBRK0070
      NBRK0080
      NBRK0090
      NBRK0100
      NBRK0110
      NBRK0120
      NBRK0130

```



```

NPNL0010
NPNL0020
NPNL0030
NPNL0040
NPNL0050
NPNL0060
NPNL0070
NPNL0080
NPNL0090
NPNL0100
NPNL0110
NPNL0120
NPNL0130
NPNL0140
NPNL0150
NPNL0160
NPNL0170
NPNL0180
NPNL0190
NPNL0200
NPNL0210
NPNL0220
NPNL0230
NPNL0240
NPNL0250
NPNL0260
NPNL0270
NPNL0280
NPNL0290
NPNL0300
NPNL0310
NPNL0320
NPNL0330
NPNL0340
NPNL0350

SUBROUTINE NEWPNL
      N*E*W*P*N*L
C.....
C SURROUTINE NEWPNL USES THE INPUT DATA FORMAT OF THE PRESENT
C PROGRAM FOR FINDING OUT AERODYNAMIC PANELS
C
C      KONT=1 FUSELAGE DATA
C      KONT=2 WING DATA
C      KONT=3 HORIZONTAL TAIL 1 DATA
C      KONT=4 HORIZONTAL TAIL 2 DATA
C
C.....
C COMMON/CNTR0L/ LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WGNPNL,HT1PNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHT1P,NHT2P,HALFB,ALPH,HALFB1,HALFB2,NCPSWL,NCPWNG,MAX
COMMON XCG(300),XCP(300),YCP(300),ZCP(300),AREA(300),AMASS(300),
1 XN(300,4),YN(300,4),ZN(300,4),BPRIM(300,4)
COMMON/PNL/CPCWL(35),CPSWL(35),IPANEL
DIMENSION XXL(2),YL(2),XXT(2)
INTEGFR WGNPNL,HT1PNL,HT2PNL
KKK=0
IPANEL=1
NWNGP=0
NHT1P=0
NHT2P=0
C*****
READ (5,8) NCP1,NCP2,NCP3,NCP4
READ (5,8) NC
C*****
NCPFUS=NCPI-1
NCPWNG=NCP2-1
NCPHT1=NCP3-1
NCPHT2=NCP4-1
WRITE (6,9) NC
KONT=0

```

```

NPNL0360
C*****
DO 6 KK=1,NC
READ (5,8) NCP SWL,KONTL
IF (KONTL.EQ.1) NCP SWL=NCP1
IF (KONTL.EQ.2) NCP SWL=NCP2
IF (KONTL.EQ.3) NCP SWL=NCP3
IF (KONTL.EQ.4) NCP SWL=NCP4
READ (5,10) (XXL(I),XXT(I),YL(I),I=1,2),Z
IF (KONTL.NE.KONTL) READ (5,10) (CPCWL(I),I=1,NCPCWL)
READ (5,10) (CPSWL(K),K=1,NCPSWL)
C*****
IF (KONTL.EQ.2) GO TO 1
GO TO 2
1 N WNGP=N WNGP+NCP SWL-1
  HALFR=YL(2)
2 IF (KONTL.EQ.3) NHT1P=NHT1P+NCP SWL-1
  IF (KONTL.EQ.4) NHT2P=NHT2P+NCP SWL-1
  IF (KONTL.EQ.3) HALFB1=YL(2)
  IF (KONTL.EQ.4) HALFB2=YL(2)
C
C   SUBROUTINE RITXYZ WRITES THE GEOMETRY DATA
C
CALL RITXYZ(KK,XXL,XXT,YL,CPCWL,NCP SWL,CPSWL,NCP SWL,Z)
IF (KONT.LT.2.AND.KONTL.EQ.2) GO TO 3
GO TO 4
3 CREF=XXT(1)-XXL(1)
  WNGPNI=IPANFL
GO TO 5
4 IF (KONT.LT.3.AND.KONTL.EQ.3) HT1PNI=IPANFL
  IF (KONT.LT.4.AND.KONTL.EQ.4) HT2PNI=IPANFL
C
C   SUBROUTINE PANEL DIVIDES A LIFTING SURFACE INTO AERODYNAMIC
C   PANELS
C
5 CALL PANEL(XXL,YL,XXT,NCP SWL,NCP SWL,Z)
NPNL0370
NPNL0380
NPNL0390
NPNL0400
NPNL0410
NPNL0420
NPNL0430
NPNL0440
NPNL0450
NPNL0460
NPNL0470
NPNL0480
NPNL0490
NPNL0500
NPNL0510
NPNL0520
NPNL0530
NPNL0540
NPNL0550
NPNL0560
NPNL0570
NPNL0580
NPNL0590
NPNL0600
NPNL0610
NPNL0620
NPNL0630
NPNL0640
NPNL0650
NPNL0660
NPNL0670
NPNL0680
NPNL0690
NPNL0700

```

```

IPANEL=L PANEL+1
KONT=KONTL
6 CONTINUF
  IM=I+IPNL-1
  IF (HTIPNL.LE.0) IM=L PANEL
  HALFSW=0.
  DO 7 I=WGNPNL,IM
    HALFSW=HALFSW+AREA(I)
  READ (5,10) SREF,CCRFF
  IF (SRFF.NE.0.) HALFSW=SREF/2.
  IF (CCRFF.NF.0.) CREF=CCRFF
  LSTPNL=L PANEL
  SW=2.*HALFSW
  WRITE (6,11) SW
  WRITE (5,12) CREF
  RETURN
3 FORMAT (4I2)
9 FORMAT (1H1,/,11X,45H*****
1*,/,11X,32H* GEOMETRY DATA IS DIVIDED IN TO,I2,11H SECTIONS *,/,11NPNL0880
2X,45H*****
10 FORMAT (8F10.5)
11 FORMAT (10X,10HREF. AREA=,E12.5)
12 FORMAT (10X,11HREF. CHORD=,E12.5)
END
NPNL0710
NPNL0720
NPNL0730
NPNL0740
NPNL0750
NPNL0760
NPNL0770
NPNL0780
NPNL0790
NPNL0800
NPNL0810
NPNL0820
NPNL0830
NPNL0840
NPNL0850
NPNL0860
NPNL0870
NPNL0880
NPNL0890
NPNL0900
NPNL0910
NPNL0920
NPNL0930
NPNL0940

```

```

C..... SUBROUTINE ORDER(X,Y,CHORD,INTL,XWLE,XWTE,YL,II) ORDR0010
C..... O*R*D*E*R ORDR0020
C..... SUBROUTINE ORDER ARRANGES ALL THE BREAK LINES IN ORDER FROM ORDR0030
C..... INBOARD TO OUTBOARD ORDR0040
C..... DIMENSION X(1),Y(1),CHORD(1),XWLE(1),XWTE(1),YL(1) ORDR0050
C..... INTL=INTL+1 ORDR0060
C..... DO 2 I=1,INT1 ORDR0070
C..... JJ=1 ORDR0080
C..... YL(II)=Y(I) ORDR0090
C..... XWLF(II)=X(I) ORDR0100
C..... XWTF(II)=CHORD(I) ORDR0110
C..... DO 1 J=2,INTL ORDR0120
C..... IF (YL(I).LE.Y(J)) GO TO 1 ORDR0130
C..... YL(II)=Y(J) ORDR0140
C..... XWLE(II)=X(J) ORDR0150
C..... XWTE(II)=CHORD(J) ORDR0160
C..... JJ=J ORDR0170
C..... 1 CONTINUE ORDR0180
C..... Y(JJ)=1.E06 ORDR0190
C..... 2 CONTINUE ORDR0200
C..... I=0 ORDR0210
C..... DO 3 J=1,INTL ORDR0220
C..... IF (XWLE(J).EQ.XWLE(J+1).AND.YL(J).EQ.YL(J+1).AND.XWTE(J).EQ.XWTE(J+1)) GO TO 3 ORDR0230
C..... I=I+1 ORDR0240
C..... X(I)=XWLE(J) ORDR0250
C..... Y(I)=YL(J) ORDR0260
C..... CHORD(I)=XWTE(J) ORDR0270
C..... 3 CONTINUE ORDR0280
C..... II=I ORDR0290
C..... DO 4 J=1,II ORDR0300
C..... XWLF(J)=X(J) ORDR0310
C..... YL(J)=Y(J) ORDR0320
C..... ORDR0330
C..... ORDR0340
C..... ORDR0350

```

ORDK0360
ORDR0370
ORDK0380

4 XWTF(J)=CHORD(J)
RFTIIRN
END


```

C.....SURROUTINE PANEL DIVIDES A LIFTING SURFACE INTO AERODYNAMIC
C.....PANELS
C.....COMMON/CNTR0L/ LPANEL,NEAMAX,NCMTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HTIPNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHT1P,NHT2P,HALFB,ALPH,HALFB1,HALFB2,NCPSSL,NCPWNG,MAX
COMMON XCG(300),YCP(300),ZCP(300),AREA(300),AMASS(300),
1 XN(300,4),YN(300,4),ZN(300,4),BPRIM(300,4)
COMMON/PNL/CPCWL(35),CPSWL(35),IPANEL
DIMENSION XXL(2),YL(2),XXT(2)
INTEGER WNGPNL,HTIPNL,HT2PNL
DIMENSION C(2),X(35,35),Y(35,35),SLOPE(35),XL(2,35)
NSW1=NSW-1
NCW1=NCW-1
DO 1 I=1,2
C(I)=XXT(I)-XXL(I)
DO 1 J=1,NCW
1 XL(I,J)=XXL(I)+CPCWL(J)*C(I)/100.
SPAN=YL(2)-YL(1)
DO 2 J=1,NCW
2 SLOPE(J)=(XL(2,J)-XL(1,J))/SPAN
DO 3 K=1,NSW
YK=CPSWL(K)*SPAN/100.
DO 3 J=1,NCW
Y(J,K)=YK+YL(1)
X(J,K)=XL(1,J)+SLOPE(J)*(Y(J,K)-YL(1))
3 CONTINUE
DO 6 K=1,NSW1
DO 6 J=1,NCW1
NPANEL=(K-1)*NCW1+J-1+IPANEL
DO 5 I=1,4
Z:(NPANEL,I)=Z

```

```

PANLU010
PANLU020
PANLU030
PANLU040
PANLU050
PANLU060
PANLU070
PANLU080
PANLU090
PANLU100
PANLU110
PANLU120
PANLU130
PANLU140
PANLU150
PANLU160
PANLU170
PANLU180
PANLU190
PANLU200
PANLU210
PANLU220
PANLU230
PANLU240
PANLU250
PANLU260
PANLU270
PANLU280
PANLU290
PANLU300
PANLU310
PANLU320
PANLU330
PANLU340
PANLU350

```

```

KI1=K+I-1
KI3=K+I-3
IF (I.LE.2) GO TO 4
XN(NPANEL,I)=X(J+1,KI3)
YN(NPANEL,I)=Y(J+1,KI3)
APRIM(NPANEL,I)=SLOPE(J+1)
GO TO 5
4 XN(NPANEL,I)=X(J,KI1)
  YN(NPANEL,I)=Y(J,KI1)
  APRIM(NPANEL,I)=SLOPE(J)
5 CONTINUE
  A1=X(J+1,K)-X(J,K)
  A2=X(J+1,K+1)-X(J,K+1)
  R=Y(J,K+1)-Y(J,K)
  YBAR=R*(A1+2.*A2)/(3.*(A1+A2))
  CBAR=A1+(A2-A1)*YBAR/R
  XBAR=X(J,K)+YBAR*(X(J,K+1)-X(J,K))/B
  FE=X(J+1,K+1)-X(J+1,K)
  AE=A1+FE
  RC=X(J,K+1)-X(J,K)
  XK=(AE*AE+2.*AE*A1-A1*FE-8C*BC)/(3.*(A1+A2))
  XCG(NPANEL)=X(J,K)+XK
  XCP(NPANEL)=XBAR+0.95*CRAR
  YCP(NPANEL)=Y(J,K)+YRAR
  ZCP(NPANEL)=Z
  ARFA(NPANEL)=(A1+A2)/2.*B
6 CONTINUE
  LPANEL=NPANEL
  RETURN
  END

```

```

PANLO360
PANLO370
PANLO380
PANLO390
PANLO400
PANLO410
PANLO420
PANLO430
PANLO440
PANLO450
PANLO460
PANLO470
PANLO480
PANLO490
PANLO500
PANLO510
PANLO520
PANLO530
PANLO540
PANLO550
PANLO560
PANLO570
PANLO580
PANLO590
PANLO600
PANLO610
PANLO620
PANLO630
PANLO640
PANLO650

```

```

SUBROUTINE RITXYZ(KK,XXL,XXT,YL,CPCWL,NCPCWL,CPSWL,NCPSWL,Z)
C.....R*I*T*X*Y*Z
C.....KITX0020
C.....KITX0030
C.....KITX0040
C.....KITX0050
C.....KITX0060
C.....KITX0070
C.....KITX0080
C.....KITX0090
C.....KITX0100
C.....KITX0110
C.....KITX0120
C.....KITX0130
C.....KITX0140
C.....KITX0150
C.....KITX0160
C.....KITX0170
C.....KITX0180
C.....KITX0190
C.....KITX0200
C.....KITX0210
C.....KITX0220
C.....KITX0230
SUBROUTINE RITXYZ(KK,XXL,XXT,YL,CPCWL,NCPCWL,CPSWL,NCPSWL,Z)
R*I*T*X*Y*Z
SUBROUTINE RITXYZ WRITES THE GEOMETRY DATA
DIMENSION XXL(1),XXT(1),YL(1),CPCWL(1),CPSWL(1)
KK=KK+1
WRITE (6,1) KK
WRITE (6,2)
WRITE (6,3) (XXL(I),XXT(I),YL(I),Z,I=1,2)
WRITE (6,4) NCPCWL,(CPCWL(I),I=1,NCPCWL)
WRITE (6,5) NCPSWL,(CPSWL(I),I=1,NCPSWL)
1 FORMAT (1H0,10X,21HDEFINITION OF SECTION,I2,/,11X,23H*****RITX0130
1*****RITX0140
2 FORMAT (1H0,10X,14HX-LEADING EDGE,5X,15HX-TRAILING EDGE,5X,14HY-LEADING EDGE,5X,14HY-LEADING EDGE,12X,1HZ)
3 FORMAT (4(10X,F11.5))
4 FORMAT (10X,10HTHERE ARE ,I2,36H CONSTANT PERCENT CHORDWISE LINES RITX0180
1AT,/,10X,(12F10.3))
5 FORMAT (10X,10HTHERE ARE ,I2,37H CONSTANT PERCENT STREAMWISE LINES RITX0200
1 AT,/,10X,(12F10.3))
RETURN
END

```

```

SURROUTINE WIDTH, <FUS,YFUS,NFUS,>.F,XLE,XTE,FUSWTH)
C.....W*I*D*T*H
C.....
C.....SURROUTINE WIDTH FINDS OUT THE AVERAGE FUSELAGE WIDTH BETWEEN
C.....THE GIVEN TWO STATIONS
C.....
C.....DIMENSION XFUS(1),YFUS(1)
K=0
SUM=0.
DO 1 J=1,NFUSXF
IF (XFUS(J)).LT.XLE.OR.XFUS(J).GT.XTE) GO TO 1
K=K+1
SUM=SUM+YFUS(J)
1 CONTINUE
IF (SUM.EQ.0.) GO TO 2
FUSWTH=SUM/FLOAT(K)
RETURN
2 FUSWTH=0.
RETURN
END
WIDT0010
WIDT0020
WIDT0030
WIDT0040
WIDT0050
WIDT0060
WIDT0070
WIDT0080
WIDT0090
WIDT0100
WIDT0110
WIDT0120
WIDT0130
WIDT0140
WIDT0150
WIDT0160
WIDT0170
WIDT0180
WIDT0190
WIDT0200

```

```

      OPROGRAM AERELA(INPUT=201,OUTPUT=201,TAPE5=INPUT,TAPE6=OUTPUT,
      1 TAPE7=1001,TAPE20=401)
      .....
      C COMPUTER PROGRAM FOR CALCULATING ALPHA- AND Q- STABILITY
      C DERIVATIVES AND INDUCED DRAG FOR THIN ELASTIC AEROPLANES AT
      C SURSONIC AND SUPERSONIC SPEEDS
      C
      C MAIN INPUT DATA
      C N=NUMBER OF PANELS OR NUMBER OF UNIT LOADING POINTS FOR (C)
      C M=MAXIMUM NUMBER OF ELASTIC AXIS END-POINTS
      C IF NCNTL=0T (A),(C) AND ALL DERIVATIVES ARE COMPUTED
      C IF NCNTL=1, ONLY (A) AND RIGID DERIVATIVES ARE COMPUTED
      C IF NCNTL=2, ONLY (C) IS COMPUTED AND PRINTED OUT
      C IF NCNTL=3, (A) IS COMPUTED, (C) IS READ FROM TAPE AND ALL
      C THE DERIVATIVES ARE CALCULATED
      C IF NCNTL=4, (A),(C) AND ALL DERIVATIVES ARE COMPUTED (PRINTS (C))
      C
      C THE SUBROUTINE FOR GENERATING STRUCTURAL INFLUENCE COEFFICIENT
      C MATRIX CANNOT HANDLE A CONFIGURATION WITH CANARD SURFACE
      C
      C **AERELA USES DATA PROCESSED IN AEREA AND STORED ON TAPE20
      C TO GENERATE THE A-MATRIX. ELASTIC AXIS DATA IS READ FROM CARDS
      C TO CREATE THE C-MATRIX. ALTITUDE DATA IS READ FROM CARDS FOR
      C SOLUTION OF THE R-MATRIX.
      C
      C **IN THIS VERSION OF AEREL, ONLY ONE FULL MATRIX RESIDES IN
      C CORE AT ANY ONE TIME. THE OTHERS RESIDE ON DISC, STORED
      C BY ROWS.
      C
      C **OPTIMIZED BY COMPUTER SCIENCES CORPORATION FOR NASA LANGLEY
      C RESEARCH CENTER.
      C
      C MODIFICATIONS BY C.BOLZ AND B.PARKER JUNE 1972.

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ARLAU010
ARLA0020
ARLAU030
ARLAU040
ARLAU050
ARLA0060
ARLA0070
ARLA0080
ARLA0090
ARLA0100
ARLAU110
ARLAU120
ARLAU130
ARLAU140
ARLAU150
ARLAU160
ARLAU170
ARLAU180
ARLAU190
ARLAU200
ARLA0210
ARLAU220
ARLAU230
ARLAU240
ARLAU250
ARLAU260
ARLAU270
ARLAU280
ARLAU290
ARLAU300
ARLAU310
ARLAU320
ARLAU330
ARLA0340
ARLAU350

```

```

C.....ARLAU360
COMMON IND(1)
COMMON/CNTROL/LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HT1PNL,HT2PNL,NCPT1,NCPT2,NWNGP,
2 NHT1P,NHT2P, HALFB,ALPH,HALFB1,HALFB2,NCPSWL,NCPWNG,MAX
DIMENSION D(1)
EQUIVALENCE (IND(1),D(1))
COMMON/INDMS/ IA,IR,IC
DIMENSION DUM1(25)
EQUIVALENCE (DUM1(1),LPANEL)
EQUIVALENCE (NEAMAX,M)
INTEGER WNGPNL,HT1PNL,HT2PNL
CALL OPENMS(20,IND,12,0)
CALL READMS(20,LPANEL,25,1)
N=LPANEL
INL=1
NN=N*N
IA=1
IB=N+IA
IC=N+IB

C**PARTITION COMMON FOR PROBLEM ARRAYS.
IRASE=13
IXP=IRASE+3*N+1
IYP=IXP+N
IZP=IYP+N
IXG=IZP+N
IAR=IXG+N
IAM=IAR+N
IXN=IAM+N

N4=4*N
IYN=IXN+N4
IZN=IYN+N4
I9P=IZN+N4

C.....ARLAU370
ARLAU380
ARLAU390
ARLAU400
ARLAU410
ARLAU420
ARLAU430
ARLAU440
ARLAU450
ARLAU460
ARLAU470
ARLAU480
ARLAU490
ARLAU500
ARLAU510
ARLAU520
ARLAU530
ARLAU540
ARLAU550
ARLAU560
ARLAU570
ARLAU580
ARLAU590
ARLAU600
ARLAU610
ARLAU620
ARLAU630
ARLAU640
ARLAU650
ARLAU660
ARLAU670
ARLAU680
ARLAU690
ARLAU700

```

```

ICP=IRP+N4
IMM=ICP+N
IWA=IMM+NN
IWR=IWA+N
C**READ PROBLEM INPUT FROM DISC.
      OCALL DISCRD(IND(1),D(IXP),D(IYP),D(IZP),D(IXG),D(IAR),D(IAM),
      1 D(IXN),D(IYN),D(IZN),D(IRP),D(ICP),N)
C
C**CHANGE DISC KEY. RECORD NO.1 WILL NOW BE THE FIRST ROW OF MATRIX A.
      N3=3*N+1
      CALL STINDX(20,IND(IBASE),N3)
C
C**AERODYNAMIC MATRIX. IWA AND IWR ARE FOR WORKING STORAGE.
      IF (NCNTL.EQ.2) GO TO 2
C
C LINK LINK11 CALCULATES THE AERODYNAMIC INFLUENCE COEFFICIENT
C MATRIX, RIGID DERIVATIVES, THE RIGID INDUCED DRAG PARAMETER
C (CDI/(CL*CL)) AND THE PRESSURE COEFFICIENTS
C
      OCALL LINK11(IND(IBASE),D(IXP),D(IYP),D(IZP),D(IXG),D(IAR),D(IAM),
      1 D(IXN),D(IYN),D(IZN),D(IRP),D(IWA),D(IWB),D(ICP),D(IMM),N)
      IF (NCNTL.EQ.1) GO TO 3
      2 M1=M-1
      NM=M*N
      INC=1
      INPHUP=IMM
      INPHUM=INPHUP+MM
      INPHUT=INPHUM+MM
      INXEA=INPHUT+MM
      INYFA=INXEA+M
      INPHIP=INYEA+M
      INPHIM=INPHIP+M
      INPHIT=INPHIM+M
      INFI=INPHIT+M
      INGJ=INFI+M1

```

```

ARLA0710
ARLA0720
ARLA0730
ARLA0740
ARLA0750
ARLA0760
ARLA0770
ARLA0780
ARLA0790
ARLA0800
ARLA0810
ARLA0820
ARLA0830
ARLA0840
ARLA0850
ARLA0860
ARLA0870
ARLA0880
ARLA0890
ARLA0900
ARLA0910
ARLA0920
ARLA0930
ARLA0940
ARLA0950
ARLA0960
ARLA0970
ARLA0980
ARLA0990
ARLA1000
ARLA1010
ARLA1020
ARLA1030
ARLA1040
ARLA1050

```

```

ARL1060
ARL1070
ARL1080
ARL1090
ARL1100
ARL1110
ARL1120
ARL1130
ARL1140
ARL1150
ARL1160
ARL1170
ARL1180
ARL1190
ARL1200
ARL1210
ARL1220
ARL1230
ARL1240
ARL1250
ARL1260
ARL1270
ARL1280
ARL1290
ARL1300
ARL1310
ARL1320
ARL1330
ARL1340
ARL1350
ARL1360
ARL1370
ARL1380

INCA=INGJ+M1
INGAMA=INCA+M1
ING=INGAMA+M1
INSTRP=ING+M1*M1
INSTRM=INSTRP+M

C LINK LINK22 CALCULATES THE STRUCTURAL INFLUENCE COEFFICIENT
C MATRIX
C
C**STRUCTURAL MATRIX
C OCALL LINK2L(D(IXG),D(IYP),D(INPHUP),D(INPHUM),D(INPHUT),D(INXEA),
1 D(INYEA),D(INPHIP),D(INPHIM),D(INPHIT),D(INEI),D(INGJ),D(INCA),
2 D(INGAMA),D(ING),D(INSTRP),D(INSTRM),M,M1,N ,D(IWA),D(IWB),
3 IND(IRASE),D(IMM))
IF(NCNTL.EG.2) STOP
N1=N+1
IZN1=IZN+N
IZN2=IZN1+N
IZN3=IZN2+N

C LINK LINK33 CALCULATES ELASTIC DERIVATIVES, THE ELASTIC
C INDUCED DRAG PARAMETER AND THE ELASTIC PRESSURE COEFFICIENTS
C
C CALL LINK3L(IND(IBASE),D(IXP),D(IYP),D(IZP),D(IXG),D(IAR),D(IAM),
1 D(IXN),D(IYN),D(ICP),D(IMM),D(IZN),D(IZN1),D(IZN2),D(IZN3),N,N1)
3 WRITE (6,7)
7 FORMAT (I1,55X,21HTHIS CASE IS COMPLETE,/,56X,21H*****
1*****)
C** CHANGE INDEX KEY TO SET UP DISC FOR NEXT CASE
CALL STINDX(20,IND(1),12)
STOP
END

```



```

SUBROUTINE DISCRD(IND,XCP,YCP,ZCP,XCG,AREA,AMASS,XN,YN,ZN,BPRIM, DISC0010
1 DUM,N) DISC0020
C..... DISC0030
C SUBROUTINE DISCRD READS THE DATA STORED ON TAPE20 INTO CORE DISC0040
C..... DISC0050
C..... DISC0060
C..... DISC0070
C..... DISC0080
C..... DISC0090
C..... DISC0100
C..... DISC0110
C..... DISC0120
C..... DISC0130
C..... DISC0140
C..... DISC0150
C..... DISC0160
C..... DISC0170
C..... DISC0180
C..... DISC0190
C..... DISC0200
C..... DISC0210
C..... DISC0220
C..... DISC0230
C..... DISC0240
C..... DISC0250
C..... DISC0260
C..... DISC0270
C..... DISC0280
C..... DISC0290
C..... DISC0300
C..... DISC0310
C..... DISC0320
C..... DISC0330
DIMENSION XCP(N),YCP(N),ZCP(N),XCG(N),AREA(N),AMASS(N),
1 XN(N,4),YN(N,4),ZN(N,4),BPRIM(N,4)
DIMENSION IND(12),DUM(4,N)
CALL READMS(20,XCP(1),N,2)
CALL READMS(20,YCP(1),N,3)
CALL READMS(20,ZCP(1),N,4)
CALL READMS(20,XCG(1),N,5)
CALL READMS(20,AREA(1),N,6)
CALL READMS(20,AMASS(1),N,7)
N4=4*N
CALL READMS(20,DUM(1,1),N4, 8)
DO 1 I=1,N
DO 1 J=1,4
1 XN(I,J)=DUM(J,I)
CALL READMS(20,DUM(1,1),N4, 9)
DO 2 I=1,N
DO 2 J=1,4
2 YN(I,J)=DUM(J,I)
CALL READMS(20,DUM(1,1),N4,10)
DO 3 I=1,N
DO 3 J=1,4
3 ZN(I,J)=DUM(J,I)
CALL READMS(20,DUM(1,1),N4,11)
DO 4 I=1,N
DO 4 J=1,4
4 BPRIM(I,J)=DUM(J,I)
RETURN
END

```

```

C.....LN1L0010
C.....LN1L0020
C.....LN1L0030
C.....LN1L0040
C.....LN1L0050
C.....LN1L0060
C.....LN1L0070
C.....LN1L0080
C.....LN1L0090
C.....LN1L0100
C.....LN1L0110
C.....LN1L0120
C.....LN1L0130
C.....LN1L0140
C.....LN1L0150
C.....LN1L0160
C.....LN1L0170
C.....LN1L0180
C.....LN1L0190
C.....LN1L0200
C.....LN1L0210
C.....LN1L0220
C.....LN1L0230
C.....LN1L0240
C.....LN1L0250
C.....LN1L0260
C.....LN1L0270
C.....LN1L0280
C.....LN1L0290
C.....LN1L0300
C.....LN1L0310
C.....LN1L0320
C.....LN1L0330
C.....LN1L0340
C.....LN1L0350

SUBROUTINE LINKIL(IND,XCP,YCP,ZCP,XCG,AREA,AMASS,XN,YN,ZN,BPRIM,
1 WA,WR,CP,AW,N)
      L*I*N*K*I*L
C.....
C.....SUBROUTINE LINKIL CONTROLS THE CALCULATION OF THE AERODYNAMIC
C.....INFLUENCE COEFFICIENT MATRIX, RIGID DERIVATIVES, THE RIGID
C.....INDUCED DRAG PARAMETER AND THE PRESSURE COEFFICIENTS
C.....
C.....
C.....COMMON/INDMS/IA,IR,IC
C.....COMMON/CONTROL/LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HT1PNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHT1P,NHT2P,HALFB,ALPHA,HALF1,HALF2,NCPSWL,NCPWNG,MAX
C.....DIMENSION XCP(N),YCP(N),ZCP(N),XCG(N),AREA(N),AMASS(N),
1 XN(N,4),YN(N,4),ZN(N,4),BPRIM(N,4),WA(N),WB(N),CP(N),AW(N,N)
C.....DIMENSION HEAD(6),IND(1)
C.....INTFGR WNGPNL,HT1PNL,HT2PNL
C.....DATA (HEAD(I),I=1,6)/5HWING ,5HHORIZ,5HONTAL,5H TAIL,5H(GNE),5H(TW
10)/
      MAX=N
      ALPHA=1.
C.....SUBROUTINE ADICMX CALCULATES DOWNWASH MATRIX
C.....
C.....CALL ADICMX(AM,XN,YN,ZN,XCP,YCP,ZCP,LPANEL,BPRIM,AW,MAX)
C.....
C** MINV INVERTS A WELL-CONDITIONED MATRIX
C.....CALL MINV(AW,LPANEL)
C.....
C.....SUBROUTINE DELTCP FINDS OUT PRESSURE COEFFICIENTS FOR A
C.....GIVEN VALUE OF ALPHA
C.....CALL DELTCP(AW,ALPHA,LPANEL,CP)
      DO 1 J=1,LPANEL

```

```

LNIL0360
LNIL0370
LNIL0380
LNIL0390
LNIL0400
LNIL0410
LNIL0420
LNIL0430
LNIL0440
LNIL0450
LNIL0460
LNIL0470
LNIL0480
LNIL0490
LNIL0500
LNIL0510
LNIL0520
LNIL0530
LNIL0540
LNIL0550
LNIL0560
LNIL0570
LNIL0580
LNIL0590
LNIL0600
LNIL0610
LNIL0620
LNIL0630
LNIL0640
LNIL0650
LNIL0660
LNIL0670
LNIL0680
LNIL0690
LNIL0700

DO 1 I=1,LPANEL
  1 AW(I,J)=-2.*ARFA(I)*AW(I,J)
C
C   AW(I,J) IS THE AERODYNAMIC INFLUENCE COEFFICIENT MATRIX A(I,R)
C
C** DERIVR FINDS STABILITY DERIVATIVES
C
  DO 2 I=1,LPANEL
    2 XCG(I)=-XCG(I)
    CALL DERIVR(HALFSW,CREF,LPANEL,AW,XCG,WA,WB,CLALPA)
C**STORE MATRIX A ON DISC
  DO 30 I=1,N
    IAA=IA+I-1
    DO 29 J=1,N
      29 WA(J)=AW(I,J)
    30 CALL WRITMS(20,WA,N,IAA)
    DO 3 I=1,LPANEL
      3 XCG(I)=-XCG(I)
    IF (CLDES.EQ.0.) GO TO 5
C
C   NEXT THREE CARDS COMPUTE THE PRESSURE COEFFICIENTS FOR
C   DESIRED VALUE OF LIFT COEFFICIENT
C
  ALPHA=CLDES/CLALPA
  DO 4 I=1,LPANEL
    4 CP(I)=CP(I)*ALPHA
    CL=CLDES
    GO TO 6
  5 CL=ALPHA*CLALPA
  DO 7 I=1,LPANEL
    7 WA(I)=0.0
C
C   SETDRAG SEQS UP CALLS TO COMPUTE WING, TAIL AND CANARD DRAG.
C
  CALL SETDRAG(XN,YN,YCP,AREA,CP,XCG,WA,CL,AW,N)

```

```

WRITE (6,19)
WRITE(6,24)AM
IF(CLDES.NE.0.)WRITE(6,26)CLDES
WRITE(6,25)ALPHA
IF(NCNTL.NE.1)GO TO 14
WRITE(6,20)
WRITE(6,21)(I,XCP(I),YCP(I),ZCP(I),XCG(I),AREA(I),CP(I),I=1,
1 LPANEL)
WRITE(6,19)
RETURN
14 WRITE(6,22)
WRITE(6,23) (I,XCP(I),YCP(I),ZCP(I),XCG(I),AREA(I),CP(I),AMASS(I),I=1,LPANEL)
WRITE(6,19)
RETURN
19 FORMAT (1H1)
20 FORMAT (7X,5HPANEL,8X,3HXCP,12X,3HYCP,10X,3HZCP,15X,3HXCG,11X,4HARLN1L0870
1EA,10X,2HCP,7X,6HNUMBER)
21 FORMAT ((7X,13,5(5X,F10.5),5X,E12.5))
22 FORMAT (7X,5HPANEL,8X,3HXCP,12X,3HYCP,10X,3HZCP,15X,3HXCG,11X,4HARLN1L0900
1EA,10X,2HCP,12X,4HMASS,/,7X,6HNUMBER)
23 FORMAT ((7X,13,5(5X,F10.5),5X,E12.5,5X,F10.7))
24 FORMAT (55X,12HMACH NUMBER=,F5.2,/,55X,17H*****//)
25 FORMAT (44X,24HCP VALUES ARE FOR ALPHA=,F10.6,8H RADJAN,44X,42HLN1L0940
1*****//)
26 FORMAT (48X,25HDESIRED LIFT COEFFICIENT=,F10.5,/,48X
1*****//)
END
LN1L0710
LN1L0720
LN1L0730
LN1L0740
LN1L0750
LN1L0760
LN1L0770
LN1L0780
LN1L0790
LN1L0800
LN1L0810
LN1L0820
LN1L0830
LN1L0840
LN1L0850
LN1L0860
LN1L0870
LN1L0880
LN1L0890
LN1L0900
LN1L0910
LN1L0920
LN1L0930
LN1L0940
LN1L0950
LN1L0960
LN1L0970
LN1L0980

```

```

C.....ADIC0010
C.....ADIC0020
C.....ADIC0030
C.....ADIC0040
C.....ADIC0050
C.....ADIC0060
C.....ADIC0070
C.....ADIC0080
C.....ADIC0090
C.....ADIC0100
C.....ADIC0110
C.....ADIC0120
C.....ADIC0130
C.....ADIC0140
C.....ADIC0150
C.....ADIC0160
C.....ADIC0170
C.....ADIC0180
C.....ADIC0190
C.....ADIC0200
C.....ADIC0210
C.....ADIC0220
C.....ADIC0230
C.....ADIC0240
C.....ADIC0250
C.....ADIC0260
C.....ADIC0270
C.....ADIC0280
C.....ADIC0290
C.....ADIC0300
C.....ADIC0310
C.....ADIC0320
C.....ADIC0330
C.....ADIC0340
C.....ADIC0350

SUBROUTINE ADICMX(AM,XN,YN,ZN,XCP,YCP,ZCP,NPANEL,BPRIM,AW,MAX)
      A*D*I*C*M*X
C.....
C.....ADICMX CALCULATES DOWNWASH MATRIX
C.....
      DIMENSION XCP(1),YCP(1),A(2),ZCP(1)
      DIMENSION XN(NPANEL,4),YN(NPANEL,4),ZN(NPANEL,4),BPRIM(NPANEL,4)
      DIMENSION AW(NPANEL,NPANEL),W(4),TWO(2),CON(2)
      DATA TWO/1.,-1./,CON/O.25,O.50/,PAI/3.14159265/,EPSLON/1.E-8/
      RPTA=1./SQRT(ABS(1.-AM*AM))
      I,J=1
      IF(AM.GE.1.0) IJ=2
      DO 1 I=1,NPANEL
      DO 1 J=1,4
          1 RPRIM(I,J)=RPRIM(I,J)*BETA1
C.....
C**DOWNWASH MATRIX COMPUTATION
C.....
      F5=0.
      DO 16 I=1,NPANEL
      DO 16 J=1,NPANEL
      DO 15 II=1,2
      DO 14 K=1,4
          RPM=RPRIM(J,K)
          XIPRIM=(XCP(I)-XN(J,K))*BETA1
          YPRIM=TWO(II)*YCP(I)-YN(J,K)
          ZPRIM=ZCP(I)-ZN(J,K)
          KK=1
          IF(RPM.GE.0.0) GO TO 4
          RPM=-RPM
          YPRIM=-YPRIM
          KK=2
          4 IF(RPM.LE.FPSLON) RPM=0.0
          IF(ABS(RPM-1.)LE.EPSLON)RPM=1.0

```

```

RPM2=5.24*RPM
RR=ARS(1.-RPM2)
IF(IJ.FO.2)RR=SQRT(RR)
IF(RR.GT.EPSLON) GO TO 5
RPM=1.0
RR=0.0
5 R1=XIPRIM*XIPRIM
R2=YPRIM*YPRIM+ZPRIM*ZPRIM
GO TO (51,120),IJ
C**SURSONIC CASE
C
C
CONTINUE
A1=XIPRIM+SQRT(R1+R2)
A11=XIPRIM/SQRT(R2)
A2=RPM*XIPRIM+YPRIM
A3=XIPRIM-RPM*YPRIM
A33=(RPM2+1.)*ZPRIM*ZPRIM
SQA3=1./SQRT(A3*A3+A33)
A4=A2*SQA3
IF(A11+1000.) 53,53,57
53 CALL F(XIPRIM,YPRIM,ZPRIM,F1)
GO TO 6
57 F1=ALOG(A11)+SQRT(A11*A11+1.0)
C
6 IF(A4+1000.) 63,63,67
63 CALL F(A2,A3,A33,A6)
GO TO 7
67 CONTINUE
C
A7=SQRT(A4*A4+1.)
A8=A4+A7
A6=ALOG(A8)
7 F2=A6/SQRT(1.+RPM2)
F6=A1/R2
ADIC0360
ADIC0370
ADIC0380
ADIC0390
ADIC0400
ADIC0410
ADIC0420
ADIC0430
ADIC0440
ADIC0450
ADIC0460
ADIC0470
ADIC0480
ADIC0490
ADIC0500
ADIC0510
ADIC0520
ADIC0530
ADIC0540
ADIC0550
ADIC0560
ADIC0570
ADIC0580
ADIC0590
ADIC0600
ADIC0610
ADIC0620
ADIC0630
ADIC0640
ADIC0650
ADIC0660
ADIC0670
ADIC0680
ADIC0690
ADIC0700

```

```

A5=ARS(RPM)*SQRT(R2)*SQA3
F5=0.
IF(A5.GT.EPSLON)F5=ALOG(A5)
GO TO 13

C
C**SUPERSONIC CASE
C
120 A1=R2
A2=SQRT(A1)
IF(XIPRIM.GT.A2) GO TO 127
F1=0.
F2=0.
F6=0.
IF(RPM2.GE.1.0) GO TO 13
TEST=YPRIM-RPM*XIPRIM
IF(XIPRIM.FQ.A2) GO TO 122
IF(YPRIM.LE.0.0) GO TO 13

C
CONTL=RPM*YPRIM+RR*ABS(ZPRIM)
IF(XIPRIM-CONTL) 13,123,122
122 IF(TEST) 13,123,124
123 F2=1.570796327/RR
GO TO 13
124 F2=PAI/RR
GO TO 13

C
127 A3=XIPRIM/A1
SQXI=SQRT(XIPRIM*XIPRIM-A1)
F6=SQXI/A1
A11=XIPRIM/A2
F1=ALOG(A11+SQRT(A11*A11-1.))
IF (RPM2.FQ.1.) GO TO 128
A4=XIPRIM-RPM*YPRIM
A5=(RPM2-1.)*ZPRIM*ZPRIM
A6=SQRT(A4*A4+A5)

```

```

ADIC0710
ADIC0720
ADIC0730
ADIC0740
ADIC0750
ADIC0760
ADIC0770
ADIC0780
ADIC0790
ADIC0800
ADIC0810
ADIC0820
ADIC0830
ADIC0840
ADIC0850
ADIC0860
ADIC0870
ADIC0880
ADIC0890
ADIC0900
ADIC0910
ADIC0920
ADIC0930
ADIC0940
ADIC0950
ADIC0960
ADIC0970
ADIC0980
ADIC0990
ADIC1000
ADIC1010
ADIC1020
ADIC1030
ADIC1040
ADIC1050

```

```

A7=RPM*XIPRIM-YPRIM
IF (RPM2.GT.1.) GO TO 129
F2=(1./PR)*ACOS(A7/A6)
GO TO 131
128 F2=SQRT/(XIPRIM-YPRIM)
GO TO 131
129 A8=A7/A6
F2=(1./BB)*ALOG(A8+SQRT(A8*A8-1.))
GO TO 131
130 RPM=-RPM
YPRIM=-YPRIM
KK=?
GO TO 120
131 CONTINUE
130W(K)=CON(IJ)/(RETA1*PA1)*((BPM2+TWO(IJ))*F2-8PM*(F1-F5)-YPRIM*F6)*
1 TWO(KK)
14 CONTINUE
15 A(II)=W(1)-W(2)-W(3)+W(4)
16 AW(I,J)=A(1)+A(2)
RETURN
END
ADIC1060
ADIC1070
ADIC1080
ADIC1090
ADIC1100
ADIC1110
ADIC1120
ADIC1130
ADIC1140
ADIC1150
ADIC1160
ADIC1170
ADIC1180
ADIC1190
ADIC1200
ADIC1210
ADIC1220
ADIC1230
ADIC1240
ADIC1250
ADIC1260

```



```

C..... SUBROUTINE DERIVR(AREA,CREF,L PANEL,A,X,A1,UNIT1,CLALPA) DRVR0010
C..... D*E*R*I*V*R DRVR0020
C..... SURROUTINE DERIVR FINDS RIGID STABILITY DERIVATIVES DRVR0030
C..... SURROUTINE DERIVR FINDS RIGID STABILITY DERIVATIVES DRVR0040
C..... DIMENSION A(LPANEL,L PANEL),X(LPANEL,1),A1(LPANEL,1),UNIT1(LPANEL,1) DRVR0050
C..... 1) DRVR0060
C..... DO 1 I=1,L PANEL DRVR0070
C..... 1 UNIT1(I,1)=1. DRVR0080
C..... DRVR0090
C..... DRVR0100
C..... CLALPA COMPUTATION DRVR0110
C..... (A1)=(A)*(UNIT1) DRVR0120
C..... SURROUTINE MATMPY FINDS OUT PRODUCT OF TWO MATRICES DRVR0130
C..... CALL MATMPY(A,UNIT1,A1,L PANEL,L PANEL,1) DRVR0140
C..... (A3)=(UNIT1)T*(A1) DRVR0150
C..... SURROUTINE TRNPRD FINDS OUT DOT PRODUCT OF TWO VECTORS DRVR0160
C..... CALL TRNPRD(UNIT1,A1,A3,L PANEL) DRVR0170
C..... CLALPA=A3/AREA DRVR0180
C..... WRITE(6,2) CLALPA DRVR0190
C..... CMALPA COMPUTATION DRVR0200
C..... (A4)=(X)T*A1 DRVR0210
C..... CALL TRNPRD(X,A1,A4,L PANEL) DRVR0220
C..... CMALPA=A4/(AREA*CREF) DRVR0230
C..... WRITE(6,3) CMALPA DRVR0240
C..... CLQ COMPUTATION DRVR0250
C..... A1=A*X(1) DRVR0260
C..... CALL MATMPY(A,X,A1,L PANEL,L PANEL,1) DRVR0270
C..... DRVR0280
C..... DRVR0290
C..... DRVR0300
C..... DRVR0310
C..... DRVR0320
C..... DRVR0330
C..... DRVR0340
C..... DRVR0350

```

```

C      (A3)=(UNIT1)T*(A1)
      CALL TRNPRD(UNIT1,A1,A3,LPANEL)
      CLQ=-2.*A3/(AREA*CREF)
      WRITE(6,4) CLQ
C
C      CMQ COMPUTATION
      (A4)=(X)T*(A1)
C
      CALL TRNPRD(X,A1,A4,LPANEL)
      CMQ=-2.*A4/(AREA*CREF*CREF)
      WRITE(6,5) CMQ
      2 FORMAT (10X,9HCLALPR =,E12.5)
      3 FORMAT (10X,9HCMALPR -,E12.5)
      4 FORMAT (10X,9HCLQ =,F12.5)
      5 FORMAT (10X,9HCMQ =,E12.5)
      RETURN
      END
DRVR0360
DRVR0370
DRVR0380
DRVR0390
DRVR0400
DRVR0410
DRVR0420
DRVR0430
DRVR0440
DRVR0450
DRVR0460
DRVR0470
DRVR0480
DRVR0490
DRVR0500
DRVR0510
DRVR0520

```

```
0010  
0020  
0030  
0040  
0050  
0060  
  
F F F F F F
```

```
SUBROUTINE F(X2,X3,X4,FUNCT)  
A6=X2/SQRT(X3*X3+X4*X4)  
A7= SQRT(A6*A6+1.)  
FUNCT=ALOG(A6+A7)  
RETURN  
END
```



```

C   HOWEVER, IF AN END OF FILE IS ENCOUNTERED AFTER THE FIRST READ,
C   AN ATTEMPT WILL BE MADE TO READ THE ENTIRE MATRIX FROM TAPE7.
C
      NCP=NUNP/NL
      IF(IARS(NCNTL),NE.3) GO TO 99
      REWIND 7
      DO 40 I=1,NCP
      ICC=IC+I-1
      READ(7) (C(J),J=1,NCP)
      IF(EOF,7) 50,40
      40 CALL WRITMS(20,C,NCP,ICC)
      IF(NCNTL) 80,80,90
C
C**EOF ENCOUNTERED
      50 NREC=I-1
      IF(NREC) 55,55,60
      55 WRITE(6,56)
      56 FORMAT(IH1,*NO DATA FOUND ON TAPE7. EXECUTION TERMINATED*)
      CALL EXIT
C
      60 WRITE(6,61) NREC
      610FORMAT(IH1,I5,*RECORDS FOUND ON TAPE7*/*
      1 RECORD BEING ATTEMPTED*)
      REWIND 7
      READ(7) ((C(I,J),J=1,NCP),I=1,NCP)
C
      DO 70 I=1,NCP
      ICC=IC+I-1
      DO 65 J=1,NCP
      C(I,J)=C(I,J)
      70 CALL WRITMS(20,C,NCP,ICC)
      IF(NCNTL) 80,80,90
C
C**MATRIX WAS READ BY COLUMNS. STORE BY ROWS.
      80 CALL CWRITE(PHUP(1),C,NCP,IND)

```

```

LN2L0296
LN2L0297
LN2L0298
LN2L0299
LN2L0300
LN2L0301
LN2L0302
LN2L0303
LN2L0304
LN2L0305
LN2L0306
LN2L0307
LN2L0308
LN2L0309
LN2L0310
LN2L0311
LN2L0312
LN2L0313
LN2L0314
LN2L0315
LN2L0316
LN2L0317
LN2L0318
LN2L0319
LN2L0320
LN2L0321
LN2L0322
LN2L0323
LN2L0324
LN2L0325
LN2L0326
LN2L0327
LN2L0328
LN2L0329
LN2L0330

```

```

90 REWIND 7
   RETURN
C
99 CONTINUE
  DO 29 I=1,NCP
29 C(I)=0.0
  DO 31 I=1,NCP
    ICC=IC+I-1
31 CALL WRITMS(20,C,NCP,ICC)
C*****
  READ(5,12)(LPNL(I),I=1,4),N1,MOVTEL,NEIGJ
C*****
  FPNLFF=1
  LPNLFF=LPNL(1)
  FPNLRF=LPNLFF+1
  LPNLRF=LPNLFF+LPNL(2)
  FPNLMW=LPNLRF+1
  LPNLMW=LPNLRF+LPNL(3)
  FPNLHT=LPNLMW+1
  LPNLHT=LPNLMW+LPNL(4)
  IF (LPNLFF.GE.FPNLFF) WRITE (6,16) FPNLFF,LPNLFF
  IF (LPNLRF.GE.FPNLRF) WRITE (6,17) FPNLRF,LPNLRF
  IF (LPNLMW.GE.FPNLMW) WRITE (6,18) FPNLMW,LPNLMW
  IF (LPNLHT.GE.FPNLHT) WRITE (6,19) FPNLHT,LPNLHT
C*****
  READ (5,9) (IASIGN(I),I=1,NCP)
  READ (5,10) CSMW,CSHT,WDTHMW,WDTHHT,XREF
C*****
  IF (CSMW.NE.0.) WRITE (6,20) CSMW
  IF (CSHT.NE.0.) WRITE (6,21) CSHT
  IF (WDTHMW.NE.0.) WRITE (6,22) WDTHMW
  IF (WDTHHT.NE.0.) WRITE (6,23) WDTHHT
  WRITE (6,24) XREF
C*****
  IF (NCNTL.EQ.2) READ (5,10) (XCG(I),YCG(I),I=1,NUMPNL)

```

```

LN2L0331
LN2L0332
LN2L0333
LN2L0334
LN2L0335
LN2L0336
LN2L0340
LN2L0350
LN2L0360
LN2L0370
LN2L0380
LN2L0390
LN2L0400
LN2L0410
LN2L0420
LN2L0430
LN2L0440
LN2L0450
LN2L0460
LN2L0470
LN2L0480
LN2L0490
LN2L0500
LN2L0510
LN2L0520
LN2L0530
LN2L0540
LN2L0550
LN2L0560
LN2L0570
LN2L0580
LN2L0590
LN2L0600
LN2L0610
LN2L0620

```



```

C
3  NCP1=FPNLRF
   NCP2=LPNLRF
   NW1=FPNLMW
   NW2=LPNLMW
   NH1=FPNLHT
   NH2=LPNLHT
   GO TO 30
C
C   USE OF CTHETA FOR WING
C
4  NCP1=FPNLMW
   NCP2=LPNLMW
   GO TO 30
C
C   USE OF CTHETA FOR HORIZONTAL TAIL
C
5  NCP1=FPNLHT
   NCP2=LPNLHT
   NH1=FPNLHT
   NH2=LPNLHT
   NC1=FPNLRF
   NC2=LPNLRF
C
C   SUBROUTINE CTHETA IS THE ACTUAL SUBROUTINE WHICH CALCULATES
C   STRUCTURAL MATRIX
C
30 CALL CTHETA(NCONTL,XEA,YEA,XCG,YCG,EI,GJ,IASIGN,CSMW,WDTHMW,CSHT,
1DTHHT,NCP1,NCP2,NW1,NW2,N1,NH1,NH2,NC1,NC2,NEA,NN,PHIUP,PHIUL,
2T,PHUP,PHUM,PHUT,A,STORP,STORM,GAMMA,G,C,NCP,XREF,M1,M2,IND)
   GO TO 1
C** CWRITE STORES THE C MATRIX ON DISC BY ROWS
   6 CALL CWRITE(PHUP1),C,NUMPNL,IND)
C
C** WRITEC PRINTS OUT THE INFLUENCE COEFFICIENT MATRIX
LN2L0980
LN2L0990
LN2L1000
LN2L1010
LN2L1020
LN2L1030
LN2L1040
LN2L1050
LN2L1060
LN2L1070
LN2L1080
LN2L1090
LN2L1100
LN2L1110
LN2L1120
LN2L1130
LN2L1140
LN2L1150
LN2L1160
LN2L1170
LN2L1180
LN2L1190
LN2L1200
LN2L1210
LN2L1220
LN2L1230
LN2L1240
LN2L1250
LN2L1260
LN2L1270
LN2L1280
LN2L1290
LN2L1300
LN2L1310
LN2L1320

```

```

IF(NCNTL.EQ.2.OR.NCNTL.EQ.4) CALL WRITEC(PHUP'1),NCP)
RETURN
7 IERROR=7
WRITE (6,28) IERROR
WRITE (6,26)
RETURN
8 IFFOR=3
WRITE (6,28) IFFOR
WRITE (6,25) NEA,MI
RETURN
9 FORMAT (40I2)
10 FORMAT (8F10.5)
11 FORMAT (4E15.8)
12 FORMAT (10I3)
13 FORMAT(14,65H COORDINATES OF UNIT LOADING POINTS AND LOADING POINTS,
1T ASSIGNMENTS, //33H I XCG YCG IASIGN/(15,2F10.5,1L2L1480
28)
14 FORMAT(//,37H COORDINATES OF ELASTIC AXIS SEGMENTS//25H I
1 XEA YEA/(15,2F10.5)
15 FORMAT(//,46H ELASTIC AXIS TORSIONAL AND BENDING STIFFNESS /
14X,1H1,10X,2HE1,9X,3HKGJ/(1,2E12.4)
16 FORMAT (10X,38HFIRST PANEL NUMBER ON FRONT FUSELAGE =,I3,/,10X,38H
1LAST PANEL NUMBER ON FRONT FUSELAGE =,I3)
17 FORMAT (10X,38HFIRST PANEL NUMBER ON REAR FUSELAGE =,I3)
18 FORMAT (10X,38HFIRST PANEL NUMBER ON MAIN WING =,I3,/,10X,38H
1LAST PANEL NUMBER ON MAIN WING =,I3)
19 FORMAT (10X,38HFIRST PANEL NUMBER ON HORIZONTAL TAIL=,I3,/,10X,38H
1LAST PANEL NUMBER ON HORIZONTAL TAIL =,I3)
20 FORMAT (10X,42H STRUCTURAL CHORD FOR MAIN WING =,F10.5)
21 FORMAT (10X,42H STRUCTURAL CHORD FOR HORIZONTAL TAIL=,F10.5)
22 FORMAT (10X,64HHALF THE WIDTH OF FUSELAGE AT ROOT CHORD OF THE MAIL
INWING =,F10.5)
23 FORMAT (10X,64HHALF THE WIDTH OF FUSELAGE AT ROOT CHORD OF THE H
ORIZONTAL TAIL=,F10.5)
LN2L1330
LN2L1340
LN2L1350
LN2L1360
LN2L1370
LN2L1380
LN2L1390
LN2L1400
LN2L1410
LN2L1420
LN2L1430
LN2L1440
LN2L1450
LN2L1460
LN2L1470
LN2L1480
LN2L1490
LN2L1500
LN2L1510
LN2L1520
LN2L1530
LN2L1540
LN2L1550
LN2L1560
LN2L1570
LN2L1580
LN2L1590
LN2L1600
LN2L1610
LN2L1620
LN2L1630
LN2L1640
LN2L1650
LN2L1660
LN2L1670

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```

24 FORMAT (10X,28HX-COORDINATE OF FIXED POINT=,F10.5) LN2L1680
25 FORMAT (10X,45HNEA IS GREATER THAN MAXIMUM ASSUMED NEA VALUE,/,10XLN2L1690
1,30HFIRST INPUT DATA CARD IS WRONG,/,10X,26HSECOND VARIABLE SHOULD LN2L1700
2 9F ,12.9H AND NOT ,I2) LN2L1710
26 FORMAT (10X,31HNCONTL CANNOT BE GREATER THAN 4) LN2L1720
27 FORMAT (1H1,33HNUMBER OF ELASTIC AXIS POINTS ON ,3A5,1H=,I2,///) LN2L1730
28 FORMAT (1H1,10X,7HIFROR=,I2) LN2L1740
END LN2L1750

```

```

SUBROUTINE CTHETA(NCONTL,XEA,YEA,XCG,YCG,EI,GJ,IASIGN,CSMW,WDTHMW,CTHEU010
1CSHT,WDTHHT,NCPI,NC2,NW1,NW2,N1,NH1,NH2,NC1,NC2,NEA,NN,PHIUP,PHIUCTHEU020
2M,PHIUT,PHUP,PHUM,PHUT,A,STORP,STORM,GAMMA,G,C,NCP,XREF,M1,M2,IND)CTHEU030
CTHEU040
C.....CTHEU050
C SURROUTINE CTHETA IS THE ACTUAL SUBROUTINE WHICH CALCULATES
C THE STRUCTURAL MATR X C. C RESIDES ON DISC. ROWS ARE ACCESSED
C AS NFFDFD.
C
C NCONTL=1 FRONT FUSELAGE ONLY
C NCONTL=2 REAR FUSELAGE ONLY
C NCONTL=3 MAIN WING ONLY
C NCONTL=4 HORIZONTAL TAIL ONLY
C.....
C.....
DIMENSION A(1),XEA(1),YEA(1),XCG(1),YCG(1),EI(1),GJ(1),GAMMA(1)
DIMENSION PHIUP(1),PHUM(1),PHIUT(1)
DIMENSION STORP(1),STORM(1),IASIGN(1)
DIMENSION PHUP(M1,M1),PHUM(M1,M1),PHUT(M1,M1),G(M2,M2)
DIMENSION IND(1),C(1)
COMMON/INDMS/IA,IR,IC
INTEGER FPNLFF,FPNLRF,FPNLMW,FPNLHT
COMMON /PNLUM/ FPNLFF,FPNLRF,FPNLFF,FPNLRF,FPNLMW,LPNLMW,FPNLHT,LPNLMW,FPNLHT,L
1PNLHT,MOVTEL
N=NCP
IF (NCONTL.GT.2) GO TO 24
DO 1 I=2,NEA
1 A(I-1)=ARS(XEA(I)-XEA(I-1))
IF (NCONTL.EQ.1) CK=1.
IF (NCONTL.EQ.2) CK=-1.
DO 5 I=1,NN
J=NFA-I
JP=J+1
JJ=J+1
2 XM=(XEA(JJ)-XEA(JP))*CK

```

```

PHIUP(JJ)=(XM*A(J)/EI(J)+A(J)*A(J)/(2.*EI(J))*CK
PHIUM(JJ)='A(J)/EI(J))*CK
J=J-1
IF (JJ.GT.2) GO TO 2
PHUP(1,JP)=0.
PHUM(1,JP)=0.
DO 4 II=2,NEA
IF (II.GT.JP) GO TO 3
PHUP(II,JP)=PHUP(II-1,JP)+PHIUP(II)
PHUM(II,JP)=PHUM(II-1,JP)+PHIUM(II)
GO TO 4
3 PHUP(II,JP)=PHUP(JP,JP)
PHUM(II,JP)=PHUM(JP,JP)
4 CONTINUE
5 CONTINUE
C
C EFFECT OF FRONT FUSELAGE ON FRONT FUSELAGE
C
IF (NCONTL.EQ.1) GO TO 7
N2=IASIGN(N1)
DO 6 II=1,NFA
STORP(II)=PHUP(II,N2)
6 STORM(II)=PHUM(II,N2)
C
C EFFECT OF REAR FUSELAGE ON REAR FUSELAGE
C
7 DO 12 K=NCP1,NCP2
ICC=IC+K-1
C** READ C MATRIX FROM DISC
CALL READMS(20,C,N,ICC)
I=IASIGN(K)
IF (I.EQ.1) GO TO 8
XM=(XFA(I)-XCG(K))*CK
GO TO 10
8 DO 9 J=NCP1,NCP2
CTHEU360
CTHEU370
CTHEU380
CTHEU390
CTHEU400
CTHEU410
CTHEU420
CTHEU430
CTHEU440
CTHEU450
CTHEU460
CTHEU470
CTHEU480
CTHEU490
CTHEU500
CTHEU510
CTHEU520
CTHEU530
CTHEU540
CTHEU550
CTHEU560
CTHEU570
CTHEU580
CTHEU590
CTHEU600
CTHEU610
CTHEU620
CTHEU630
CTHEU640
CTHEU650
CTHEU660
CTHEU670
CTHEU680
CTHEU690
CTHEU700

```

```

CTHE0710
CTHE0720
CTHE0730
CTHE0740
CTHE0750
CTHE0760
CTHE0770
CTHE0780
CTHE0790
CTHE0800
CTHE0810
CTHE0820
CTHE0830
CTHE0840
CTHE0850
CTHE0860
CTHE0870
CTHE0880
CTHE0890
CTHE0900
CTHE0910
CTHE0920
CTHE0930
CTHE0940
CTHE0950
CTHE0960
CTHE0970
CTHE0980
CTHE0990
CTHE1000
CTHE1010
CTHE1020
CTHE1030
CTHE1040
CTHE1050

L=IASIGN(J)
9 C(L)=0.
  GO TO 12
10 DO 11 J=NCP1,NCP2
  L=IASIGN(J)
11 C(J)=PHUP(L,I)+PHUM(L,I)*XM
C** REPLACE C MATRIX WITH REAR FUSELAGE ON REAR FUSELAGE EFFECTS
12 CALL WRITIN(20,C,N,ICC)
C
C EFFECT OF FRONT FUSELAGE ON MAIN WING
C EFFECT OF REAR FUSELAGE ON MAIN WING
C
NHH1=NCP1
NHH2=NCP2
NCP11=NCP1
IF (NCONTL.EQ.2) NCP11=NCP1-1
NCP22=NCP2
13 CSMW2=CSMW/2.
  YLIMIT=WIDTHW+CSMW2
  DO 17 K=NHH1,NHH2
  ICC=IC+K-1
C** READ C MATRIX FROM DISC
  CALL READMS(20,C,N,ICC)
  DO 16 I=NW1,NW2
  IF(YCG(I).GT.YLIMIT) GO TO 165
  XCONT=(XCG(I)-XRFF)*CK
  IF(XCONT.GF.0.) GO TO 16
C
  DO 14 J=NCP11,NCP22
  IF(XCG(I).GT.XCG(J).AND.XCG(I).LE.XCG(J+1)) GO TO 15
C
15 Y=1.-(YCG(I)-WIDTHW)/CSMW2
  X=(XCG(J+1)-XCG(I))/(XCG(J+1)-XCG(J))
  CMAX=C(J+1) +C(J) -C(J+1) *X
16 C(I) =CMAX*Y

```

```

165 CONTINUE
C** REPLACE C MATRIX WITH FRONT AND REAR FUSELAGE ON MAIN WING EFFECTS
17 CALL WRITIN(20,C,N,ICC)
18 CONTINUE
IF (INCONTL.EQ.4) GO TO 36
IF (INCONTL.EQ.1) RETURN
C
C EFFECT OF REAR FUSELAGE ON HORIZONTAL TAIL
C
CSHT2=CSHT/2.
YLIMIT=WDTHHT+CSHT2
DO 23 I=NH1,NH2
IF (YCG(I).GT.YLIMIT) GO TO 21
DO 19 J=NCP1,NCP2
IF (XCG(I).LE.XCG(J+1).AND.XCG(I).GT.XCG(J)) GO TO 20
19 CONTINUE
20 Y=1.-(YCG(I)-WDTHHT)/CSHT2
X=(XCG(J)-XCG(I))/(XCG(J+1)-XCG(J))
GO TO 22
21 Y=0.
22 DO 23 K=NCP1,NCP2
ICC=IC+K-1
C** READ C MATRIX FROM DISC
CALL RFADMS(20,C,N,ICC)
CMAX=C(J)+(C(J)-C(J+1))*X
C(I)=C(N1)*(1.-Y)+CMAX*Y
C** REPLACE C MATRIX WITH REAR FUSELAGE ON HORIZONTAL TAIL EFFECTS
23 CALL WRITIN(20,C,N,ICC)
RETURN
24 CONTINUE
C
C EFFECT OF MAIN WING ON MAIN WING
C EFFECT OF HORIZONTAL TAIL ON HORIZONTAL TAIL
C (WITHOUT REAR FUSELAGE BENDING)
C
CTHE1060
CTHE1070
CTHE1080
CTHE1090
CTHE1100
CTHE1110
CTHE1120
CTHE1130
CTHE1140
CTHE1150
CTHE1160
CTHE1170
CTHE1180
CTHE1190
CTHE1200
CTHE1210
CTHE1220
CTHE1230
CTHE1240
CTHE1250
CTHE1260
CTHE1270
CTHE1280
CTHE1290
CTHE1300
CTHE1310
CTHE1320
CTHE1330
CTHE1340
CTHE1350
CTHE1360
CTHE1370
CTHE1380
CTHE1390
CTHE1400

```

```

DO 26 I=2,NEA
  A(I-1)=SQRT((XEA(I)-XEA(I-1))*2+(YEA(I)-YEA(I-1))*2)
  IF (YEA(I).EQ.YEA(I-1)) GO TO 25
  GAMMA(I-1)=ATAN((XEA(I)-XEA(I-1))/(YEA(I)-YEA(I-1)))
  GO TO 26
25 GAMMA(I-1)=1.570796325
26 CONTINUE
DO 27 I=1,NN
DO 27 J=1,NN
27 G(I,J)=GAMMA(J)-GAMMA(I)
DO 31 I=1,NN
  J=NEA-I
  JP=J+1
28 JJ=J+1
  SINF=SIN(GAMMA(J))
  COSINE=COS(GAMMA(J))
  T=(YEA(JP)-YEA(JJ))*SINE-(XEA(JP)-XEA(JJ))*COSINE
  XM=(YEA(JP)-YEA(JJ))*COSINE+(XEA(JP)-XEA(JJ))*SINE
  SINJJP=SIN(G(J,JP-1))
  COSJJP=COS(G(J,JP-1))
  THETP=XM*A(J)/EI(J)+A(J)*A(J)/(2.*EI(J))
  PHIP=T*A(J)/GJ(J)
  THETM=COSJJP*A(J)/EI(J)
  PHIM=-SINJJP*A(J)/GJ(J)
  THETT=SINJJP*A(J)/EI(J)
  PHIT=COSJJP*A(J)/GJ(J)
  PHIUP(JJ)=PHIP*COSINE-THETP*SINE
  PHIUM(JJ)=PHIM*COSINE-THETM*SINE
  PHIUT(JJ)=PHIT*COSINE-THETT*SINE
  J=J-1
  IF (JJ.GT.21 GO TO 28
  PHUP(1,JP)=0.
  PHUT(1,JP)=0.
  PHUM(1,JP)=0.
  DO 30 II=2,NEA
CTHE1410
CTHE1420
CTHE1430
CTHE1440
CTHE1450
CTHE1460
CTHE1470
CTHE1480
CTHE1490
CTHE1500
CTHE1510
CTHE1520
CTHE1530
CTHE1540
CTHE1550
CTHE1560
CTHE1570
CTHE1580
CTHE1590
CTHE1600
CTHE1610
CTHE1620
CTHE1630
CTHE1640
CTHE1650
CTHE1660
CTHE1670
CTHE1680
CTHE1690
CTHE1700
CTHE1710
CTHE1720
CTHE1730
CTHE1740
CTHE1750

```



```

CTHE1760
CTHE1770
CTHE1780
CTHE1790
CTHE1800
CTHE1810
CTHE1820
CTHE1830
CTHE1840
CTHE1850
CTHE1860
CTHE1870
CTHE1880
CTHE1890
CTHE1900
CTHE1910
CTHE1920
CTHE1930
CTHE1940
CTHE1950
CTHE1960
CTHE1970
CTHE1980
CTHE1990
CTHE2000
CTHE2010
CTHE2020
CTHE2030
CTHE2040
CTHE2050
CTHE2060
CTHE2070
CTHE2080
CTHE2090
CTHE2100

IF (II.GT.JP) GO TO 29
PHUP(II,JP)=PHUP(II-1,JP)+PHIUP(II)
PHUM(II,JP)=PHUM(II-1,JP)+PHIUM(II)
PHUT(II,JP)=PHUT(II-1,JP)+PHIUT(II)
GO TO 30
29 PHUP(II,JP)=PHUP(JP,JP)
PHUT(II,JP)=PHUT(JP,JP)
PHUM(II,JP)=PHUM(JP,JP)
30 CONTINUE
31 CONTINUE
DO 33 K=NCPI,NCPI2
ICC=IC+K-1
CALL READMS(20,C,N,ICC)
I=IASIGN(K)
SING=5IN(GAMMA(I-1))
COSG=COS(GAMMA(I-1))
T=(YCG(K)-YEA(I))*SING-(XCG(K)-XEA(I))*COSG
XM=(YCG(K)-YEA(I))*COSG+(XCG(K)-XEA(I))*SING
DO 32 J=NCPI,NCPI2
L=IASIGN(J)
32 C(J)=PHUP(L,I)+PHUM(L,I)*XM+PHUT(L,I)*T
C** REPLACE C MATRIX WITH MAIN WING ON MAIN WING EFFECTS
33 CALL WRITIN(20,C,N,ICC)
IF (NCONTL.EQ.3) RETURN
C
C
C EFFECT OF HORIZONTAL TAIL ON REAR FUSELAGE
DO 35 K=NCPI,NCPI2
ICC=IC+K-1
CALL READMS(20,C,N,ICC)
XM=XCG(K)-XCG(N1)
DO 34 J=NC1,NC2
L=IASIGN(J)

```

```

34 C(J)=STORP(L)+STORM(L)*XM
C** REPLACE C MATRIX WITH HORIZONTAL TAIL ON REAR FUSELAGE EFFECTS
35 CALL WRITIN(20,C,N,ICC)
C
C      EFFECT OF HORIZONTAL TAIL ON MAIN WING
C
      NH1=FPNLHT
      NH2=LPNLHT
      NHH1=FPNLHT
      NHH2=LPNLHT
      NW1=FPNLMW
      NW2=LPNLMW
      NCP1=FPNLRF
      NCP2=LPNLRF
      CK=-1.
      NCP11=LPNLFF
      NCP22=LPNLRF
      GO TO 14
36 CONTINUE
C
C      EFFECT OF HORIZONTAL TAIL ON HORIZONTAL TAIL
C      (WITH REAR FUSELAGE BENDING)
C
      IF (MOVTEL.EQ.1) GO TO 43
      CSHT2=CSHT/2.
      YLIMIT=WDTHHT+CSHT2
      DO 42 K=NH1,NH2
      ICC=IC+K-1
      CALL READMS(20,C,N,ICC)
C** READ C MATRIX FROM DISC
C
      DO 41 I=NH1,NH2
      IF(YCG(I).GT.YLIMIT) GO TO 39
      DO 37 J=NC1,NC2
      IF(XCG(I).GT.XCG(J).AND.XCG(I).LE.XCG(J+1)) GO TO 38

```

```

CTHE2110
CTHE2120
CTHE2130
CTHE2140
CTHE2150
CTHE2160
CTHE2170
CTHE2180
CTHE2190
CTHE2200
CTHE2210
CTHE2220
CTHE2230
CTHE2240
CTHE2250
CTHE2260
CTHE2270
CTHE2280
CTHE2290
CTHE2300
CTHE2310
CTHE2320
CTHE2330
CTHE2340
CTHE2350
CTHE2360
CTHE2370
CTHE2380
CTHE2390
CTHE2400
CTHE2410
CTHE2420
CTHE2430
CTHE2440
CTHE2450

```

```

38  Y=1.-(YCG(I)-WDTHHT)/CSHT2
    X=(XCG(J)-XCG(I))/(XCG(J+1)-XCG(J))
    GO TO 40
39  Y=0.
    X=0.
40  CMAX=C(J)+(C(J)-C(J+1))*X
    C(I)=C(I)+C(N1)*(1.-Y)+CMAX*Y
41  CONTINUE
C
C** REPLACE C MATRIX WITH HORIZONTAL TAIL ON HORIZONTAL TAIL EFFECTS
42  CALL WRITIN(20,C,N,ICC)
    RETURN
    43 DO 44 J=NH1,NH2
        ICC=IC+K-1
C** READ C MATRIX FROM DISC
    CALL READMS(20,C,N,ICC)
    DO 44 I=NH1,NH2
        C(I)=C(I)+C(N1)
C** REPLACE C MATRIX WITH ALL-MOVABLE HORIZONTAL TAIL EFFECTS
    44 CALL WRITIN(20,C,N,ICC)
        WRITE (6,45)
    45 FORMAT (///IX*THIS AIRCRAFT HAS ALL-MOVABLE HORIZONTAL TAIL*///)
    RETURN
    END
CTHE2460
CTHE2470
CTHE2480
CTHE2490
CTHE2500
CTHE2510
CTHE2520
CTHE2530
CTHE2540
CTHE2550
CTHE2560
CTHE2570
CTHE2580
CTHE2590
CTHE2600
CTHE2610
CTHE2620
CTHE2630
CTHE2640
CTHE2650
CTHE2660
CTHE2670
CTHE2680
CTHE2690

```



```

C.....SUBROUTINE CONVERT(FI,GJ,NN)
C.....C*N*V*E*R*T
C.....
C.....SURROUTINE CONVERT IS USED TO CONVERT EI AND GJ VALUES FROM
C.....(LB-INCH**2) UNITS TO (LB-FEET**2) UNITS
C.....
C.....DIMENSION F(NN),GJ(NN)
C.....C=1./144.
C.....DO 1 I=1,NN
C.....EI(I)=EI(I)*C
C.....1 GJ(I)=GJ(I)*C
C.....RETURN
C.....END

```

```

CNVT0010
CNVT0020
CNVT0030
CNVT0040
CNVT0050
CNVT0060
CNVT0070
CNVT0080
CNVT0090
CNVT0100
CNVT0110
CNVT0120
CNVT0130

```

```

SUBROUTINE LINK3L(IND,XCP,YCP,THETAE,XCG,AREA,AMASS,XN,YN,CP,P,WA,LN3L0010
? WR,WC,WI,NUMPNL,N1)
C.....LN3L0020
C.....LN3L0030
C.....LN3L0040
C.....LN3L0050
C.....LN3L0060
C.....LN3L0070
C.....LN3L0080
C.....LN3L0090
C.....LN3L0100
C.....LN3L0110
C.....LN3L0120
C.....LN3L0130
C.....LN3L0140
C.....LN3L0150
C.....LN3L0160
C.....LN3L0170
C.....LN3L0180
C.....LN3L0190
C.....LN3L0200
C.....LN3L0210
C.....LN3L0220
C.....LN3L0230
C.....LN3L0240
C.....LN3L0250
C.....LN3L0260
C.....LN3L0270
C.....LN3L0280
C.....LN3L0290
C.....LN3L0300
C.....LN3L0310
C.....LN3L0320
C.....LN3L0330
C.....LN3L0340
C.....LN3L0350

L*I*N*K*3*L
SUPROUTINE LINK3L CONTROLS THE CALCULATION OF ALL THE ELASTIC
STABILITY DERIVATIVES, THE ELASTIC INDUCED DRAG PARAMETER
AND THE PRESSURE COEFFICIENTS

THE P-ARRAY IS USED TO HOLD THE A AND B-MATRICES AS NEEDED.

COMMON/INDMS/IA,IR,IC
DIMENSION XCG(1),AMASS(1),THETAE(1),CP(1),YCP(1),AREA(1),HEAD(6)
DIMENSION WA(1),WP(1),WC(1),WI(1)
DIMENSION P(NUMPNL,N1)
DIMENSION IND(1)
DIMENSION XCP(1)
EQUIVALENCE (N,LPANEL)
DIMENSION XN(NUMPNL,4),YN(NUMPNL,4)
COMMON/CNTROL/LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AMACH,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HTIPNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHTIP,NHT2P, HALFB,ALPHA,HALFBI,HALF82,NCPSWL,NCPWNG,MAX
INTEGER WNGPNL,HTIPNL,HT2PNL
DATA (HEAD(I),I=1,6)/5HWING,5HHORIZ,5HONTAL,5H TAIL,5H(ONE),5H(TW
10)/
WRITE (6,25) AMACH
AM=AMACH
C.....LN3L0280
C.....LN3L0290
C.....LN3L0300
C.....LN3L0310
C.....LN3L0320
C.....LN3L0330
C.....LN3L0340
C.....LN3L0350
NALT=ALTNUM
DO 18 K=1,NALT
WRITE (6,20) W
DO 1 I=1,LPANEL
1 XCG(I)=-XCG(I)

```



```

3 WA(I)=ALPHA-WA(I)*G
  CALL MATMPY(P,WA,THETA,LPANEL,LPANEL,I)
  CALL DISMPY(WR,THETA,CP,LPANEL,LPANEL,I,20,IB,0,IND)
  DO 4 J=1,LPANEL
4 CP(I)=CP(I)/AREA(I)
  ALPHAQ=ALPHA*G
  DO 6 I=1,LPANEL
  SUMA=0.
  DO 5 J=1,LPANEL
5 SUMA=SUMA+P(I,J)
6 WA(I)=SUMA*ALPHAQ-G*AMASS(I)
  CALL DISMPY(WC,WA,THETA,LPANEL,LPANEL,I,20,IC,U,IND)
  CALL DISMPY(WC,P,WB,LPANEL,LPANEL,20,IC,IB,IND)
7 CONTINUE
C**READ MATRIX B FROM DISC AND STORE IT IN MATRIX P
  DO 30 I=1,LPANEL
  IAR=IR+I-1
  CALL READMS(20,WB,LPANEL,IBB)
  DO 30 J=1,LPANEL
30 P(I,J)=WR(J)
  DO 9 I=1,LPANEL
  DO 9 J=1,LPANEL
  IF (I.EQ.J) GO TO 8
  P(I,J)=-Q*P(I,J)
  GO TO 9
8 P(I,J)=1.-Q*P(I,J)
9 CONTINUE
  CALL MINV(P,LPANEL,
  CALL MATMPY(P,THETA,WA,LPANEL,LPANEL,I)
C
C CALCULATION OF DEFORMED ANGLE OF PANELS (THETA) AND THE
C PRESSURE COEFFICIENTS (ENDS),
C
C WRITE (6,27)
  WRITE (6,28) (I,WA(I),CP(I),I=1,LPANEL)

```

```

LN3L0710
LN3L0720
LN3L0730
LN3L0740
LN3L0750
LN3L0760
LN3L0770
LN3L0780
LN3L0790
LN3L0800
LN3L0810
LN3L0820
LN3L0830
LN3L0840
LN3L0850
LN3L0860
LN3L0870
LN3L0880
LN3L0890
LN3L0900
LN3L0910
LN3L0920
LN3L0930
LN3L0940
LN3L0950
LN3L0960
LN3L0970
LN3L0980
LN3L0990
LN3L1000
LN3L1010
LN3L1020
LN3L1030
LN3L1040
LN3L1050

```

```

18 CALL SETDRAG(XN,YN,YCP,AREA,CP,XCG,WA,CL,P,N)
19 CONTINUE
20 RETURN
21 FORMAT (3F10.5)
22 FORMAT (10X,7HWEIGHT=,F10.0)
23 FORMAT (10X,4HRHO=,F12.8,5X,7HS.0.S.=,F10.3,5X,9HALTITUDE=,F6.0)
24 FORMAT (10X,9HVELOCITY=,E12.5)
25 FORMAT (10X,17HDYNAMIC PRESSURE=,E12.5)
26 FORMAT (10X,7HCLTRIM=,F10.3)
27 FORMAT (1H1,9X,36HELASTIC DERIVATIVES FOR MACH NUMBER=,5.2,/)
28 FORMAT (7X,5HPANEL,8X,8HTHETA(E),11X,5HCP(E),/,7X,6HNUMBER)
29 FORMAT (7X,13.8X,E12.5,5X,E12.5)
30 END
31 LN3L1060
32 LN3L1070
33 LN3L1080
34 LN3L1090
35 LN3L1100
36 LN3L1110
37 LN3L1120
38 LN3L1130
39 LN3L1140
40 LN3L1150
41 LN3L1160
42 LN3L1170
43 LN3L1180

```



```

                GO TO 3
                ? R(I,J)=1.-Q*R(I,J)
                3 CONTINUE
C
C** MINV INVERTS A WELL-CONDITIONED MATRIX
C
                CALL MINV(B,N)
                DO 21 I=1,N
                IRR=IR+I-1
                DO 22 J=1,N
                ?2 WR(J)=R(I,J)
                ?1 CALL WRITIN(20,WR,N,IBR)
C** THE R MATRIX HAS BEEN GENERATED AND THE INVERSE OF B
                HAS BEEN STORED ON DISC.
C
C                CLALPA COMPUTATION
C
                CALL DISMPY(WR,WI,WA,N,N,1,20,IA,0,IND)
                CALL MATMPY(B,WA,WB,N,N,1)
C
C                SUBROUTINE TRNPRD FINDS OUT THE DOT PRODUCT OF TWO ARRAYS
C
                CALL TRNPRD(WI,WR,A3,N)
                CLALPA=A3/AREA
                WRITE(6,5) CLALPA
C
C                CMALPA COMPUTATION
C
                CALL TRNPRD(X,WR,A4,N)
                CMALPA=A4/(AREA*CREF)
                WRITE(6,6) CMALPA
C
C                CLQERR COMPUTATION
C
                CALL DISMPY(WR,X,WA,N,N,1,20,IA,0,IND)

```

```

DERV0360
DERV0370
DERV0380
DERV0390
DERV0400
DERV0410
DERV0420
DERV0430
DERV0440
DERV0450
DERV0460
DERV0470
DERV0480
DERV0490
DERV0500
DERV0510
DERV0520
DERV0530
DERV0540
DERV0550
DERV0560
DERV0570
DERV0580
DERV0590
DERV0600
DERV0610
DERV0620
DERV0630
DERV0640
DERV0650
DERV0660
DERV0670
DERV0680
DERV0690
DERV0700

```

```

C
CALL MATMPY(R,WA,WB,N,N,1)
CALL TRNPRD(WI,WH,A3,N)
CLQERR=-2.*A3/(AREA*CREF)
WRITE(6,7) CLQERR
C
CMQERR COMPUTATION
C
CALL TRNPRD(X,WB,A4,N)
CMQFRR=-2.*A4/(AREA*CREF*CREF)
WRITE(6,8) CMQFRR
C
STABILITY DERIVATIVES AT VARYING LOAD FACTOR
C
AC=(AREA*CREF)/(2.*V*V)
C
CLQI COMPUTATION
C
CALL DISMPY(WB,AMASS,WA,N,N,1,2J,IC,0,IND)
CALL DISMPY(WC,WA,WB,N,N,1,20,IA,0,IND)
CALL MATMPY(R,WB,WC,N,N,1)
CALL TRNPRD(WI,WC,ACLQI,N)
CLQI=ACLQI/AC
WRITE(6,9) CLQI
C
CMQI COMPUTATION
C
CALL TRNPRD(X,WC,ACMQI,N)
CMQI=ACMQI/(AC*CREF)
WRITE(6,10) CMQI
C
CLWDI COMPUTATION
C
CLWDI=-ACLQI/AREA
WRITE(6,11) CLWDI
C
DERV0710
DERV0720
DERV0730
DERV0740
DERV0750
DERV0760
DERV0770
DERV0780
DERV0790
DERV0800
DERV0810
DERV0820
DERV0830
DERV0840
DERV0850
DERV0860
DERV0870
DERV0880
DERV0890
DERV0900
DERV0910
DERV0920
DERV0930
DERV0940
DERV0950
DERV0960
DERV0970
DERV0980
DERV0990
DERV1000
DERV1010
DERV1020
DERV1030
DERV1040
DERV1050

```

```

C          CMWDI COMPUTATION
C
C          CMWDI=-ACMOI/(AREA*CREF)
C          WRITE(6,12) CMWDI
C          DO 4 I=1,N
C            4 WR(I)=AMASS(I)*X(I)
C
C          CLTDDI COMPUTATION
C
C          CALL DISMPY(WC,WB,WA,N,N,I,20,IC,0,IND)
C          CALL DISMPY(WC,WA,WB,N,N,I,20,IA,0,IND)
C          CALL MATMPY(B,WB,WC,N,N,I)
C          CALL TRNPRD(WI,WC,ALTDDI,N)
C          CLTDDI=ALTDDI/AREA
C          WRITE(6,13) CLTDDI
C
C          CMTDDI COMPUTATION
C
C          CALL TRNPRD(X,WC,AMTDDI,N)
C          CMTDDI=AMTDDI/(AREA*CREF)
C          WRITE(6,14) CMTDDI
C
C          DCLDN COMPUTATION
C
C          DCLDN=-32.2*CLWDI
C          WRITE(6,15) DCLDN
C
C          DCMDN COMPUTATION
C
C          DCMDN=-32.2*CMWDI
C          WRITE(6,16) DCMDN
C
C          CLALPAE COMPUTATION
C
C          CLALPE=CLALPA/(1.-DCLDN/CLTRIM)

```

```

DERV1060
DERV1070
DERV1080
DERV1090
DERV1100
DERV1110
DERV1120
DERV1130
DERV1140
DERV1150
DERV1160
DERV1170
DERV118
DERV1190
DERV1200
DERV1210
DERV1220
DERV1230
DERV1240
DERV1250
DERV1260
DERV1270
DERV1280
DERV1290
DERV1300
DERV1310
DERV1320
DERV1330
DERV1340
DERV1350
DERV1360
DERV1370
DERV1380
DERV1390
DERV1400

```

```

C
C
C
WRITE(6,17) CLALPE
CMALPAE COMPUTATION
CMALPE=CMALPA+DCMDN*CLALPA/(CLTRIM-DCLDN)
WRITE(6,18) CMALPE
5 FORMAT (10X,7HCLALPA=,E12.5)
6 FORMAT (10X,7HCMALPA=,E12.5)
7 FORMAT (10X,7HCLQERR=,E12.5)
8 FORMAT (10X,7HCMQERR=,F12.5)
9 FORMAT (10X,7HCLQI =,E12.5)
10 FORMAT (10X,7HCMQI =,E12.5)
11 FORMAT (10X,7HCLWDI =,E12.5)
12 FORMAT (10X,7HCMWDI =,E12.5)
13 FORMAT (10X,7HCLTDDI=,E12.5)
14 FORMAT (10X,7HCMTDDI=,E12.5)
15 FORMAT (10X,7HDCLDN =,E12.5)
16 FORMAT (10X,7HDCMDN =,E12.5)
17 FORMAT (10X,7HCLALPE=,E12.5)
18 RETURN
END
DERV1410
DERV1420
DERV1430
DERV1440
DERV1450
DERV1460
DERV1470
DERV1480
DERV1490
DERV1500
DERV1510
DERV1520
DERV1530
DERV1540
DERV1550
DERV1560
DERV1570
DERV1580
DERV1590
DERV1600
DERV1610
DERV1620

```

```

SUBROUTINE SETDRAG(XN,YN,YCP,AREA,CP,XCG,WA,CL,P,N)
C.....
C** SETDRAG COMPUTES THE LEADING EDGE THRUST COEFFICIENT
C AND THE INDUCED DRAG COEFFICIENT
C.....
COMMON/CNTROL/ LPANEL,NEAMAX,NCNTL,HALFSW,CREF,AM,CLDES,
1 NCP2,NCP3,NCP4,WNGPNL,HT1PNL,HT2PNL,NCPHT1,NCPHT2,NWNGP,
2 NHT1P,NHT2P,HALFB,ALPH,HALFB1,HALFB2,NCPSWL,NCPWNG,MAX
INTEGER WNGPNL,HT1PNL,HT2PNL
DIMENSION XN(N,4),YN(N,4),YCP(1),AREA(1),CP(1),XCG(1),WA(1)
DIMENSION HEAD(6),P(1)
DATA HEAD/5HWING ,5HHORIZ,5HONTAL,5H TAIL,5H(ONE),5H(TWO)/

C
DO 10 I=1,N
WA(I)=WA(I)+ALPH
LFUS=WNGPNL-1
CLF=0.
IF(LFUS.LE.0) GO TO 20
DO 5 I=1,LFUS
5 CLF=CLF+CP(I)*AREA(I)
20 CDF=CLF*ALPH
WRITE(6,15) HEAD(1)
CTT=0.
CD=CDF

C
C**SET UP FOR FIRST CALL TO DRAG.
NA=NCP2
NAM=NCP2-1
NP=NWNGP
NW=WNGPNL
HR=HALFR
ASSIGN 10 TO JRACK
GO TO 100
30 IF(HT1PNL.LE.WNGPNL) GO TO 200
C**SET UP FOR SECOND CALL AND WRITE HEADING.

```

```

SETDU010
SETDU020
SETDU030
SETDU040
SETDU050
SETDU060
SETDU070
SETDU080
SETDU090
SETDU100
SETDU110
SETDU120
SETDU130
SETDU140
SETDU150
SETDU160
SETDU170
SETDU180
SETDU190
SETDU200
SETDU210
SETDU220
SETDU230
SETDU240
SETDU250
SETDU260
SETDU270
SETDU280
SETDU290
SETDU300
SETDU310
SETDU320
SETDU330
SETDU340
SETDU350

```



```

NA=NCP3
NAM=NCP4-1
NP=NHT1P
NW=HT1PNL
HR=HALFR1

C
IH=4
IF(HT2PNL.GT.HT1PNL) IH=5
WRITE(6,15) (HEAD(I),I=2,IH)
ASSIGN 40 TO JRACK
GO TO 100

C
C**SET UP FOR THIRD CALL
40 IF(HT2PNL.LE.HT1PNL) GO TO 200
NA=NCP4
NAM=NCP4-1
NW=HT2PNL
HR=HALFR2
WRITE(6,15) (HEAD(I),I=2,4),HEAD(6)
ASSIGN 200 TO JRACK
C**CALL DRAG AND INCREMENT SUMS
C
100 OCALL DRAG(XN,YN,XCG,YCP,AREA,CP,WA,P(711),N,NA,NAM,NP,NW,HB,AM,CL,
1 CTA,CDA,P(1),P(36),P(71),P(106),P(141),P(176),P(211),P(246),
2 P(281),P(316),P(351),P(386))
CTT=CTT+CTA
CD=CD+CDA
GO TO JRACK,(30,40,200)

C
C**COMPLETE DRAG COMPUTATIONS AND RETURN
200 CD=CD/HALFSW
CTT=CTT/HALFSW
CDBCL=CD/(CL*CL)
WRITE(6,17) CTT,CD,CDBCL
RETURN
SETD0360
SETD0370
SETD0380
SETD0390
SETD0400
SETD0410
SETD0420
SETL0430
SETD0440
SETD0450
SETD0460
SETD0470
SETD0480
SETD0490
SETD0500
SETD0510
SETD0520
SETD0530
SETD0540
SETD0550
SETD0560
SETD0570
SETD0580
SETD0590
SETD0600
SETD0610
SETD0620
SETD0630
SETD0640
SETD0650
SETD0660
SETD0670
SETD0680
SETD0690
SETD0700

```

```
15  FORMAT(//,5X,23HSECTIONAL CD/CL**2 FOR ,6A5)
17  OFORMAT(//,5X,38HTOTAL LEADING EDGE THRUST COEFFICIENT=,E12.5/5X,
1  31HTOTAL INDUCED DRAG COEFFICIENT=,E12.5/5X, 9HCD/CL**2=,E12.5)
END
SETD0710
SETD0720
SETD0730
SETD0740
```

```

OSUBROUTINE DRAG(XN,YN,XCG,YCP,AREA,CP,ALPHA,A,K,NCPCWL,NN,NCPSWL, DRAGUU10
1 IPANEL,HALFB,AM,CL,CTT,CD,DELT,DELTY,XCGL,DELTC,ZBAR,CT,CLA,CDL, DRAGUU20
2 GAMMA,CAK,Y,AK)
C..... D*R*A*G
C** DRAG CALCULATES THE INDUCED DRAG DISTRIBUTION
C.....
DIMENSION XN(K,4),YN(K,4),XCG(1),YCP(1),AREA(1),CP(1),ALPHA(1)
DIMENSION A(NN,1),DELT(1),DELTY(1),XCGL(1),DELTC(1),ZBAR(1)
DIMENSION CT(1),CLA(1),CDL(1),GAMMA(1),CAK(1),Y(1),AK(1)
NCC=NCPCWL-1
NCS=NCPSWL
K2=IPANEL-1
DO 1 I=1,NCS
K4=K2+NCC
K2=K2+1
DELT(I)=SQRT((XN(K3,2)-XN(K3,1))**2+(YN(K3,2)-YN(K3,1))**2)
DELTY(I)=YN(K3,2)-YN(K3,1)
XCGL(I)=XN(K3,1)+(XN(K3,2)-XN(K3,1))*(YCP(K3)-YN(K3,1))/DELTY(I)
XCGT=XN(K4,3)+(XN(K4,4)-XN(K4,3))*(YCP(K3)-YN(K4,3))/DELTY(I)
DELTC(I)=XCGT-XCGL(I)
K2=K4
1 CONTINUE
N=IPANEL
DO 2 I=1,NCC
II=N+I-1
ZBAR(I)=(XCG(II)-XCGL(1))/DELTC(1)
NCC1=NCC+1
KK=1
C PRESSURE DISTRIBUTION INTERPOLATION IN STREAMWISE DIRECTION
C
3 CONTINUE
AR=AM*AM*(DELTY(KK)*DELTY(KK)/(DELT(KK)*DELT(KK)))
IF (AR .GE. 1.0) GO TO 6
DRAGUU30
DRAGUU40
DRAGUU50
DRAGUU60
DRAGUU70
DRAGUU80
DRAGUU90
DRAGUU00
DRAGU110
DRAGU120
DRAGU130
DRAGU140
DRAGU150
DRAGU160
DRAGU170
DRAGU180
DRAGU190
DRAGU200
DRAGU210
DRAGU220
DRAGU230
DRAGU240
DRAGU250
DRAGU260
DRAGU270
DRAGU280
DRAGU290
DRAGU300
DRAGU310
DRAGU320
DRAGU330
DRAGU340
DRAGU350

```

DRAG0360
 DRAG0370
 DRAG0380
 DRAG0390
 DRAG0400
 DRAG0410
 DRAG0420
 DRAG0430
 DRAG0440
 DRAG0450
 DRAG0460
 DRAG0470
 DRAG0480
 DRAG0490
 DRAG0500
 DRAG0510
 DRAG0520
 DRAG0530
 DRAG0540
 DRAG0550
 DRAG0560
 DRAG0570
 DRAG0580
 DRAG0590
 DRAG0600
 DRAG0610
 DRAG0620
 DRAG0630
 DRAG0640
 DRAG0650
 DRAG0660
 DRAG0670
 DRAG0680
 DRAG0690
 DRAG0700

```

DO 5 J=1,NCC
  JN=J+N-1
  A(J,NCC1)=-CP(JN)*SQRT(ZBAR(J))/(1.-ZBAR(J))
DO 4 I=1,NCC
  A(J,I)=ZBAR(J)**(I-1)
4 CONTINUE
5 CONTINUE

C
C SURROUTINE VMSEGN SOLVES A SET OF SIMULTANEOUS EQUATIONS
C WITHOUT INVERTING THE MATRIX
C
CALL VMSEGN(A,AK,CAK,NCC,NCC1)
AC = SQRT(1.0 - AB)
CTL=(3.14159265*DELT(KK)*AC)/(8.0*DELT(KK))
CT(KK)=-CTL*AK(I)*AK(I)
GO TO 7
6 CT(KK)=0.0
7 N=N+NCC
  KK = KK+1
  IF (KK.GT.NCS) GO TO 8
  GO TO 3
8 CONTINUE
  K2=IPANEL-1
  CD = 0.0
  CTT = 0.0
  III=K2
DO 10 I=1,NCS
  CLA(I) = 0.0
  CDL(I)=0.
  III=(I-1)*NCC+K2
DO 9 J=1,NCC
  II = III + J
  DCY=DFLTC(I)*DFLTY(I)
  TT=(CP(II)*AREA(II))/DCY
  CDL(I)=CDL(I)+TT*ALPHA(II)

```

```

9 CLA(I) = CLA(I) + TT
  CDL(I)=CDL(I)+CT(I)
  CTT=CTT+CT(I)*DCY
  GAMMA(I)=CLA(I)*DFLTC(I)/(4.0*HALFB)
  CD=CD+CDL(I)*DCY
10 III=III+NCC
  N=IPANEL
  WRITE (6,13)
  J=N
  DO 11 I=1,NCS
    CDL2=CDL(I)/(CL*CL)
    Y(I)=YCP(J)/HALFB
    J=J+NCC
  11 WRITE (6,12) Y(I),CDL(I),CLA(I),GAMMA(I),CT(I),CDL2
  12 FORMAT (6(F5X,F10.5))
  13 FORMAT (11X,1HY,13X,3HC DI,12X,3HCL I,11X,5HGAMMA,11X,2HCT,10X,9HC DI,
1/CL**2)
  RETURN
  END
DRAG0710
DRAG0720
DRAG0730
DRAG0740
DRAG0750
DRAG0760
DRAG0770
DRAG0780
DRAG0790
DRAG0800
DRAG0810
DRAG0820
DRAG0830
DRAG0840
DRAG0850
DRAG0860
DRAG0870
DRAG0880
DRAG0890

```

```

MINV0010
MINV0020
MINV0030
MINV0040
MINV0050
MINV0060
MINV0070
MINV0080
MINV0090
MINV0100
MINV0110
MINV0120
MINV0130
MINV0140
MINV0150
MINV0160
MINV0170
MINV0180
MINV0190
MINV0200
MINV0210
MINV0220
MINV0230

SUBROUTINE MINV(A,NN)
C.....
C**GAUSSIAN ELIMINATION ROUTINE TO INVERT A WELL-CONDITIONED,
C  DIAGONALLY DOMINANT MATRIX USING THE DIAGONAL ELEMENTS
C  FOR PIVOTING.
C.....
  DIMENSION A(NN,NN)
  DO 30 I=1,NN
    PIV=1./A(I,I)
    A(I,I)=1.0
    DO 31 L=1,NN
      A(I,L)=A(I,L)*PIV
31
C
    DO 30 M=1,NN
      IF(M.EQ.I) GO TO 30
      TT=A(M,I)
      A(M,I)=0.0
C
      DO 32 L=1,NN
        A(M,L)=A(M,L)-A(I,L)*TT
32
30
CONTINUE
RETURN
END

```

```

C ..... SUBROUTINE VMSEQN(AA,A,CA,N,NI)
C ..... VM*SE*E*Q*N
C .....
C ..... SUBROUTINE VMSEGN SOLVES A SET OF SIMULTANEOUS EQUATIONS
C ..... WITHOUT INVERTING THE MATRIX
C ..... RFFFRFCF-
C ..... THE VECTOR METHOD OF SOLVING SIMULTANEOUS LINEAR EQUATIONS
C ..... BY- EVFRETT W. PURCFL
C ..... JOURNAL OF MATH. PHY. VOL.32/1953
C ..... DIMENSION AA(N,NI),A(I),CA(I)
C .....
1 A(I)=-AA(I,I+1)/AA(I,I)
  K=2
  NCI=N
2 NCI=NCI-1
  NC=K*NCI
  SUM1=0.
  KI=K-.1
  JJ=1
  DO 3 J=1,K1
    SUM1=SUM1+AA(K,J)*A(JJ)
3 JJ=JJ+NCI+1
  SUM1=SUM1+AA(K,K)
  DO 5 I=1,NCI
    SUM2=0.
    JJ=I+1
  DO 4 J=1,K1
    SUM2=SUM2+AA(K,J)*A(JJ)
4 JJ=JJ+NCI+1
  KK=K+1
  SUM2=SUM2+AA(K,KK)
5 CA(I)=-SUM2/SUM1
  M=1
  L=0

```

VMSQ0010
VMSQ0020
VMSQ0030
VMSQ0040
VMSQ0050
VMSQ0060
VMSQ0070
VMSQ0080
VMSQ0090
VMSQ0100
VMSQ0110
VMSQ0120
VMSQ0130
VMSQ0140
VMSQ0150
VMSQ0160
VMSQ0170
VMSQ0180
VMSQ0190
VMSQ0200
VMSQ0210
VMSQ0220
VMSQ0230
VMSQ0240
VMSQ0250
VMSQ0260
VMSQ0270
VMSQ0280
VMSQ0290
VMSQ0300
VMSQ0310
VMSQ0320
VMSQ0330
VMSQ0340
VMSQ0350

```

KNC=(K-1)*NCI
KI=0
DO 8 I=1,NC
IF (I.GT.KNC) GO TO 7
MM=(M-1)*NCI+1
IF (I.EQ.MM) GO TO 9
6 KK=KK+1
IL=I+L
A(I)=CA(KK)*BASE+A(IL)
GC 8
7 II=-1,NC
A(II)=CA(II)
8 CONTINUE
GO TO 10
9 II=MM+M-1
KI=KI+1
RASF=A(II)
KK=0
L=L+1
M=M+1
GO TO 6
10 CONTINUE
K=K+1
IF (K.LF.N) GO TO 2
RETURN
END
VMSQ0360
VMSQ0370
VMSQ0380
VMSQ0390
VMSQ0400
VMSQ0410
VMSQ0420
VMSQ0430
VMSQ0440
VMSQ0450
VMSQ0460
VMSQ0470
VMSQ0480
VMSQ0490
VMSQ0500
VMSQ0510
VMSQ0520
VMSQ0530
VMSQ0540
VMSQ0550
VMSQ0560
VMSQ0570
VMSQ0580
VMSQ0590
VMSQ0600
VMSQ0610

```



```

SUBROUTINE DISMPY(A,B,C,L,M,N,LU,IA,IC,IND)
  DIMENSION A(M),R(M,N),C(N),IND(1)
C**DISMPY MULTIPLIES THE L*M MATRIX A STORED BY ROWS STARTING
C  AT DISC INDEX IA ONTO THE M*N MATRIX B RESIDING IN CORE.  THE
C  N*L PRODUCT MATRIX C IS STORED BY ROWS STARTING AT DISC INDEX
C  IC
C
C**A AND C ARE SINGLY-SUBSCRIPTED ARRAYS USED FOR DISC I/O.
C  IF N IS 1, THE PRODUCT IS RETURNED IN C WITHOUT WRITING TO DISC.
C
C**IF IC IS NEGATIVE WRITIN IS USED RATHER THAN WRITMS.
C**IND IS THE DISC INDEX ARRAY.  LU IS THE DISC LOGICAL UNIT NUMBER.
C
      JWRTIT=1
      IF(IC.GT.0) GO TO 10
      JWRTIT=2
      IC=-IC
      IF(N.FQ.1) JWRTIT=3
      IAA=IA
      ICC=IC
C
      DO 100 I=1,L
      CALL READMS(LU,A,M,IAA)
      DO 50 J=1,N
      C(J)=0.0
      DO 50 K=1,M
      C(J)=C(J)+A(K)*R(K,J)
      50
C
C**GO TO WRITMS, WRITIN OR NO DISC WRITE
      GO TO (60,70,80), JWRTIT
      60  CALL WRITMS(LU,C,N,ICC)
      GO TO 90
      70  CALL WRITIN(LU,C,N,ICC)
      GO TO 90

```

```

DISM0010
DISM0020
DISM0030
DISM0040
DISM0050
DISM0060
DISM0070
DISM0080
DISM0090
DISM0100
DISM0110
DISM0120
DISM0130
DISM0140
DISM0150
DISM0160
DISM0170
DISM0180
DISM0190
DISM0200
DISM0210
DISM0220
DISM0230
DISM0240
DISM0250
DISM0260
DISM0270
DISM0280
DISM0290
DISM0300
DISM0310
DISM0320
DISM0330
DISM0340
DISM0350

```

```

C
C**FOR N-1, STORE RESULT TEMPORARILY IN C(I+1)
80  IF(I.LT.L) C(I+1)=C(I)
C**INCREMENT DISC INDICES
90  IAA=IAA+1
    ICC=ICC+1
100 CONTINUE
    IF(N.GT.1) RETURN
C**RESTORE C-VFCTOR FOR N=1
    A(I)=C(I)
    DO 120 I=2,I
120  C(I-1)=C(I)
    C(L)=A(I)
    RETURN
    END
DISM0360
DISM0370
DISM0380
DISM0390
DISM0400
DISM0410
DISM0420
DISM0430
DISM0440
DISM0450
DISM0460
DISM0470
DISM0480
DISM0490
DISM0500

```

```

C.....SURROUTINE TRNPRD(X,Y,Z,LPANEL)
C.....T*R*N#P*R#D
C.....
C.....SURROUTINE TRNPRD CALCULATES THE DOT PRODUCT OF TWO ARRAYS
C.....
C.....DIMENSION X(LPANEL,1),Y(LPANEL,1)
C.....Z=0.
C.....DO 1 I=1,LPANEL
C.....1 Z=Z+X(I,1)*Y(I,1)
C.....RETURN
C.....END
TRNPO010
TRNPO020
TRNPO030
TRNPO040
TRNPO050
TRNPO060
TRNPO070
TRNPO080
TRNPO090
TRNPO100
TRNPO110

```

10. Appendix

Assumptions for Data Reduction from Reference 3

The present computer program is valid only for thin elastic aeroplanes and therefore requires the reduction of the configuration data of Reference 3 to satisfy the input data format. The following assumptions are made for data reduction .

1. The "Y" locations of the chords in Ref. 3 are assumed to be break lines for the present program.
2. The height of the wing (ZAVWNG) is calculated by taking the average value of z - coordinates of all break lines. In other words, camber is taken to be zero.
3. If the fuselage is not circular, it is modified to a circular shape by assuming a radius equal to the maximum y- coordinate at each station, the center of which is located at the corresponding z- coordinate.
4. The z- coordinate of the fuselage (ZAVFUS) is found by taking average value of centers of circular section.
5. Half of the fuselage width (FUSWTH) is calculated by taking the average radius of fuselage sections at the root chord.
6. If $|(ZAVFUS - ZAVWNG)| \leq (FUSWTH/2)$, the wing is assumed to be in the plane of the fuselage, i.e., $ZAVWNG = ZAVFUS$ and FUSWTH is replaced by the y- coordinate of the root chord of the wing.
7. If the wing and fuselage are not in the same plane, the wing is extended to the center line of the fuselage and the number of break lines for wing is increased by one.
8. The portion of the fuselage ahead of the wing leading edge is replaced by a trapezoid having a width equal to FUSWTH and area equal to the projected area of the fuselage in the x-y plane between the nose and wing root leading edge (See Figure A1).
9. Assumption 8 is also made for the portion of fuselage behind wing root trailing edge. (See Figure A1).
10. The y- coordinates of a horizontal tail and a canard are assumed to be the y- coordinates of the break lines for the corresponding surfaces.
11. The heights of a horizontal tail (ZAVHT(1)) and a canard (ZAVHT(2)) are calculated by taking the average value of the break line z- coordinates of the corresponding surfaces.
12. The semi-width of the fuselage at the root chord of the horizontal tail (WDTH1) and the canard (WDTH2) is calculated by taking the average radius of fuselage sections between the corresponding root chords.

13. If $|(ZAVHT(1) - ZAVFUS)| \leq (WDTH/2)$, the tail is assumed to be in the plane of the fuselage i.e. $ZAVHT(1) = ZAVFS$.
14. If the tail is not in the plane of the fuselage, the tail is extended to the center line of the fuselage and the number of break lines of the tail are increased by one.
15. Assumptions 13 and 14 are also applicable to a canard surface.
16. A break line on the wing induces a break line at the same y- location on the horizontal tail and on the canard and vice versa.
17. Between the two break lines on any aerodynamic surface the constant percent streamwise lines are calculated such that they are at least $(b/20)$ apart.

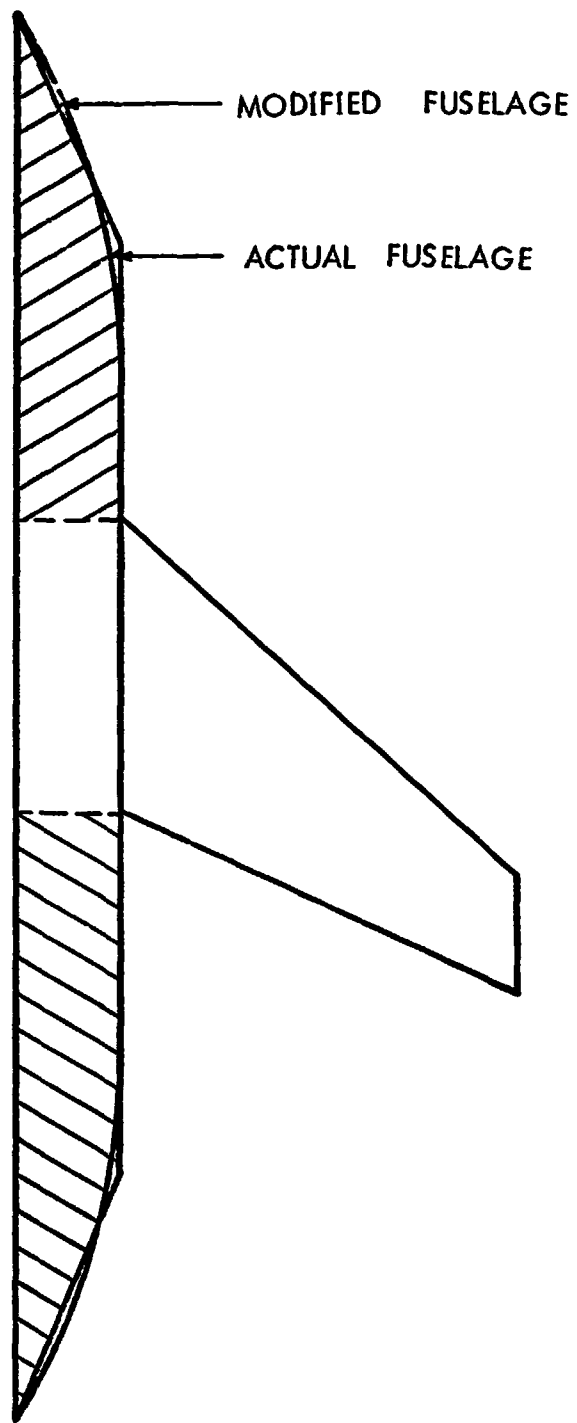


Figure A.1. Fuselage Modification

11. REFERENCES

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6. Roskam, J., Lan, C., Smith, H., and Gibson, G.; "Procedures Used to Determine the Structural Representation for Idealized Low Aspect Ratio Two Spar Fighter Wings," NASA CR-112233; Prepared under NASA Grant NGR 17-002-071 by the Flight Research Laboratory of the Department of Aerospace Engineering of the University of Kansas, October, 1972. Appendix E of the Summary Report, NASA CR-2117.